

# Study of Burnup Reactivity and Isotopic Inventories in REBUS Program

T. Yamamoto<sup>1</sup>, Y. Ando<sup>1</sup>,  
K. Sakurada<sup>2</sup>, Y. Hayashi<sup>2</sup>, and  
K. Azekura<sup>3</sup>

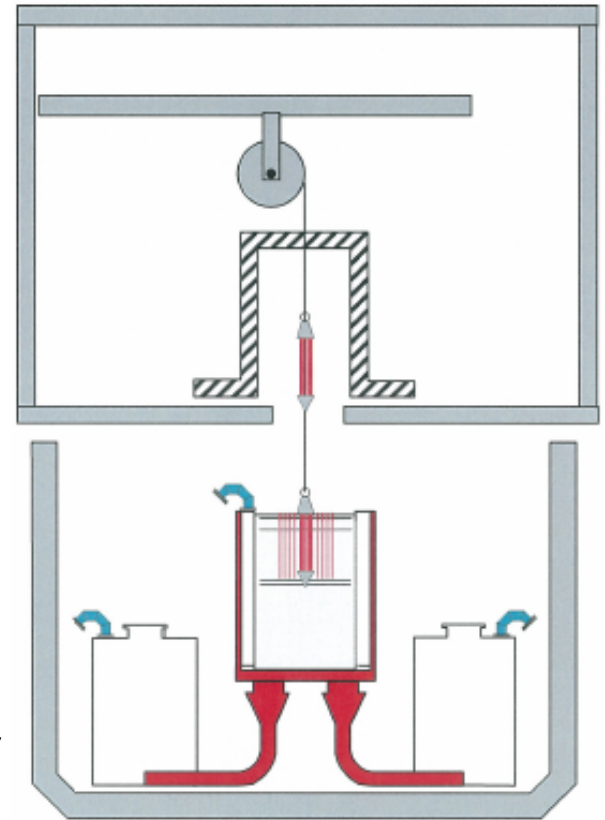
<sup>1</sup>Japan Nuclear Energy Safety Organization (JNES)

<sup>2</sup>Toshiba Corporation

<sup>3</sup>NAIS Co., Inc.

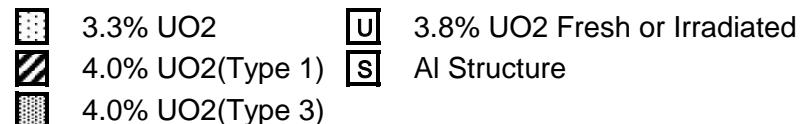
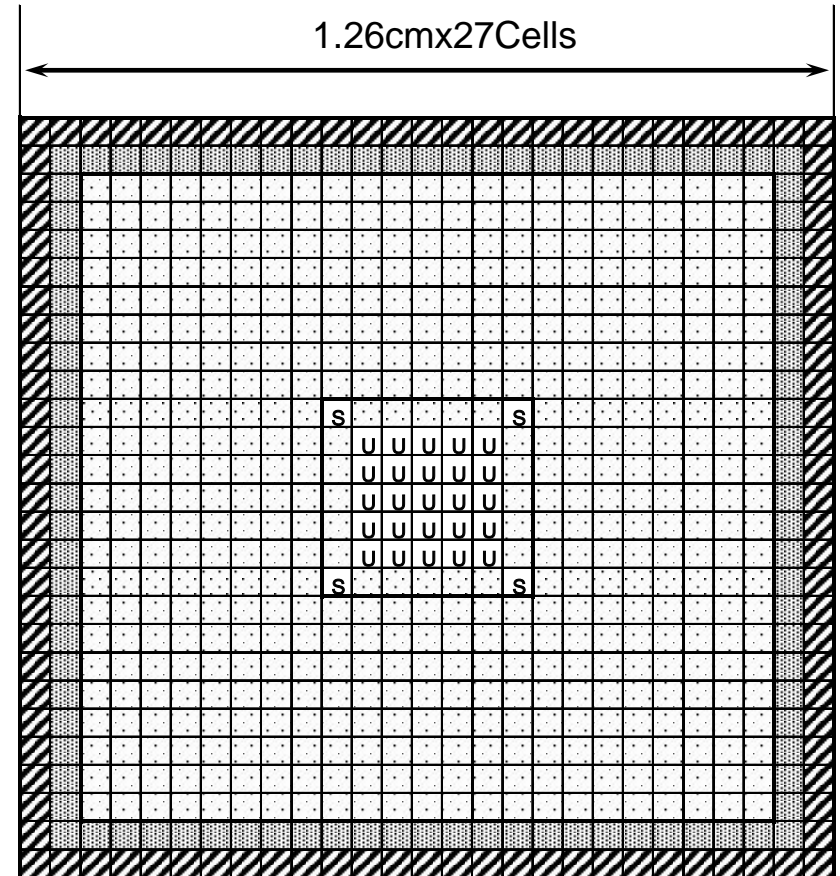
# Contents

1. REBUS Program
2. Determination of Burnup Reactivity in Critical Experiment
3. Analysis of Burnup Reactivity
  - 3.1 Calculated Isotopic Inventories
  - 3.2 Corrected Isotopic Inventories with Measured Data
4. Discussion on Bias of Inventory and Reactivity Calculations



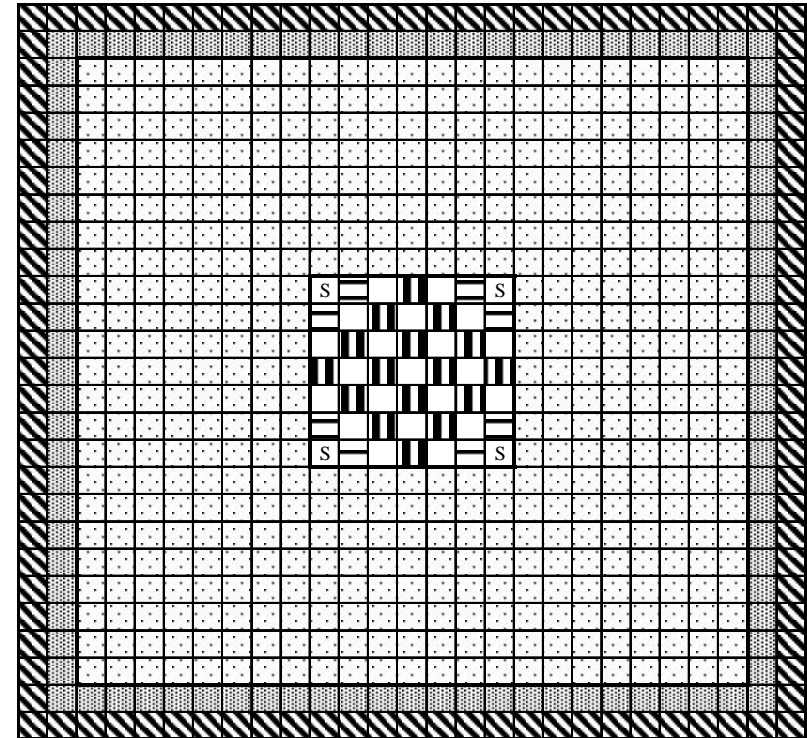
# 1. REBUS Program








- PWR 3.8wt% UO<sub>2</sub>
  - Fresh bundle
  - Irradiated fuel bundle
    - GKN II, 4 cycles
    - Average 54.5 GWd/t



## • BWR MOX

- Fresh bundle (BR3 MOX Puf 6.8 wt%)
- Irradiated BWR MOX fuel (Puf 5.5 wt%) bundle
  - Gundremmingen, 4, 5, 6 cycles
  - Average 60.6 GWd/t



	3.3% UO <sub>2</sub>		BWR MOX irradiated fuel
	4.0% UO <sub>2</sub> (Type 1)		Water channel
	4.0% UO <sub>2</sub> (Type 2)		Al structure
	BR3 MOX fresh fuel		

- VENUS

- Critical water level

- About 60 cm for fresh and about 80 cm for irradiated fuel bundle

- Water level reactivity

- Fission rate distribution ( $^{140}\text{La}$  , 1.59 MeV)

- Flux distribution (Sc or Co wire activation)

- Hot Lab.

