



Nuclear data sensitivity analyses @ SCK CEN

P. Romojaro, L. Fiorito, C. Alfonso, A. Hernandez-Solis, A. Stankovskiy and G. Van den Eynde

Introduction

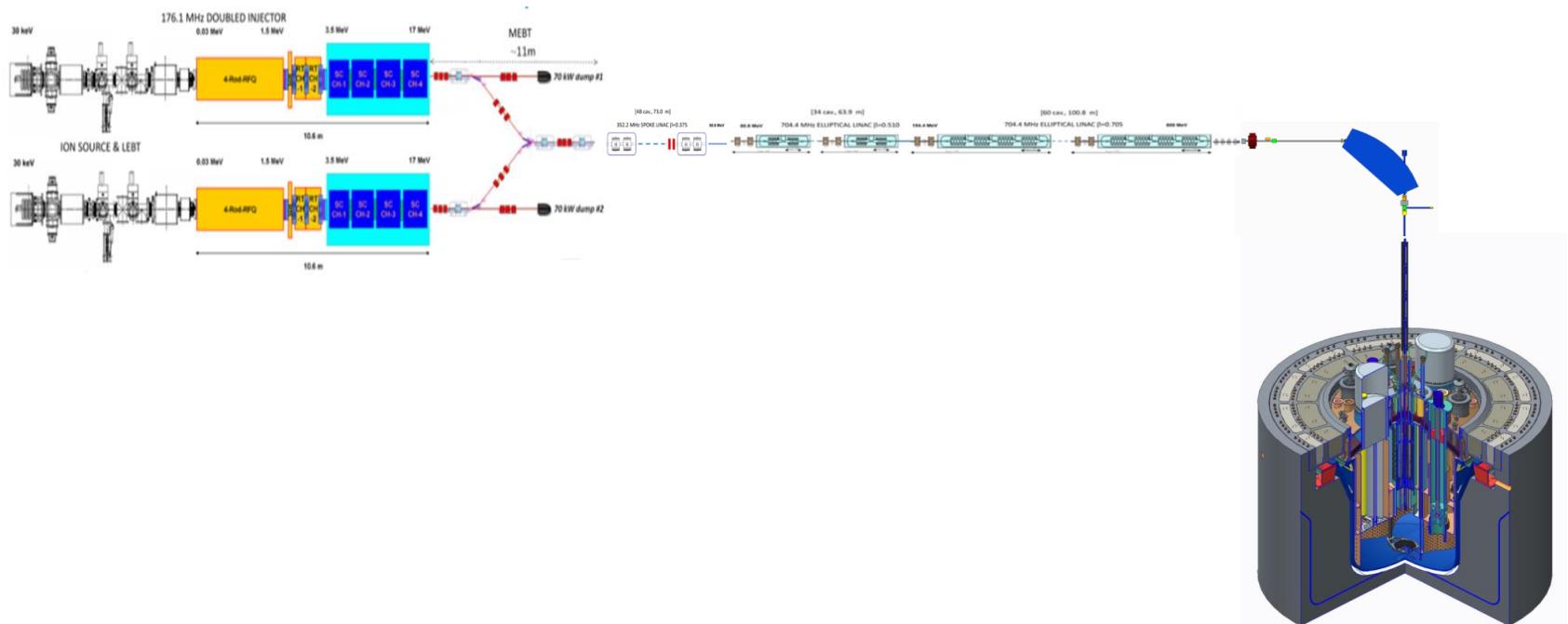
- Sensitivity analyses focused on our applications