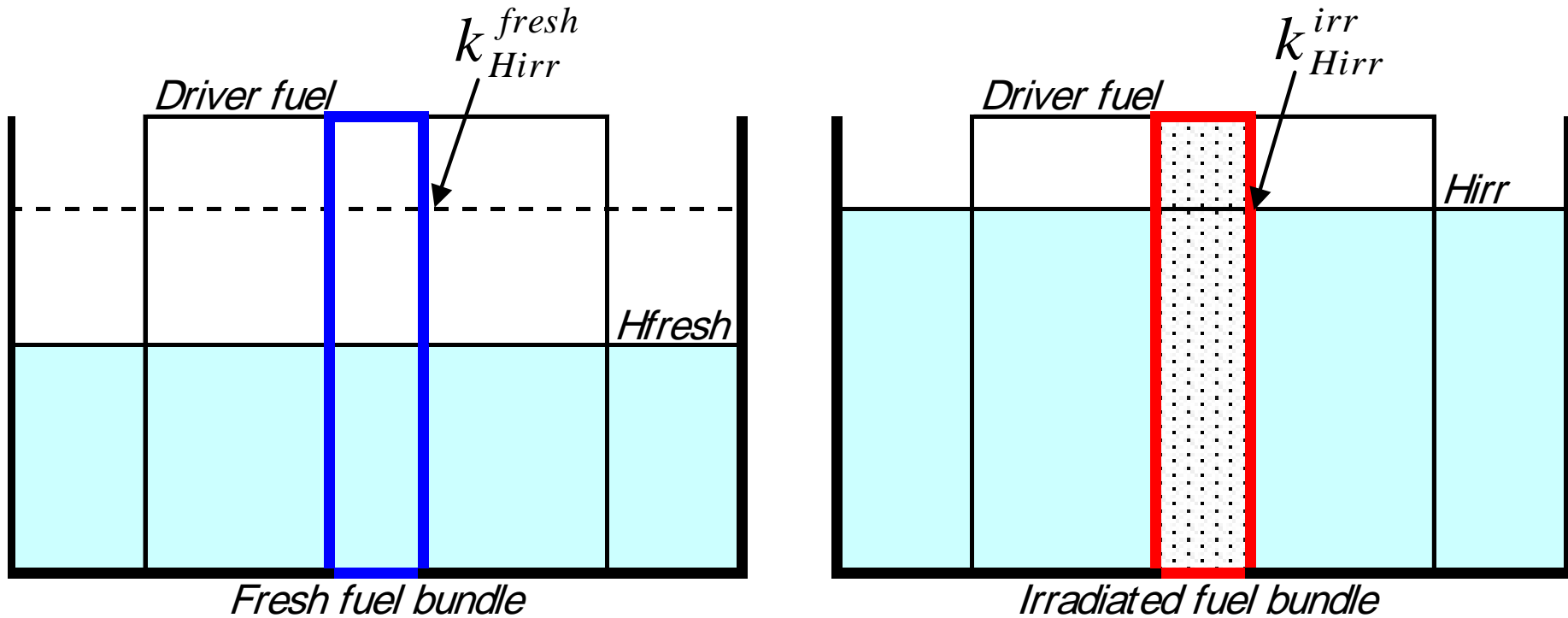
- Burn-up distribution determination (all test rods)

- Gross gamma-ray and Cs-137 Spectrometry

- Fuel sample radiochemical analysis

- U, Pu, Am, Cm (19 Actinides)
    - 19 FP and BU indicator FP

## 2. Determination of Burnup Reactivity in Critical Experiment



$$\rho = \left\{ 1 - \left( 1/k_{Hirr}^{irr} \right) \right\} - \left\{ 1 - \left( 1/k_{Hirr}^{fresh} \right) \right\}$$

In experiment  $k_{Hirr}^{irr} = 1.0$

$$\rho = - \left\{ 1 - \left( 1 / k_{Hirr}^{fresh} \right) \right\}$$

$$\rho = - \int_{H_{fresh}}^{H_{irr}} (\partial \rho / \partial h) dh$$

$(\partial \rho / \partial h)$  : Measurements at  $H_{fresh}$  and  $H_{irr}$

With one group diffusion theory

$$\rho = 1 - \left\{ 1 + M^2 B_{rad}^2 + M^2 \pi^2 / (h + \delta_z)^2 \right\} / k_{\infty}$$

$$(\partial \rho / \partial h) = 2 \pi^2 M^2 / k_{\infty} (h + \delta_z)^3 = \alpha / (h + \delta_z)^3$$

# Measured burnup reactivity

Fuel bundle	PWR UO <sub>2</sub>		BWR MOX	
	Fresh	Irradiated	Fresh	Irradiated
Critical water level (cm)	59.05	81.38	61.10	84.84
Water level reactivity coefficient (\$/cm)	0.186	0.0924	0.191	0.0887
Reflector saving (cm)	12.60	13.23	12.81	14.91
Averaged reflector saving (cm)	12.92		13.86	
$\alpha$ (pcm cm <sup>2</sup> )	$5.65 \times 10^7$	$6.26 \times 10^7$	$6.08 \times 10^7$	$6.42 \times 10^7$
Burnup reactivity (%dk/kk')	-2.28	-2.52	-2.29	-2.42
Averaged burnup reactivity and error (%dk/kk') (relative error)	$-2.40 \pm 0.17$ (7%)		$-2.36 \pm 0.09$ (4%) $-2.48 \pm 0.10$ (4%)*	

\*Corrected for reactivity difference between fresh BR3 and BWR MOX fuel



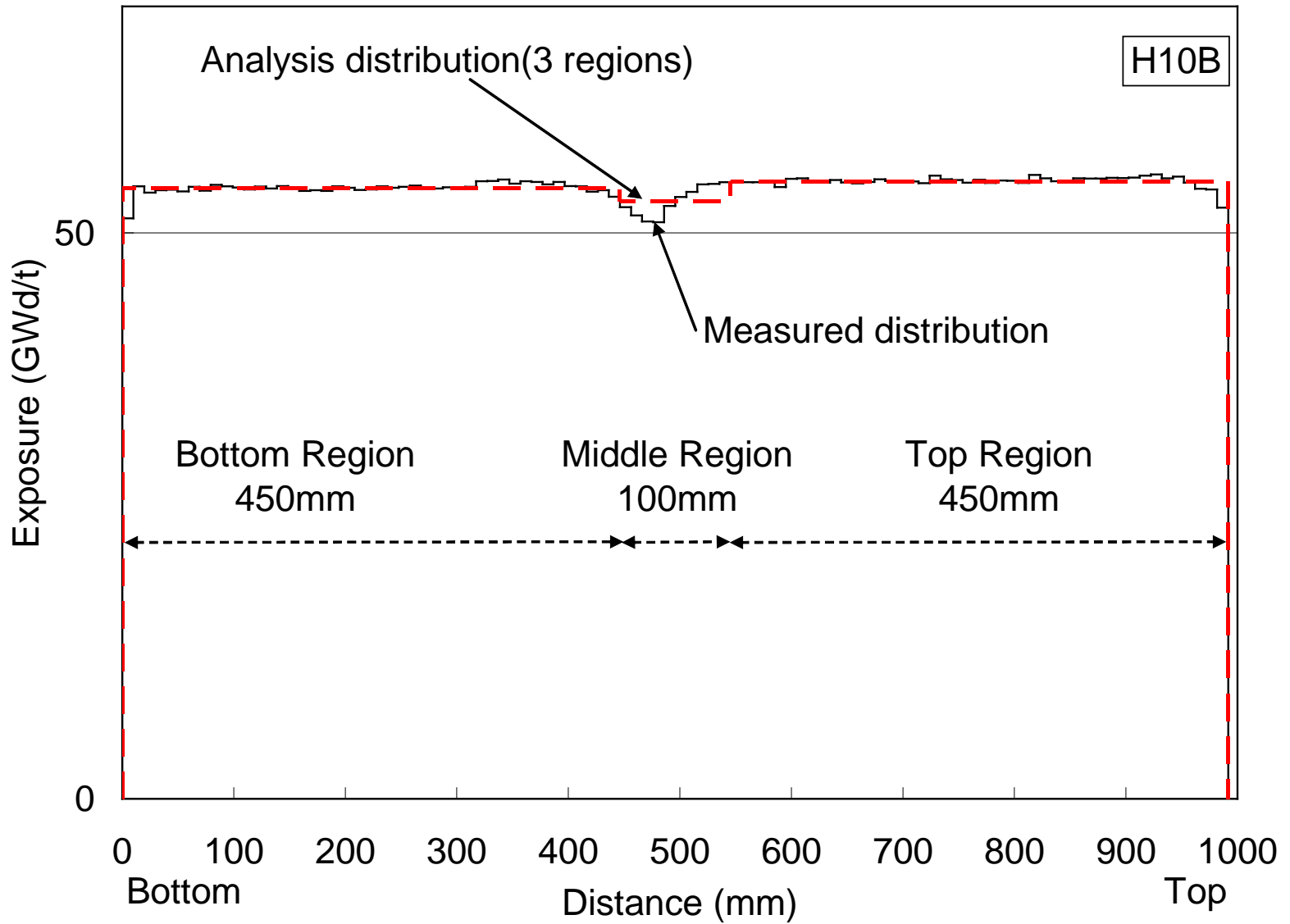
## 3. Analysis of Burnup Reactivity

$$\rho = \left\{ 1 - \left( 1/k_{Hirr}^{irr} \right) \right\} - \left\{ 1 - \left( 1/k_{Hirr}^{fresh} \right) \right\}$$

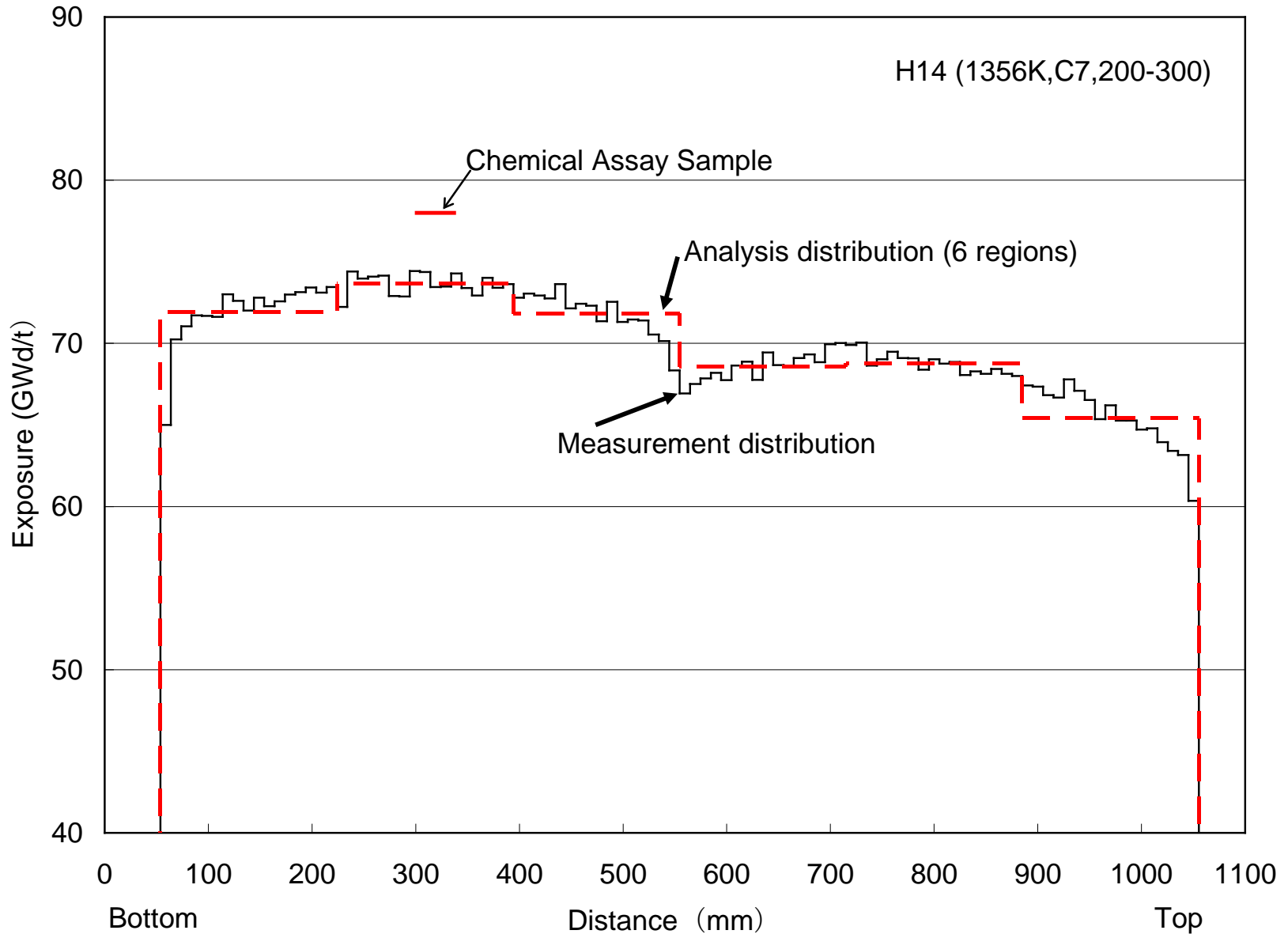
### 3.1 Calculated Isotopic Inventories

- Inventory calculation of PWR UO<sub>2</sub> and BWR MOX Fuels for core calculation loaded with irradiated fuel bundle
  - Pin cell model (assembly mock-up) for PWR UO<sub>2</sub> and assembly model for BWR MOX
  - 107 group energy spectrum (P<sub>ij</sub>) and burnup calculation by SRAC code
  - Resonance cross sections with hyper-fine energy group (PEACO)
  - JENDL-3.2 nuclear data library
  - Tracking irradiation history (rod power, boron, in-channel void)
- Target burnups: Measurements by gross gamma-ray and Cs-137 Spectrometry

– PWR UO2: Axial 3 regions x 25 rods



– BWR MOX: Axial 6 regions x 16 rods



## – Core Calculation

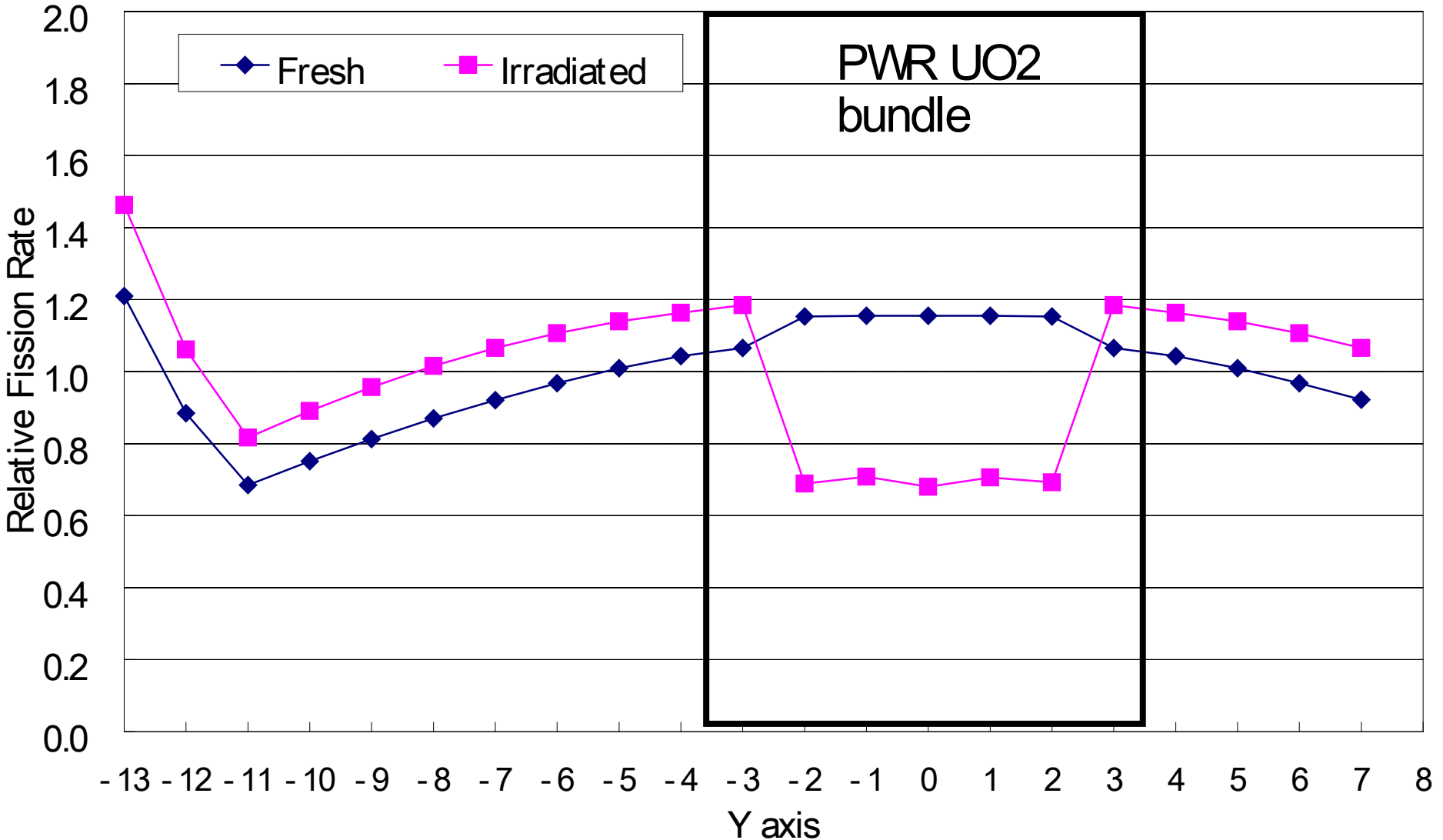
- Lattice calculation
  - Pin cell model
  - 107 energy-group
  - SRAC Pij module with resonance cross sections PEACO
  - JENDL-3.3
- Core calculation
  - Transport calculation THREEDANT
  - Collapsed 16-energy group cross sections
  - XYZ three-dimensional model