- Applications

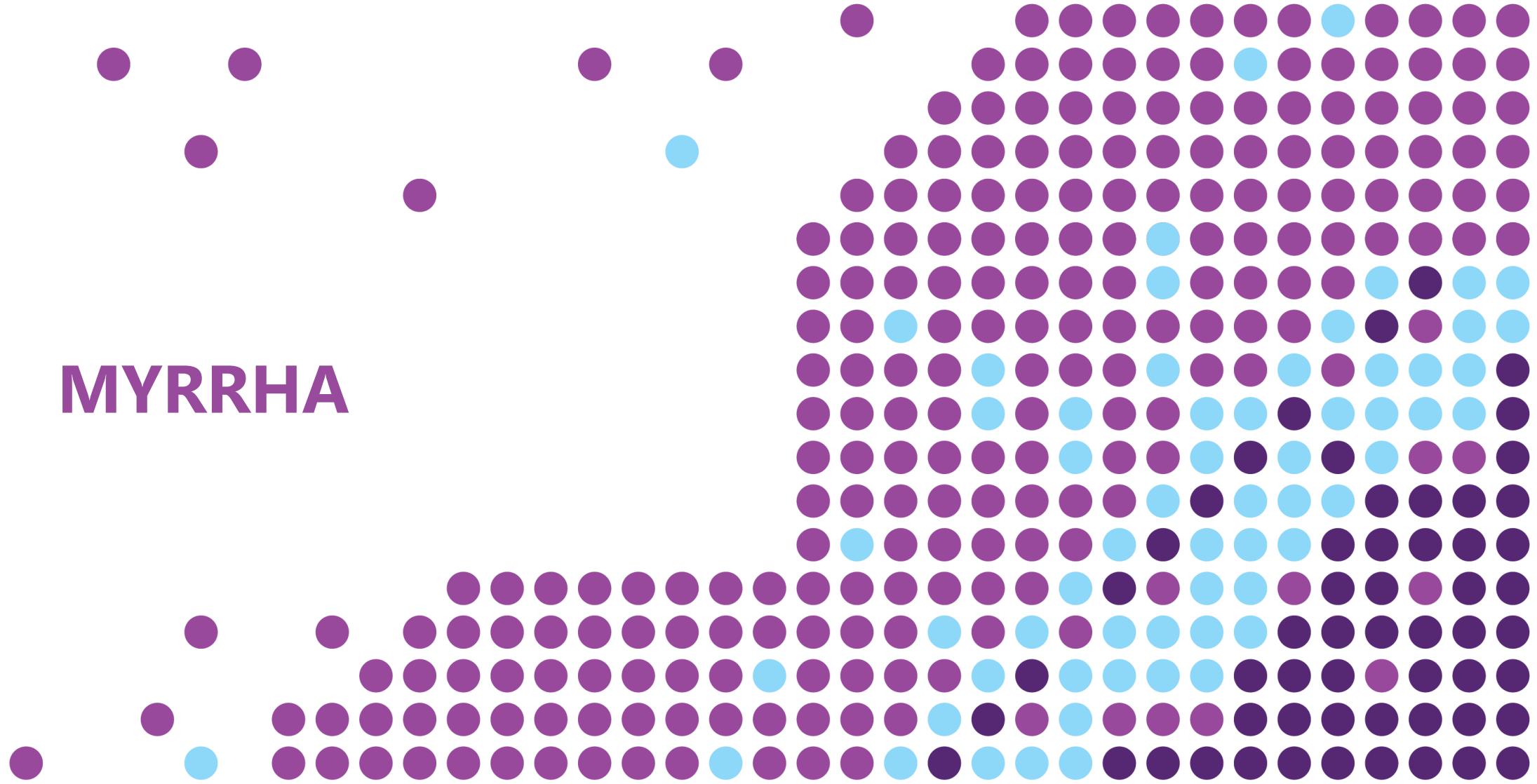
- MYRRHA
- VENUS-F
- SFC

- Codes

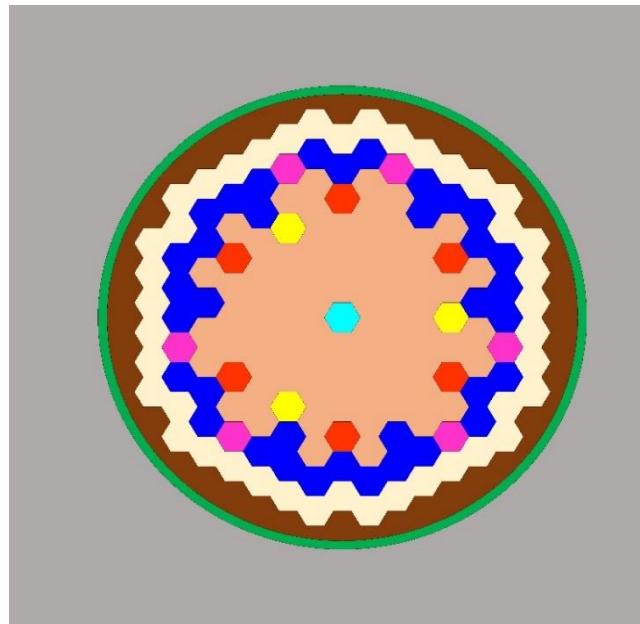
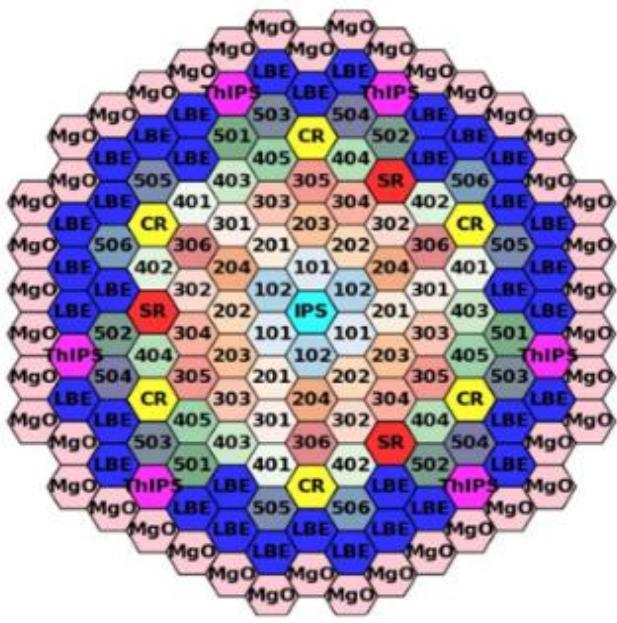
- Serpent 2
- MCNP6
- **SANDY**
- NDaST



MYRRHA



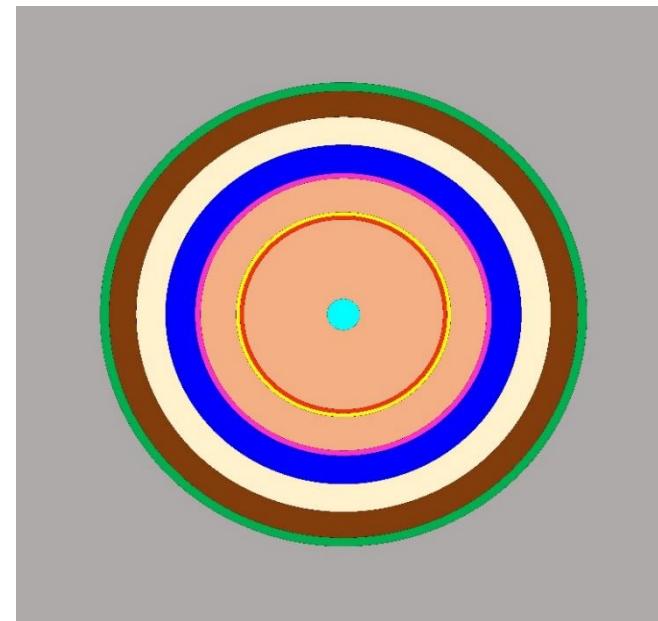
Homogenized critical configuration model



Heterogeneous model
(MCNP + Serpent + OpenMC)