# Calculated burnup reactivity with calculated inventories

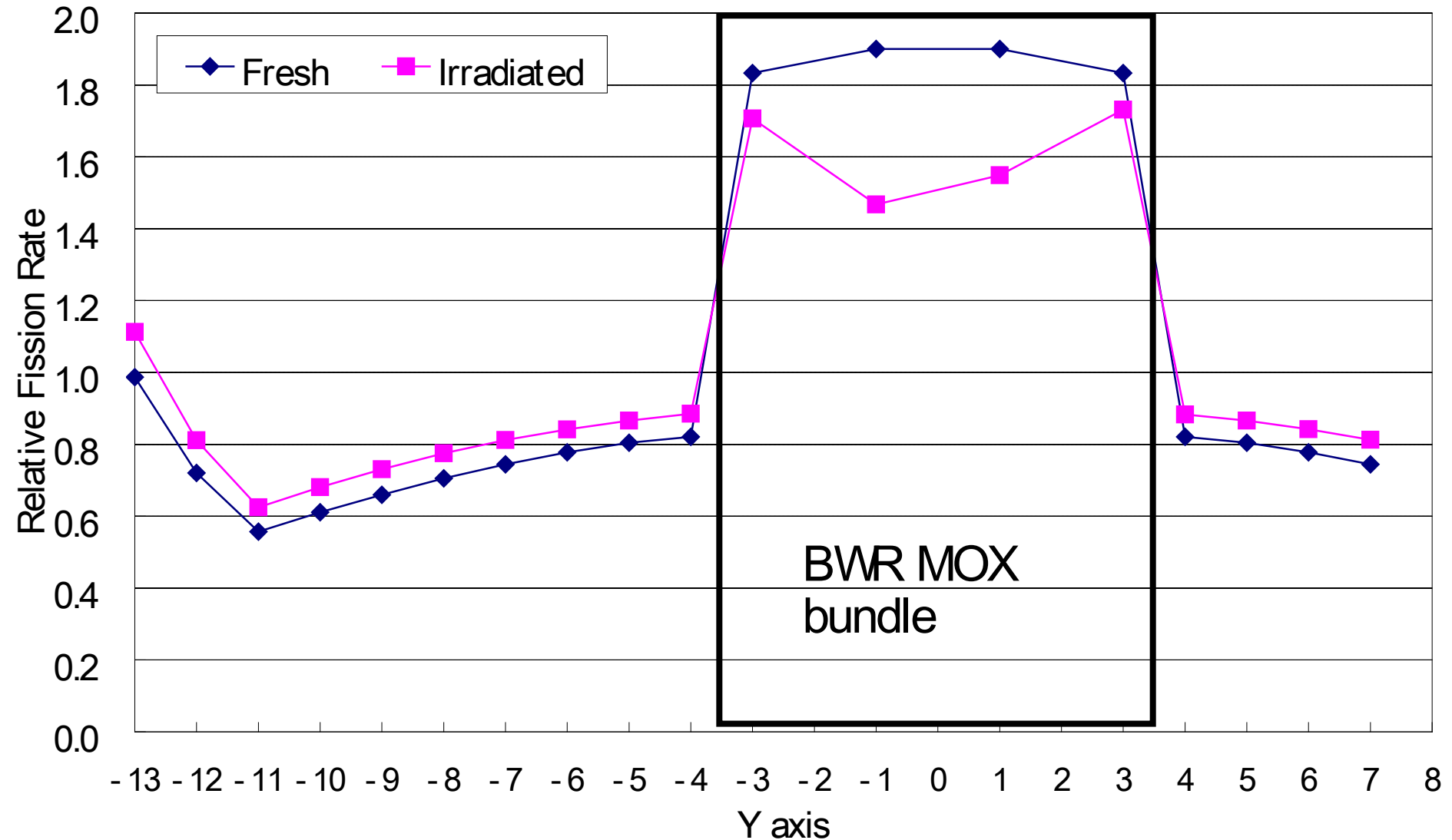
Fuel bundle	PWR UO2		BWR MOX	
k-effective	$k_{Hirr}^{irr}$	$k_{Hirr}^{fresh}$	$k_{Hirr}^{irr}$	$k_{Hirr}^{fresh}$
	0.99445	1.02004	0.99721	1.02205
Burnup reactivity (%dk/kk')	-2.522		-2.437	
Bias of burnup reactivity (Calculated - measured) (%dk/kk')	-0.1227		+0.0438	
C/E	1.051		0.982	

Biases of burnup reactivity (UO2 and MOX):  
 -0.12 and +0.04 %dk/kk' and comparable to  
 measurement errors  $\pm 0.17$  and  $0.10$  %dk/kk'

# Calculated radial fission rate distribution



# Calculated radial fission rate distribution

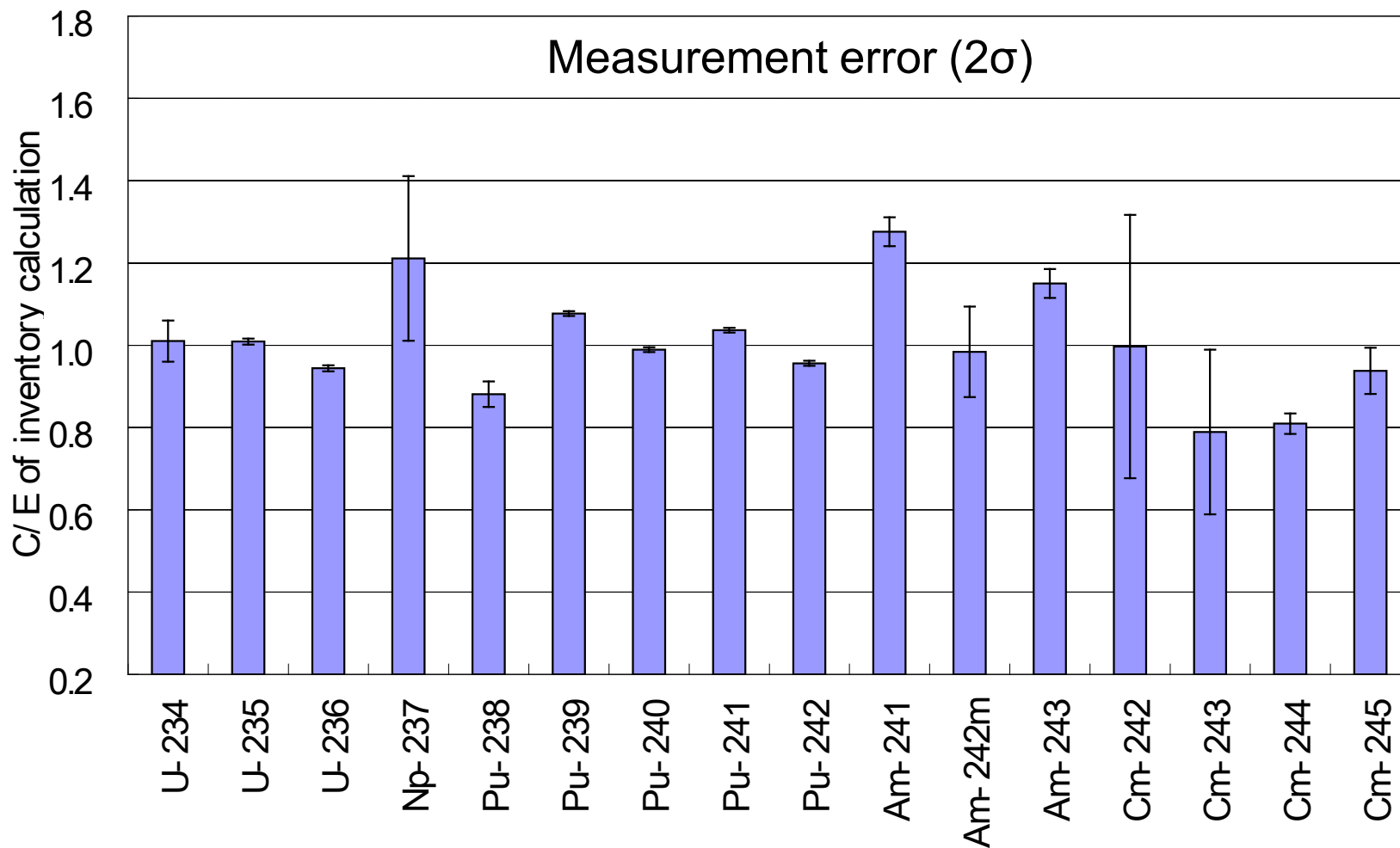


## 3.2 Corrected Isotopic Inventories with Measured Data

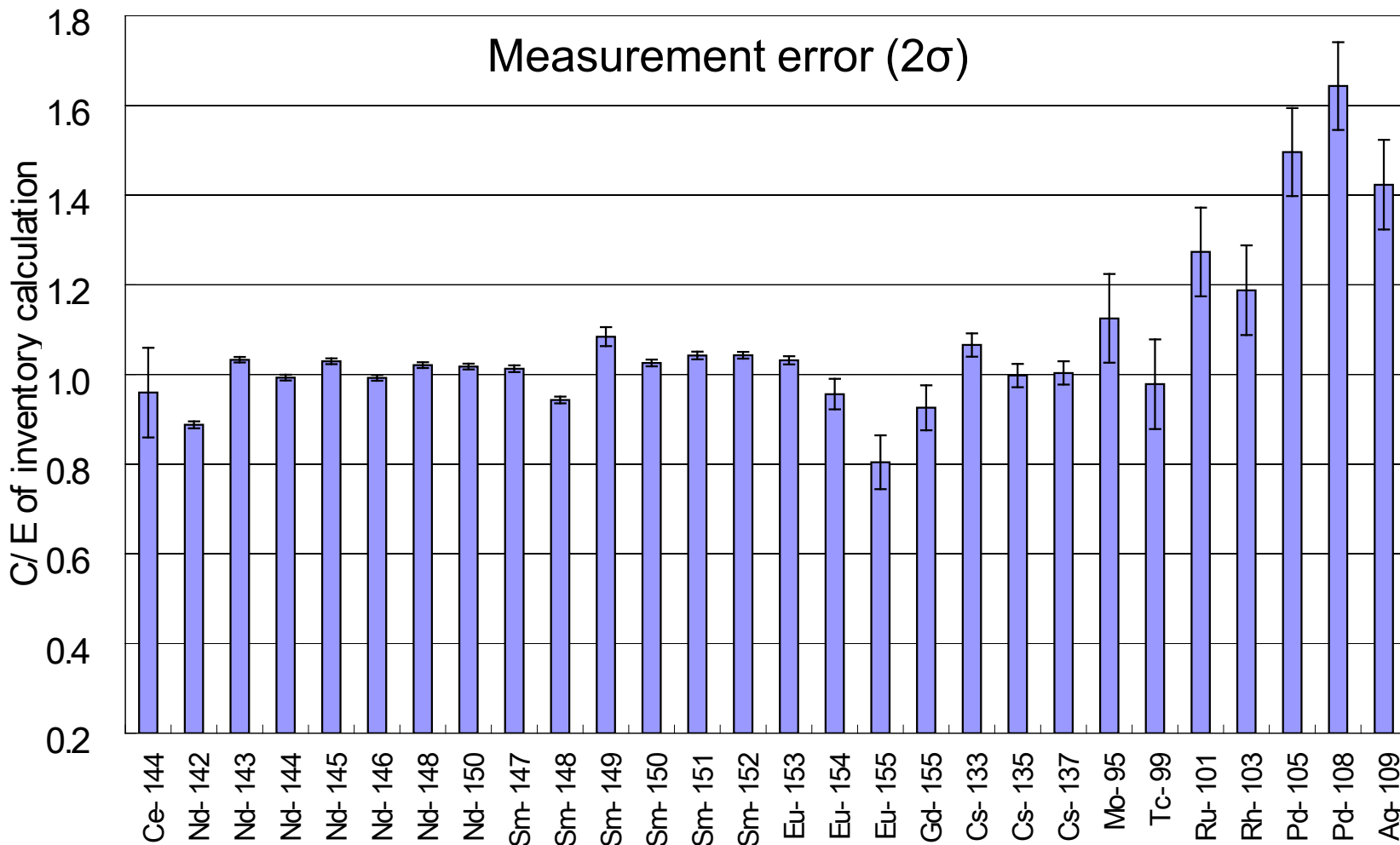
- Comparison was made for a chemical sample between
  - Calculated inventory with burnup determined by “gamma spectrometry”
    - 54.4 GWd/t for PWR UO<sub>2</sub> and
    - 73.6 GWd/t for BWR MOX
  - Measured inventory by radio chemical analysis
- Deviation caused by
  - Burnup (determined by gamma-ray spectroscopy)
  - Calculation model including nuclear data library



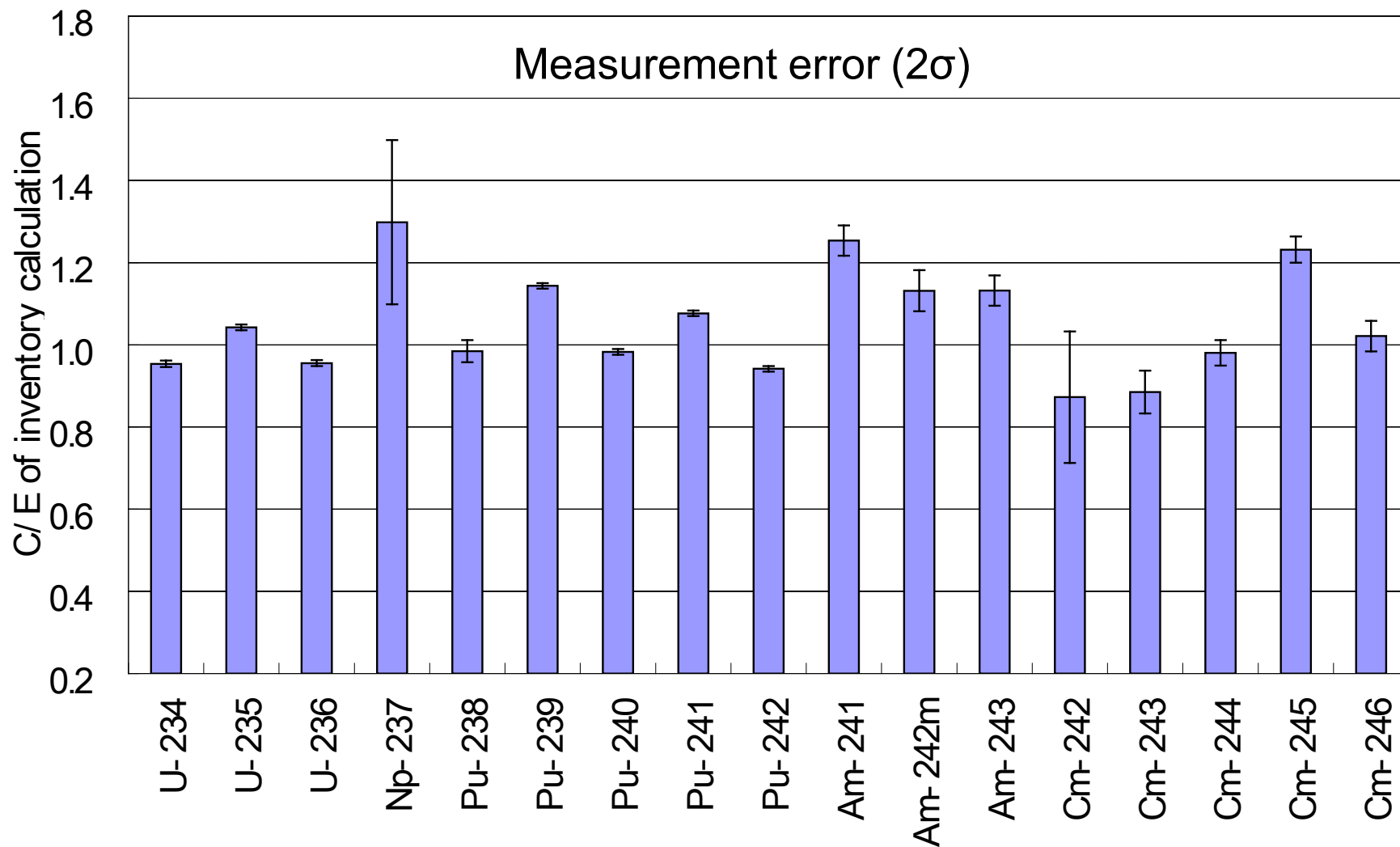
**PWR UO<sub>2</sub>** sample: marked overestimation is observed for Np-237, Am-241, Am-243 and overestimation is observed for Pu-239 and 241



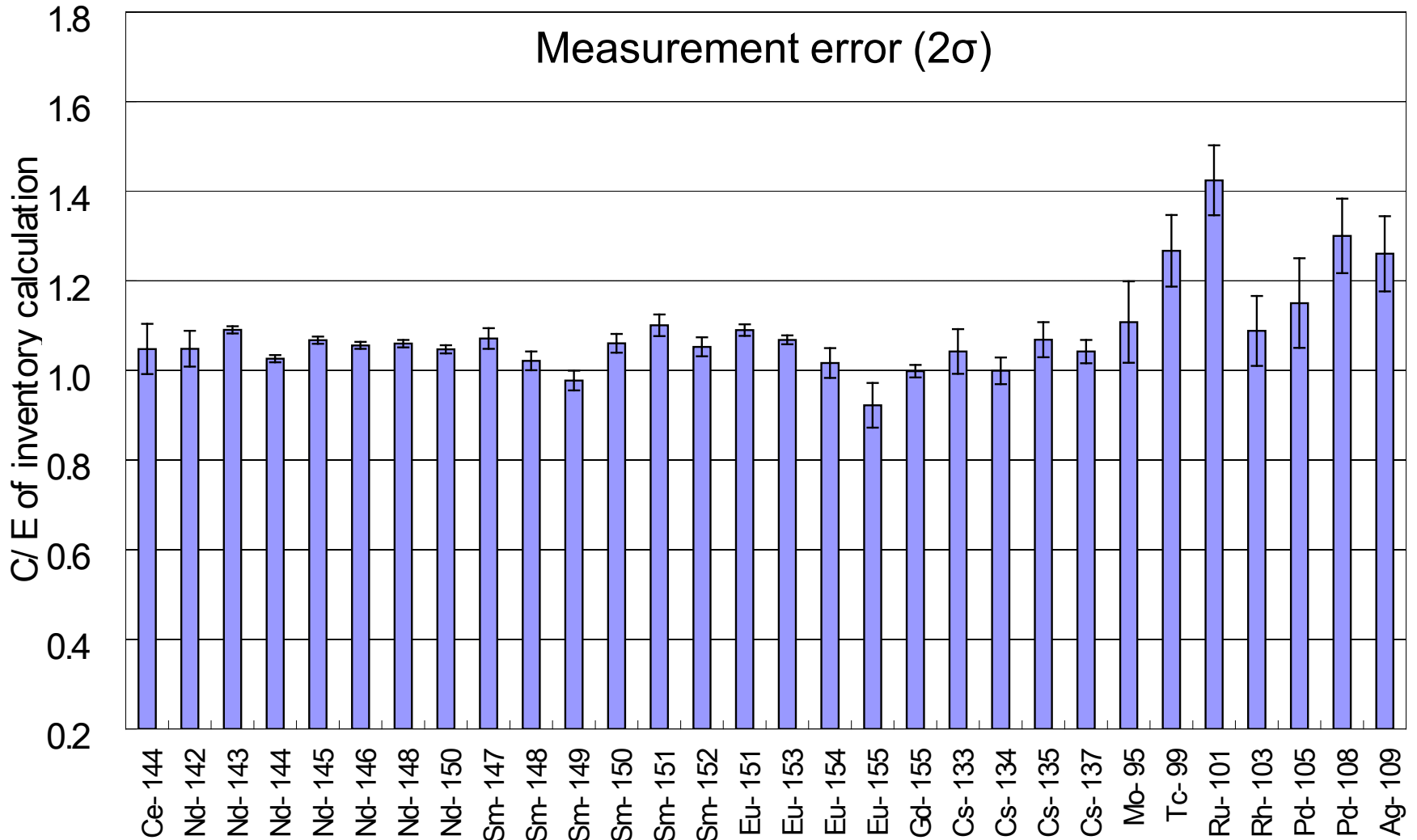
**PWR UO<sub>2</sub> sample: marked overestimation for FP nuclides (Ru-101, Rh-103, Pd-105, -108 and Ag-109)**