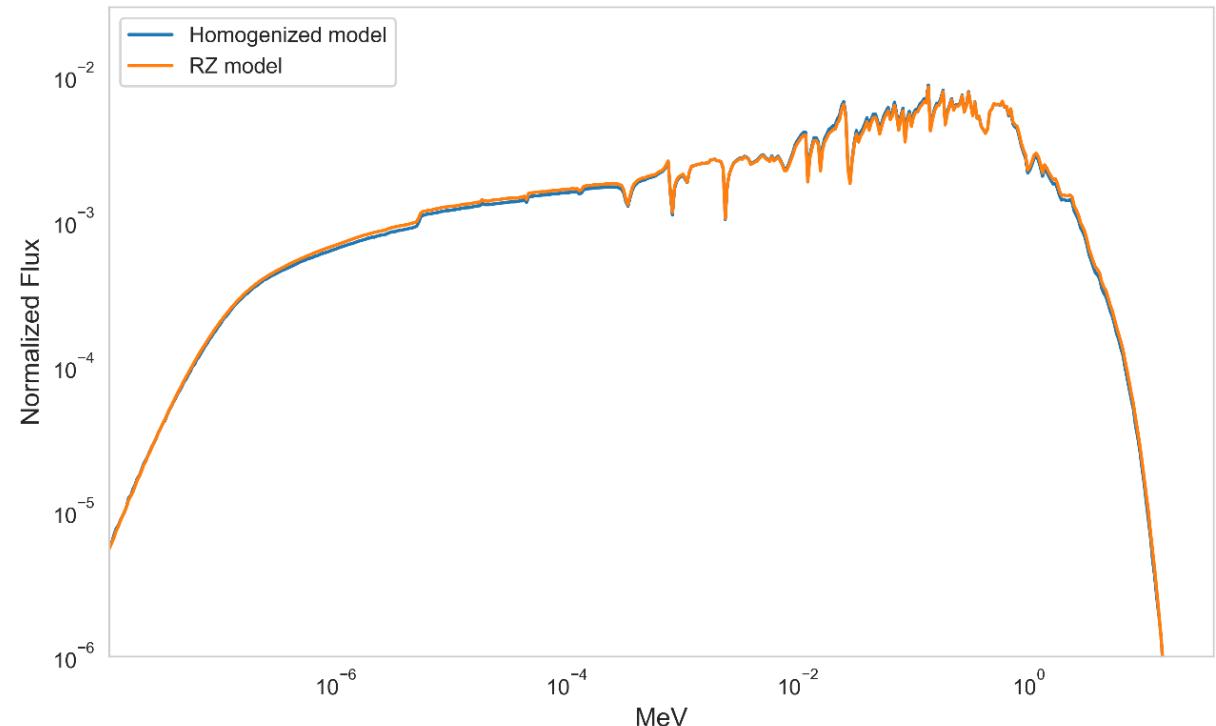
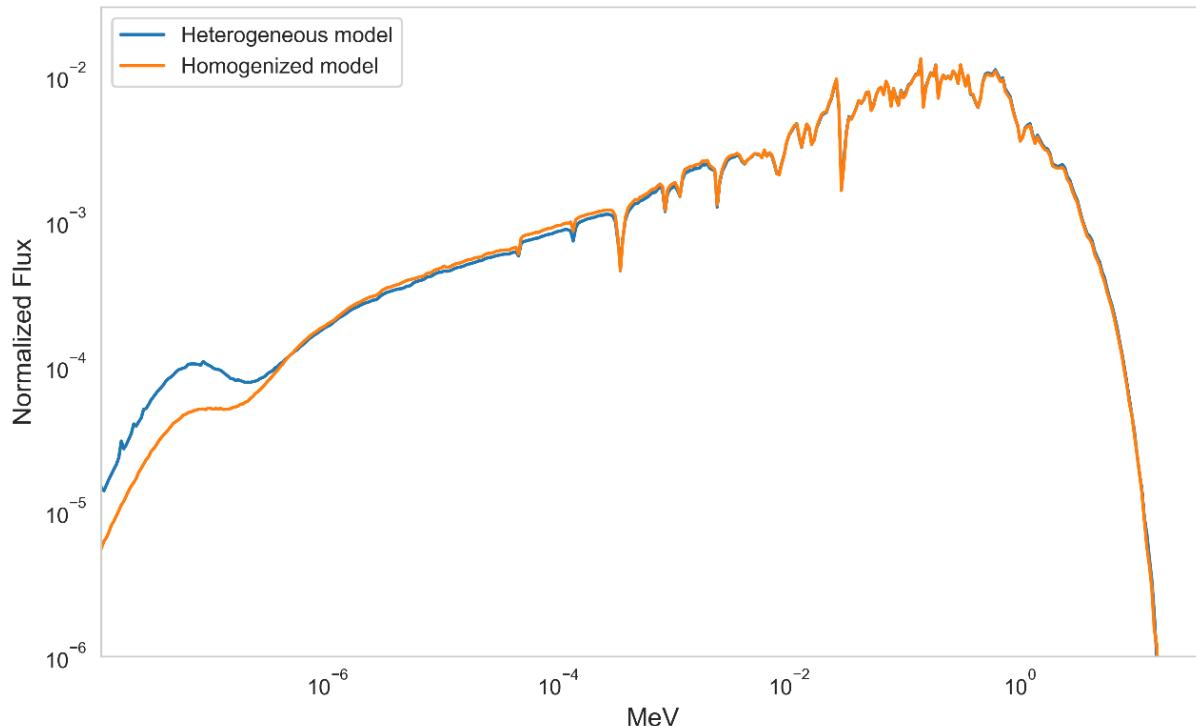
Homogeneous model
(MCNP + OpenMC + Serpent)

RZ model
(Serpent)