**BWR MOX** sample: marked overestimation appears in Np-237, Pu-239, -241, Am-241, -242m, -243, Cm-245



**BWR MOX** sample: overestimation appears for Nd isotopes (= overestimation of burnup) and marked overestimation for metallic FP nuclides



# Correction of Isotopic Inventories by using C/E for the analysis sample with assumption: C/Es are 1.0 at the burnup=0 and proportional to the burnup

$$E_i^j = C_i^j \left[ \left\{ \left( E_i / C_i \right) - 1 \right\} \left( B^j / B \right) + 1 \right]$$

$E_i^j$  : corrected inventory for nuclide  $i$  in a segment of rod  $j$

$C_i^j$  : calculated inventory

$E_i / C_i$ : inverse of the C/E for the nuclide  $i$  for the sample of the radiochemical analysis

$B^j$  : burnup of the segment  $j$  by gamma-ray spectroscopy

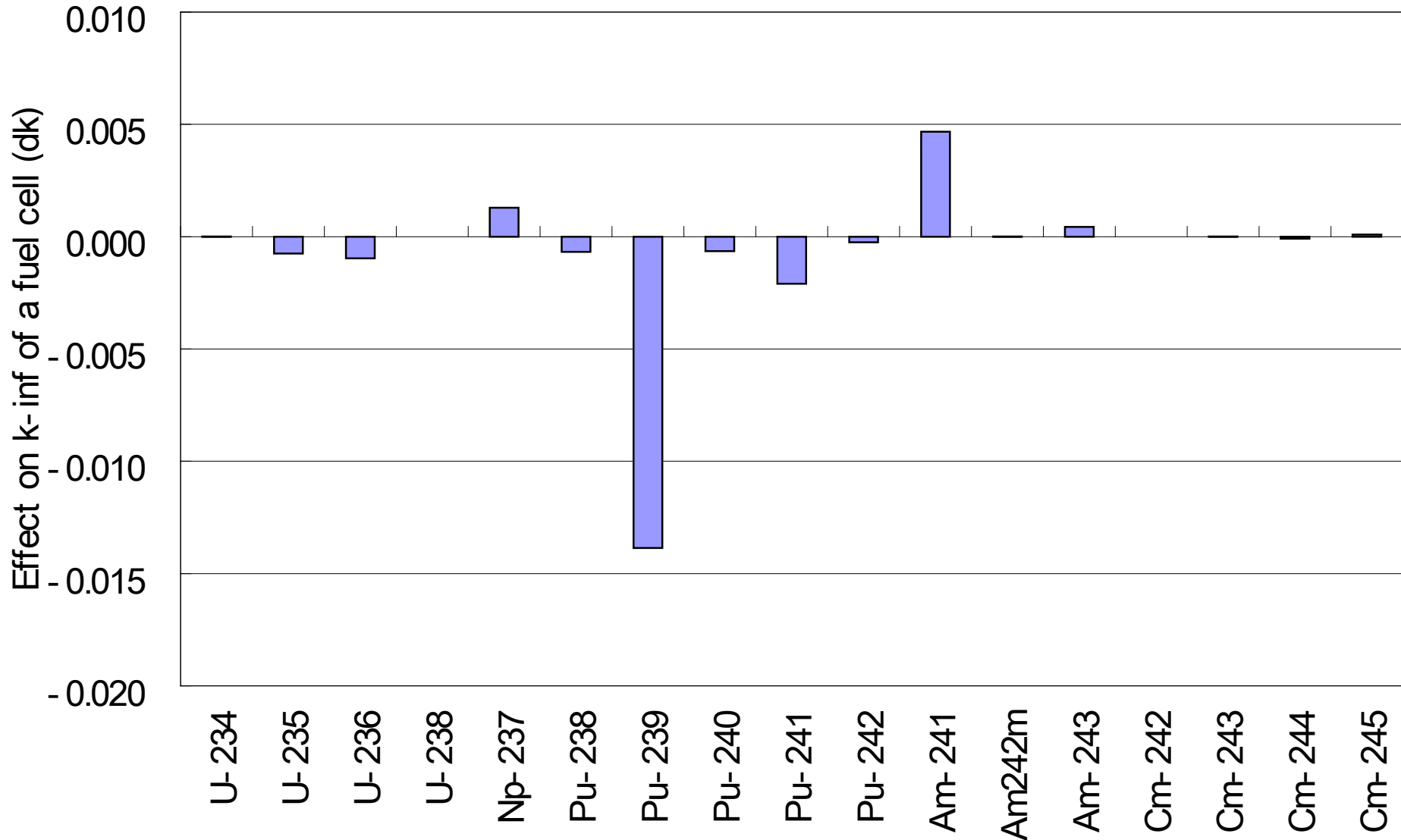
$B$  : burnup value measured by gamma-ray spectroscopy