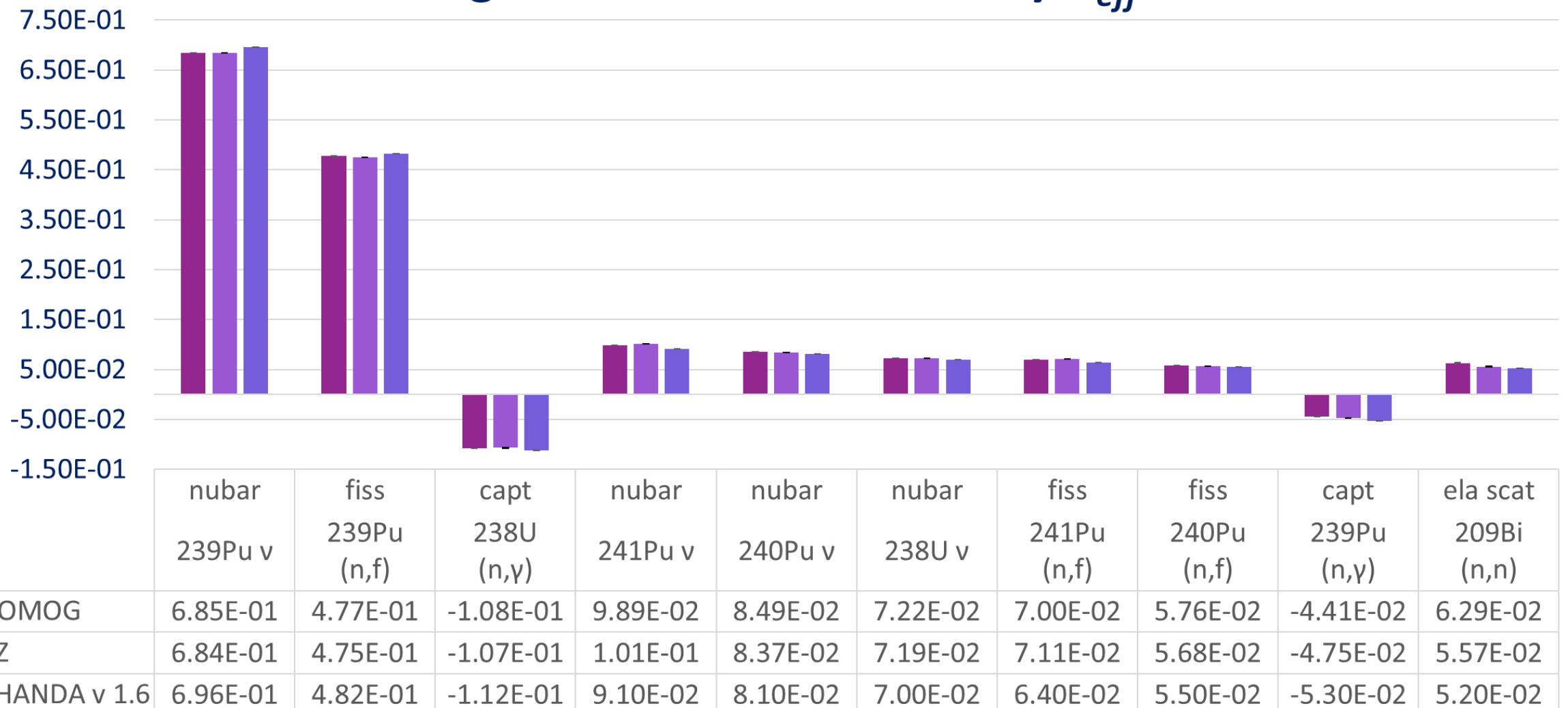
Homogenized critical configuration model

Model	k_{eff}	β_{eff}	Λ_{eff}
Heterogeneous	1.01512 ± 0.00029	$358 \pm 70 \text{ pcm}$	$657 \pm 52 \text{ ns}$
Homogeneous	1.01556 ± 0.00001	$337 \pm 1 \text{ pcm}$	$685 \pm 21 \text{ ns}$
RZ	1.01562 ± 0.00001	$337 \pm 1 \text{ pcm}$	$649 \pm 13 \text{ ns}$



Sensitivity analysis – model comparison

Homog Vs RZ model - Sensitivity K_{eff}

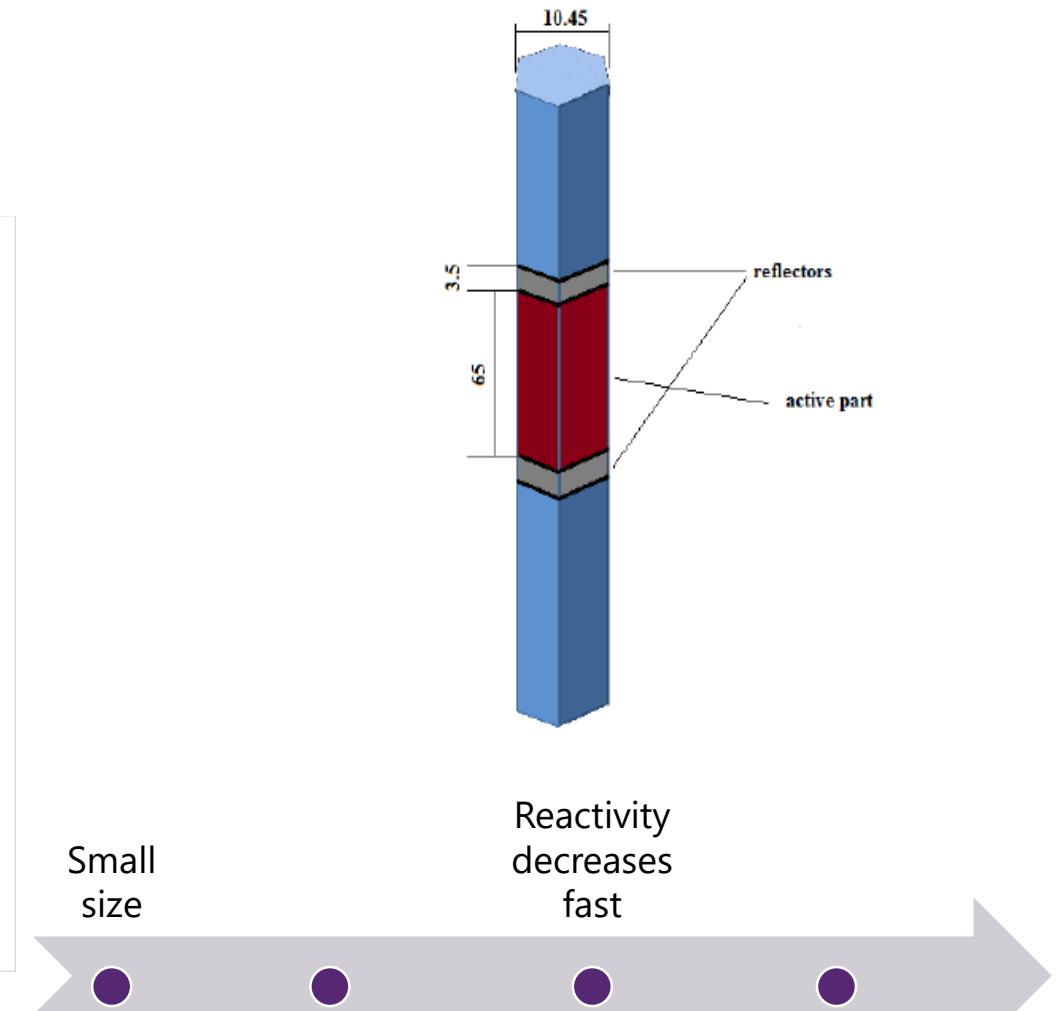
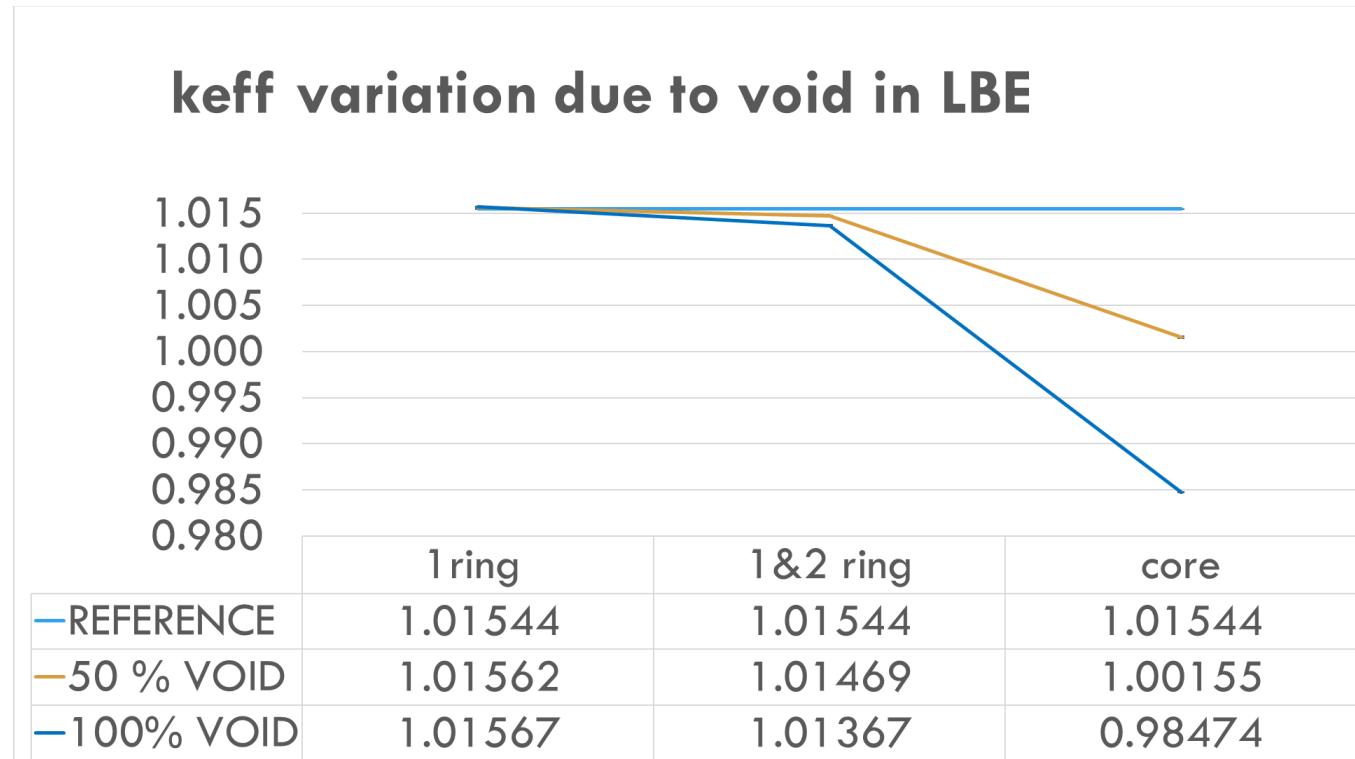


Sensitivity analysis – model comparison

Homog Vs RZ model - Sensitivity β_{eff}



Sensitivity analysis – void coefficient



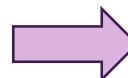
Sensitivity analysis – void coefficient

Isotope	XS	ISC (0% VOID)	std_dev 0% (%)	ISC (100% VOID)	std_dev 100% (%)	Δp [pcm]	$S_{\rho_{1 \rightarrow 2}, \alpha}$	$std_{\rho_{1 \rightarrow 2}, \alpha}$ (%)
^{239}Pu	nubar prompt	6.816E-01	0.19%	6.668E-01	0.04%	-598.803	-1.950E-01	21.03%
^{239}Pu	fission	4.728E-01	0.39%	4.701E-01	0.07%	-1173.501	-3.822E-01	15.70%
^{238}U	capture	-1.068E-01	0.96%	-9.656E-02	0.18%	-715.550	-2.330E-01	13.94%
^{241}Pu	nubar prompt	9.898E-02	0.90%	9.532E-02	0.17%	67.148	2.187E-02	131.45%
^{240}Pu	nubar prompt	8.553E-02	0.91%	8.914E-02	0.15%	-629.147	-2.049E-01	12.53%
^{238}U	nubar prompt	7.123E-02	0.99%	8.495E-02	0.16%	-1612.153	-5.250E-01	4.62%
^{241}Pu	fission	7.070E-02	1.40%	6.801E-02	0.23%	56.831	1.851E-02	172.53%
^{240}Pu	fission	5.855E-02	1.50%	6.180E-02	0.24%	-509.278	-1.659E-01	17.41%
^{239}Pu	capture	-4.432E-02	1.50%	-4.165E-02	0.27%	-135.601	-4.416E-02	48.49%
^{238}U	fission	4.371E-02	1.90%	5.431E-02	0.30%	-1209.936	-3.941E-01	7.13%

Sensitivity analysis – Doppler coefficient

SENSITIVITIES (%/%)					
ISOTOPE	XS	ISC (800 K)	std err (800 K)	ISC _{doppler} (1100 K)	std err (1100 K)
²³⁹ Pu	(n,f)	$4.773 \cdot 10^{-1}$	0.069%	$7.242 \cdot 10^{-3}$	1.300%
²³⁸ U	(n, γ)	$-1.081 \cdot 10^{-1}$	0.160%	$-9.564 \cdot 10^{-3}$	0.480%
²³⁹ Pu	(n, γ)	$-4.414 \cdot 10^{-2}$	0.270%	$-5.560 \cdot 10^{-3}$	1.300%

$$\alpha_{doppler} = \frac{ISC \cdot keff \cdot 10^5 \cdot T_{fuel}}{\Delta T}$$



Source: Heddy Barale, "Application of the SERPENT2 code to neutronic analyses of the MYRRHA core : a sensitivity approach," 2020.