for the sample

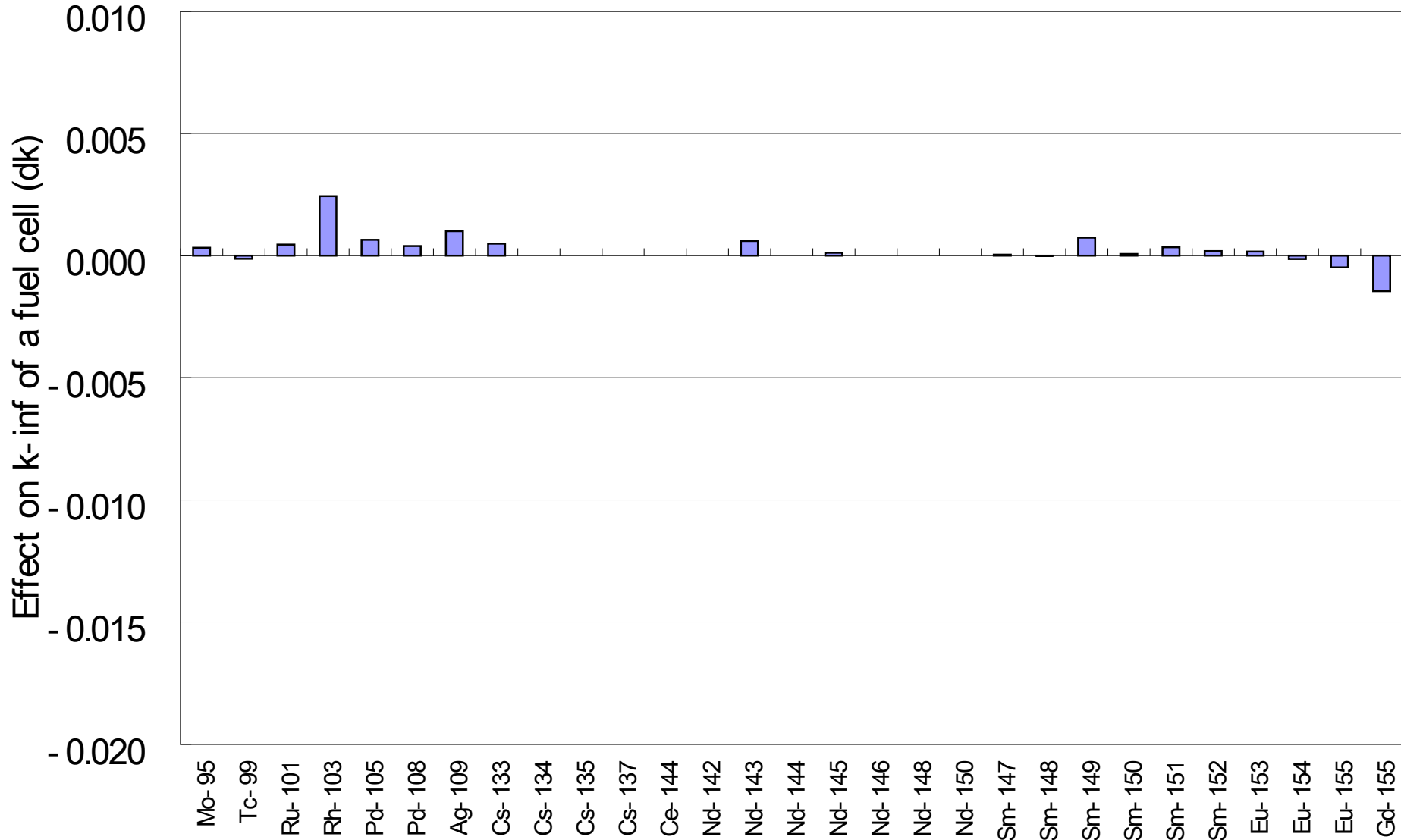
$k_{Hirr}^{irr}$

Calculated with the corrected isotopic inventories

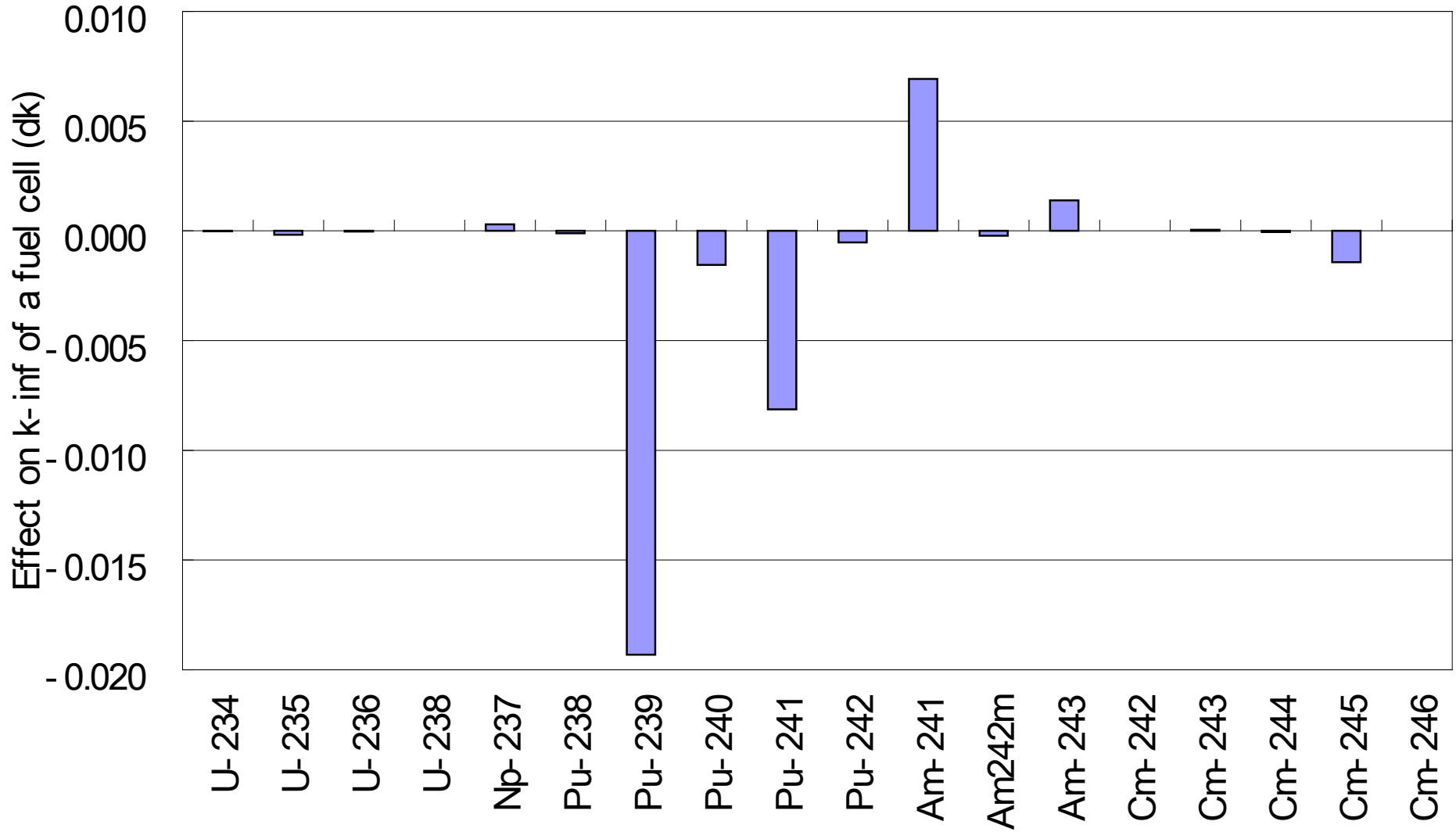
# PWR UO<sub>2</sub> cell: $\Delta k$ -inf caused by correction for actinide nuclides