Isotope	Cross section	Doppler coeff (pcm)
²³⁸ U	(n, γ)	-3561
²³⁹ Pu	(n,f)	2697
	(n, γ)	-2070

Sensitivity analysis – Power Peaking Factors

$$P_{max} = \frac{V_{core} \langle \Sigma_p \emptyset \rangle_{max}}{V_{max} \langle \Sigma_p \emptyset \rangle}$$

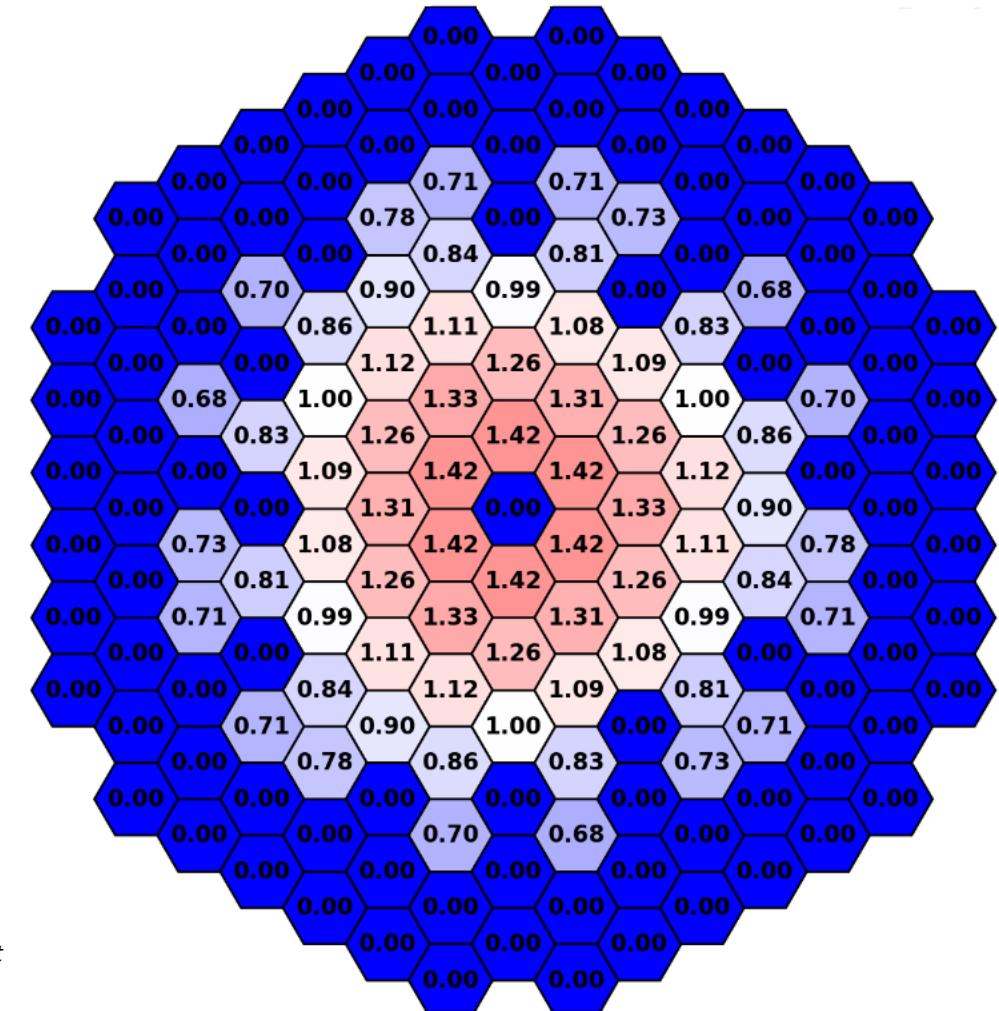
$$\begin{aligned} S_{P_{max}} &= \frac{\sigma}{P_{max}} \frac{dP_{max}}{d\sigma} = \frac{\sigma}{P_{max}} \left\{ \frac{\partial P_{max}}{\partial \sigma} - \langle \Psi^*, \left(\frac{\partial A}{\partial \sigma} - \frac{1}{k} \frac{\partial F}{\partial \sigma} \right) \emptyset \rangle \right\} \\ &= \{S_{P_{max,D}} - S_{P_{max,I}}\} \end{aligned}$$

$$S_{P_{max,D}} = \frac{\sigma}{P_{max}} \left(\frac{(\langle \Sigma_p \emptyset \rangle_{max})_{i,g}}{\langle \Sigma_p \emptyset \rangle_{max}} - \frac{(\langle \Sigma_p \emptyset \rangle)_{i,g,d}}{\langle \Sigma_p \emptyset \rangle} \right)$$

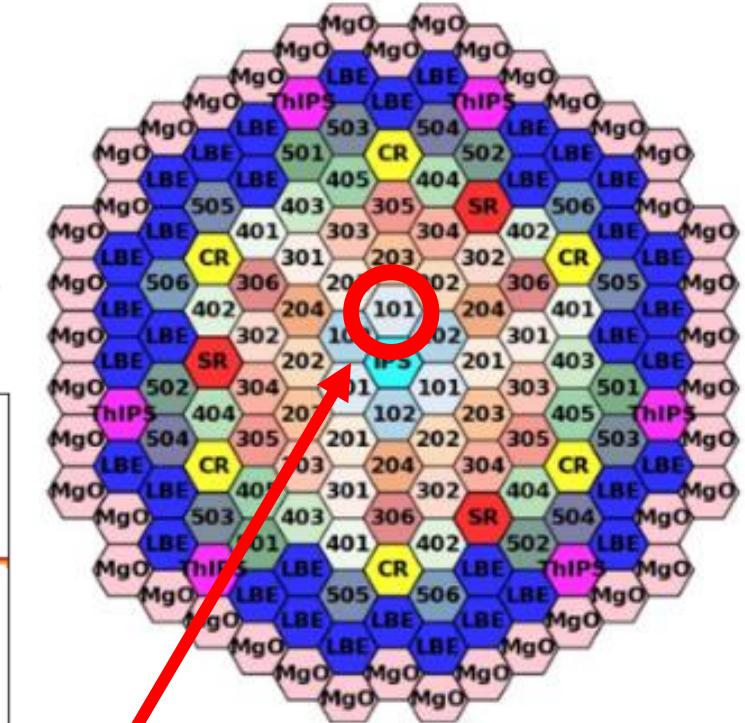
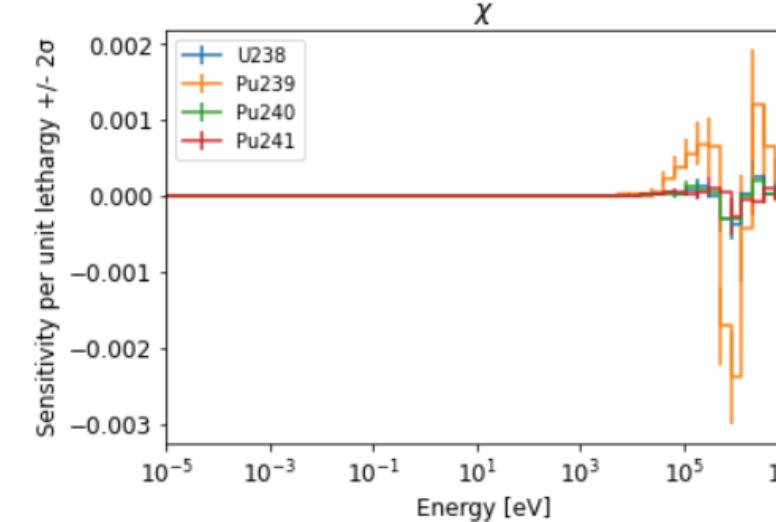
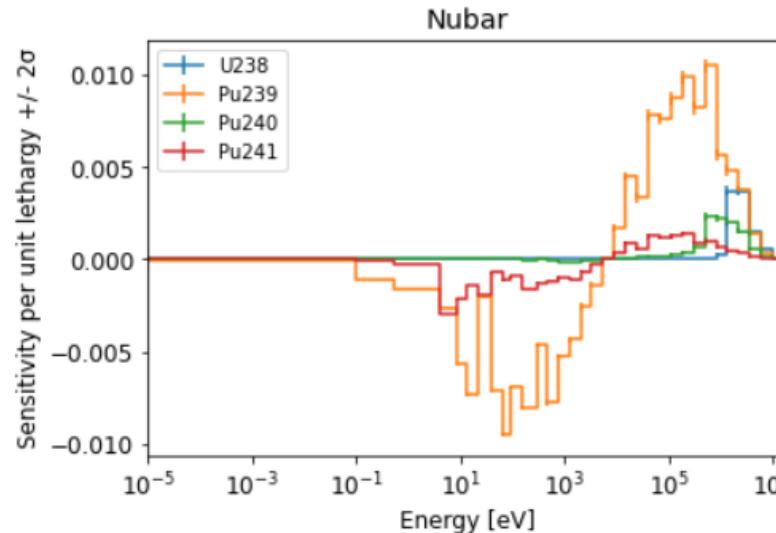
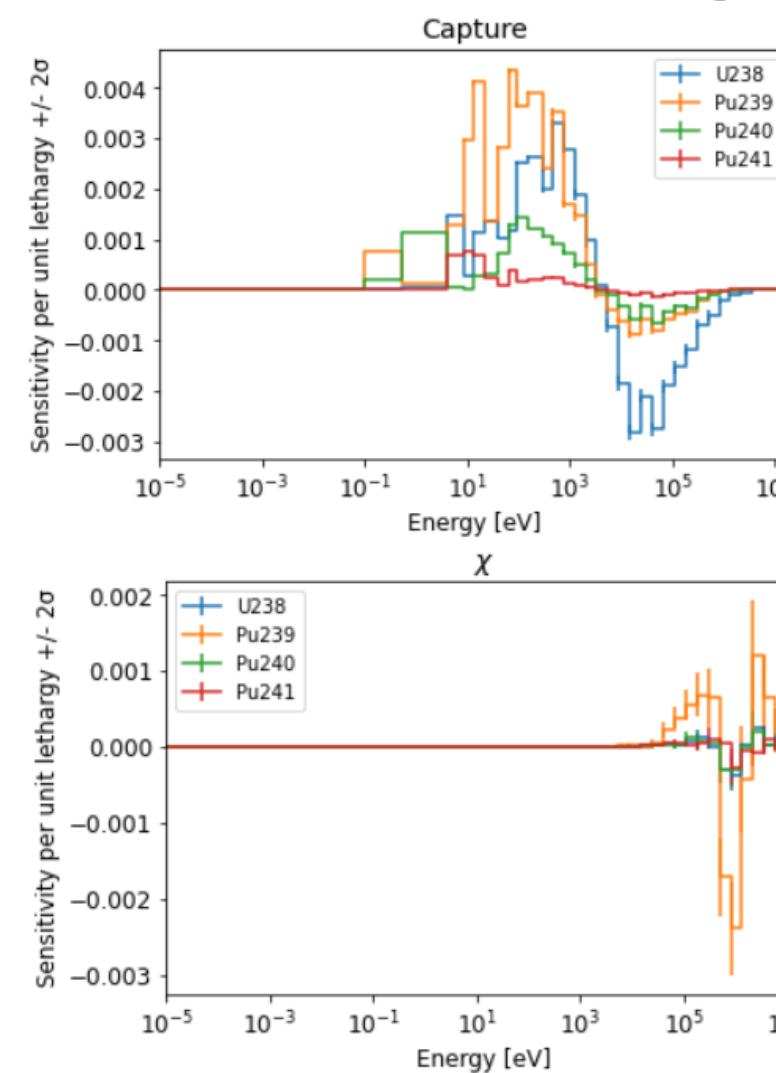
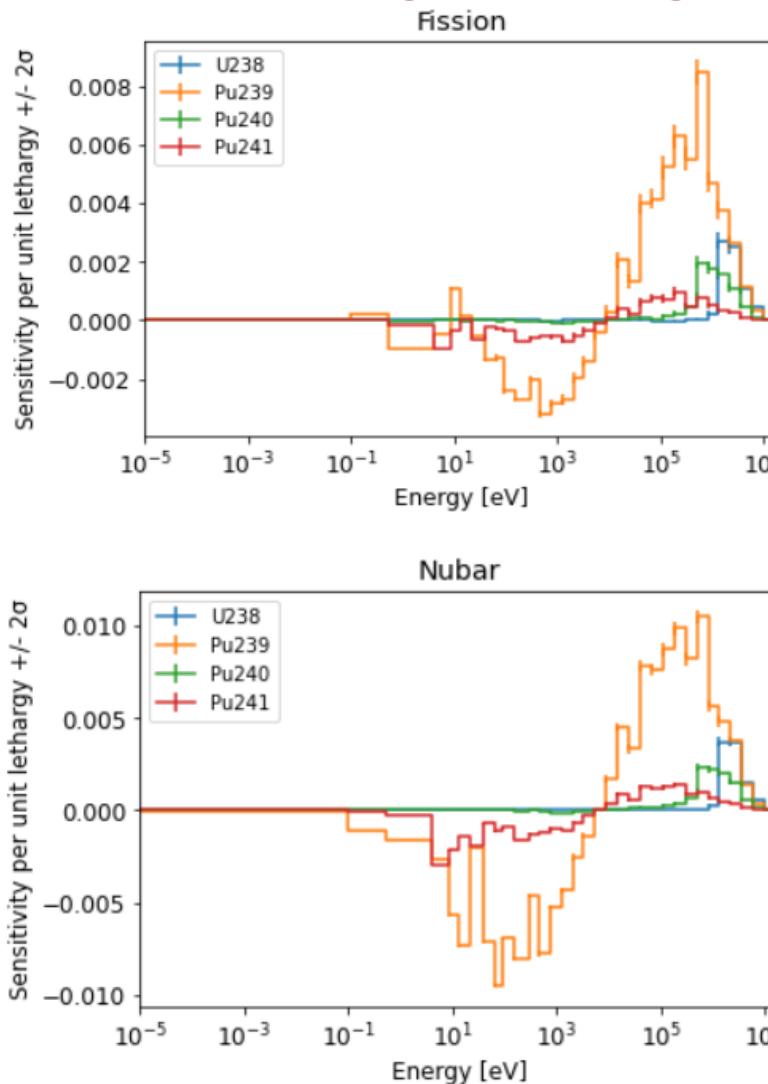
*i=isotope
g=energy group
d=reactor domain*