# PWR UO<sub>2</sub> cell: $\Delta k$ -inf caused by correction for FP nuclides

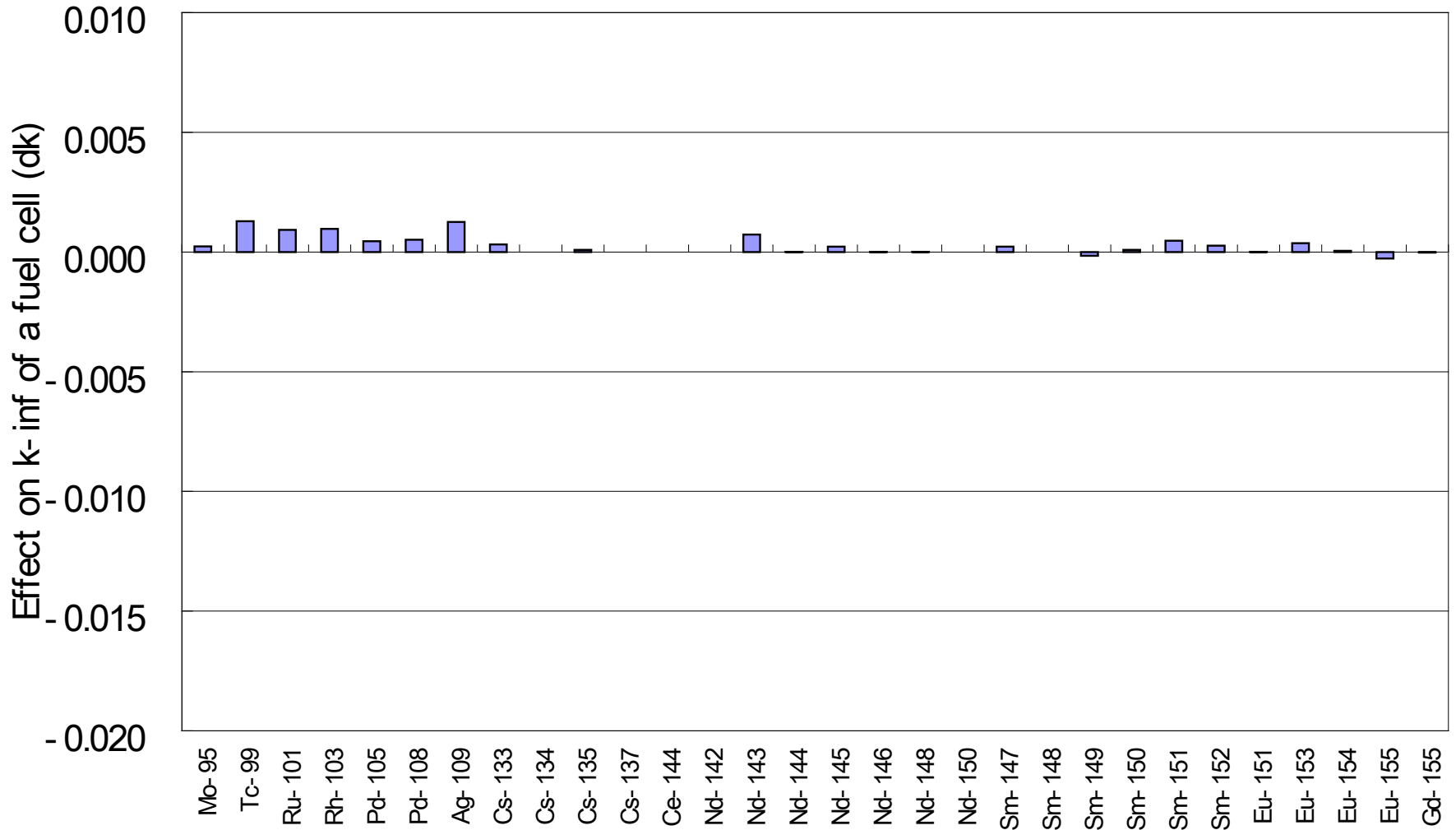


# BWR MOX cell: $\Delta k_{\text{inf}}$ caused by correction for actinide nuclides





# BWR UO<sub>2</sub> cell: $\Delta k$ -inf caused by correction for FP nuclides

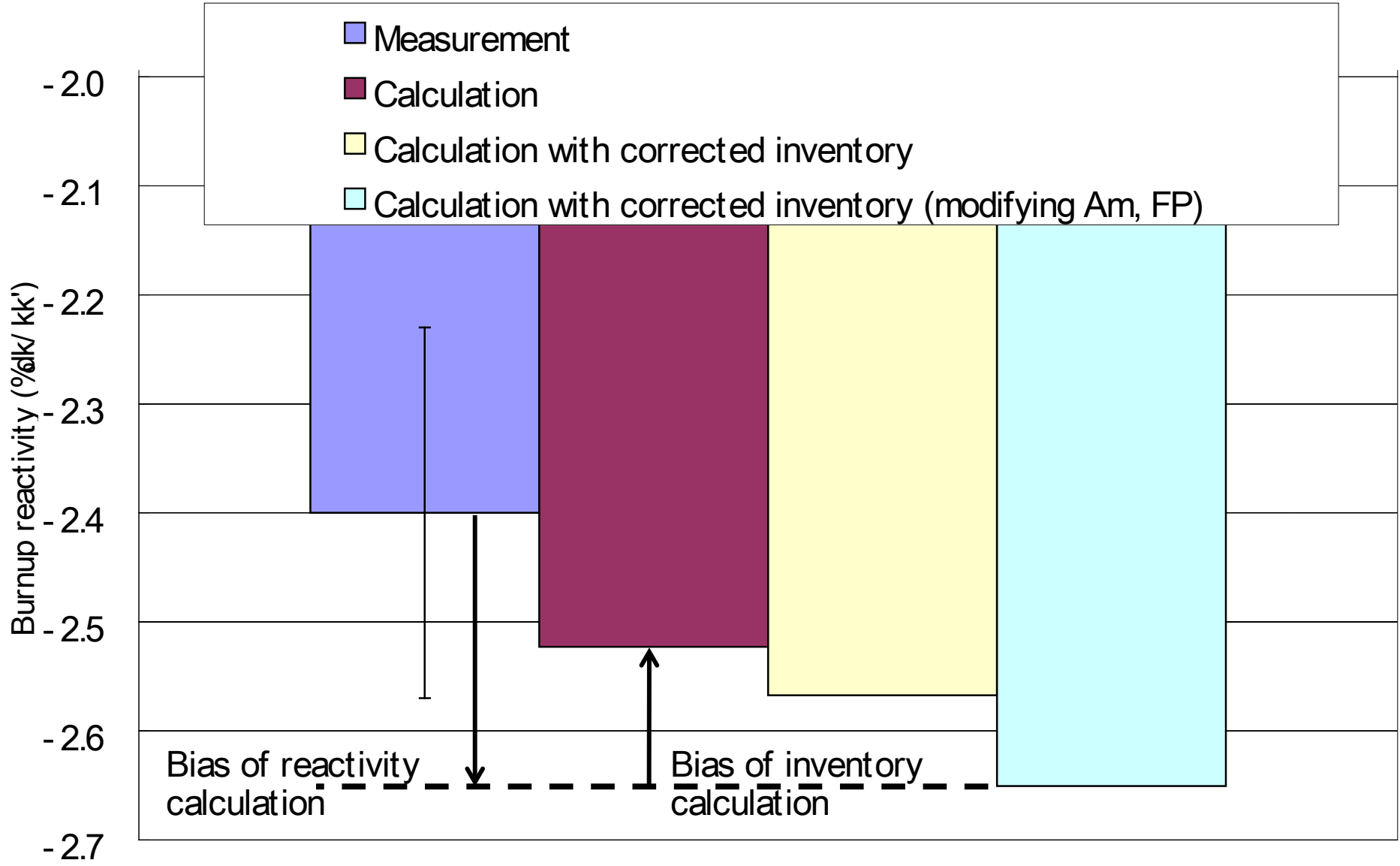


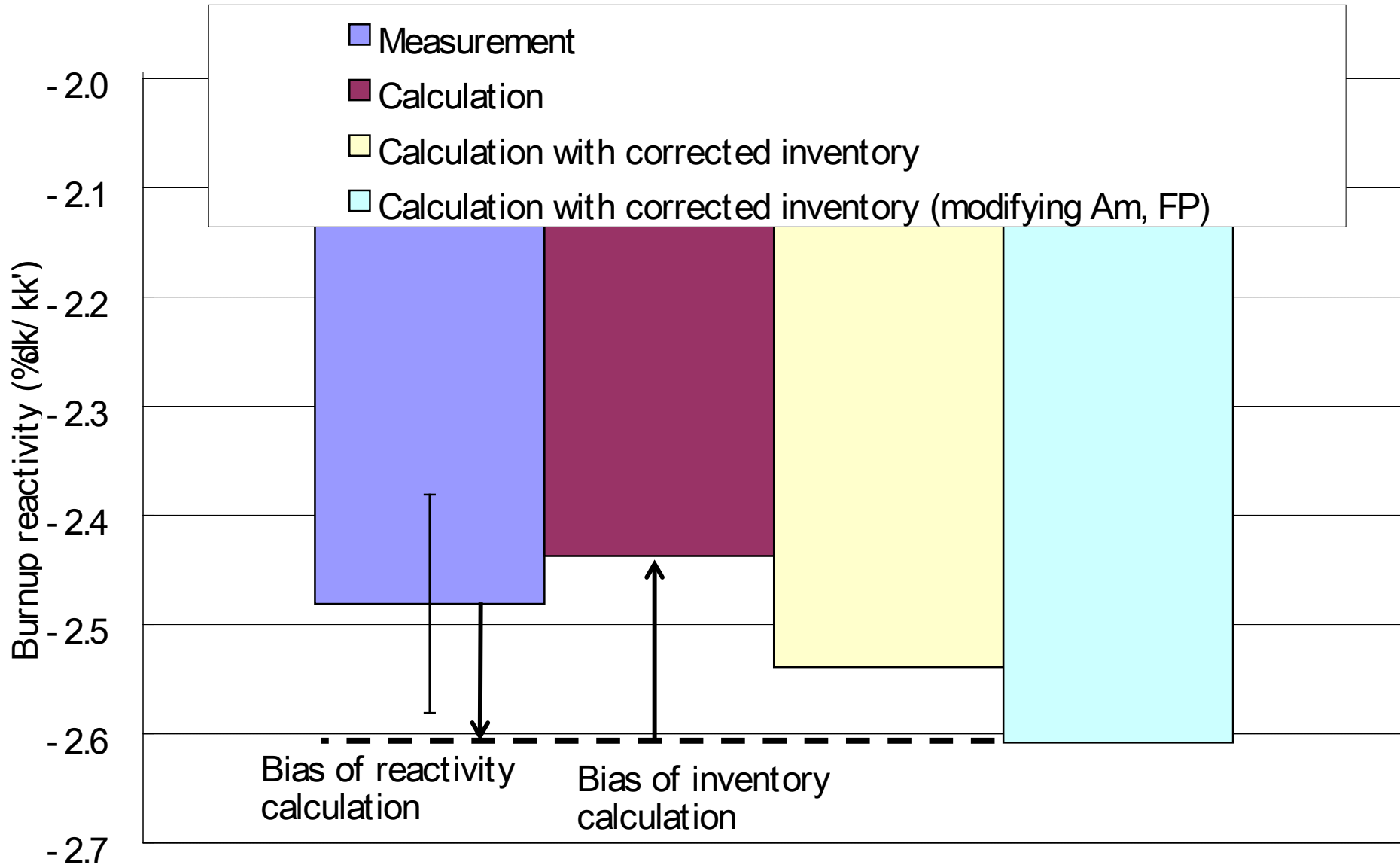
- Americium-241 and metallic FP nuclides are the nuclides showing prominent trend in C/Es and relatively large contribution to the reactivity change of typical infinite fuel cells
- The major inventory of Am-241 caused by decay of Pu-241, since the ratios of Pu-241 to Am-241 at the discharge of the fuel assembly are 30.17 and 8.07 for the PWR UO<sub>2</sub> and BWR MOX fuel, and the cooling times for the isotopic inventory measurement are 7.2 and 4.7 years, respectively
- The values of C/Es for Am-241 are fairly larger than those of Pu-241, which indicate that systematic errors in the measurements of Am-241 are large
- The values of C/Es for some of metallic FP nuclides seem to be too large to accept as they are
- Therefore, as an alternative inventory correction, it is assumed that the C/E of Am-241 equal to that of Pu-241 and the C/Es of the metallic FP nuclides are 1.0

# Calculated burnup reactivity with corrected inventories

Correction case/Fuel bundle	PWR UO2*	BWR MOX
(a) Burnup reactivity with corrected inventories (Difference from that with calculated inventories)	-2.567 (-0.045)	-2.539 (-0.102)
(b) Burnup reactivity with corrected inventories -modifying Am and metallic FP- (Difference from that with calculated inventories)	-2.651 (-0.128)	-2.608 (-0.171)

\*Neutron balance only in the region of the irradiated fuel bundle was considered for the change in  $k_{Hirr}^{irr}$  caused by the corrected inventory for the PWR UO2 fuel bundle





## 4. Discussion on Bias of Inventory and Reactivity Calculations

- The burnup reactivity of irradiated PWR UO<sub>2</sub> (average burnup: 54.5GWd/t) and BWR MOX (average burnup: 60.6GWd/t) fuel bundles in the REBUS program was obtained using the measured critical water levels and water level reactivity coefficients. Those are -2.40 and -2.48%dk/kk' for the PWR UO<sub>2</sub> fuel and BWR MOX fuel bundles, respectively.
- The study for splitting calculation biases of the burnup reactivity into inventory and reactivity calculations was performed with measured isotopic analysis data.

- The calculation biases for the PWR UO<sub>2</sub> fuel bundle are +0.13 %dk/kk' for inventory calculation and -0.25 %dk/kk' for reactivity calculation, which makes total bias -0.12 %dk/kk'. Those for the BWR MOX fuel bundle are +0.17%dk/kk' for inventory calculation and -0.13 %dk/kk' for reactivity calculation, which makes total bias +0.04 %dk/kk'
- The study shows that the calculation biases of the inventory and reactivity are in inverse relation to make the total biases smaller
- The obtained information is useful to improve the analysis tools and models for further reduction of the calculation biases in the burnup reactivity