0

Source: M. Salvatores and R. Jacqmin, *Uncertainty and target accuracy assessment for innovative systems using recent covariance data evaluations*, vol. 26, no. NEA/WPEC-26. 2008.



Sensitivity analysis – Power Peaking Factors



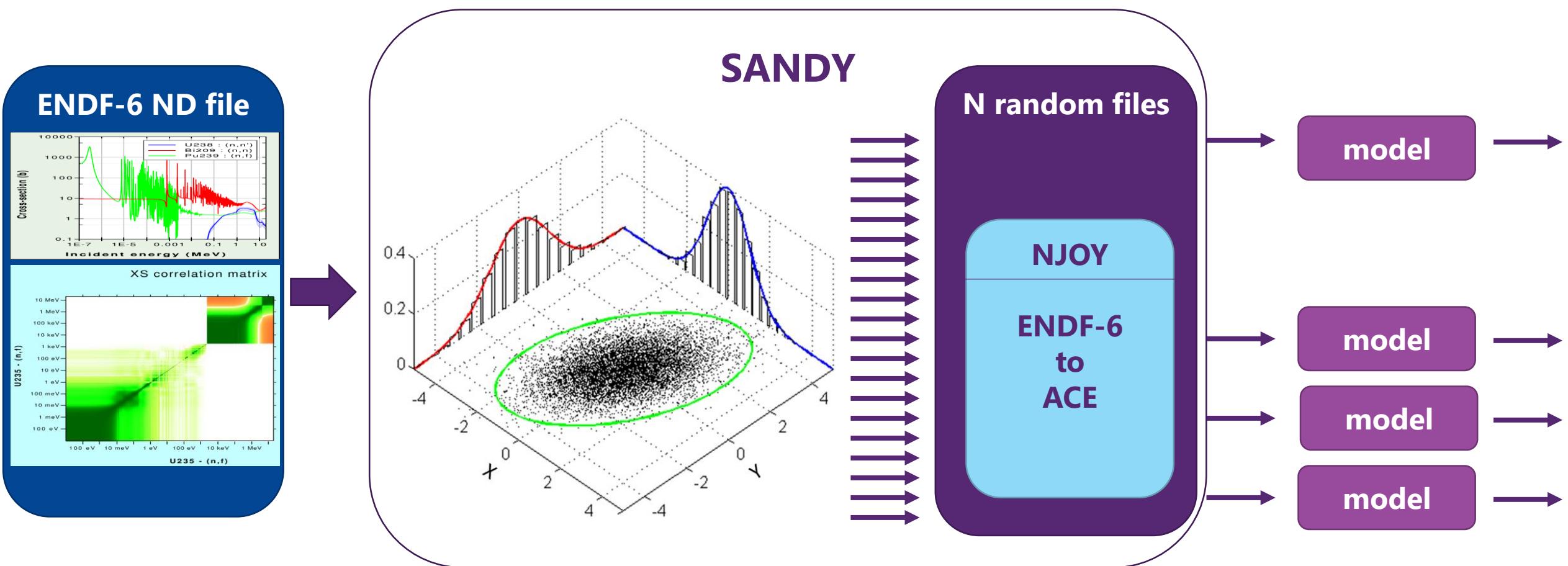
Sensitivity analysis by introducing a perturbation to the effective fission cross section of ^{235}U , ^{239}Pu , ^{240}Pu and ^{241}Pu in fuel batch 101 (highest power peaking value 1.42)

Fuel depletion



ND sampling with SANDY

Covariance-based sampling



Sensitivities

- Local / global sensitivity analysis
 - Perturbation coefficients
 - Energy/reaction-dependent sampling
 - Custom covariance matrix
 - Custom perturbations

$$\boldsymbol{x} \longrightarrow \mathcal{N}_{\boldsymbol{x}}(\boldsymbol{x}_0, \Sigma_x)$$

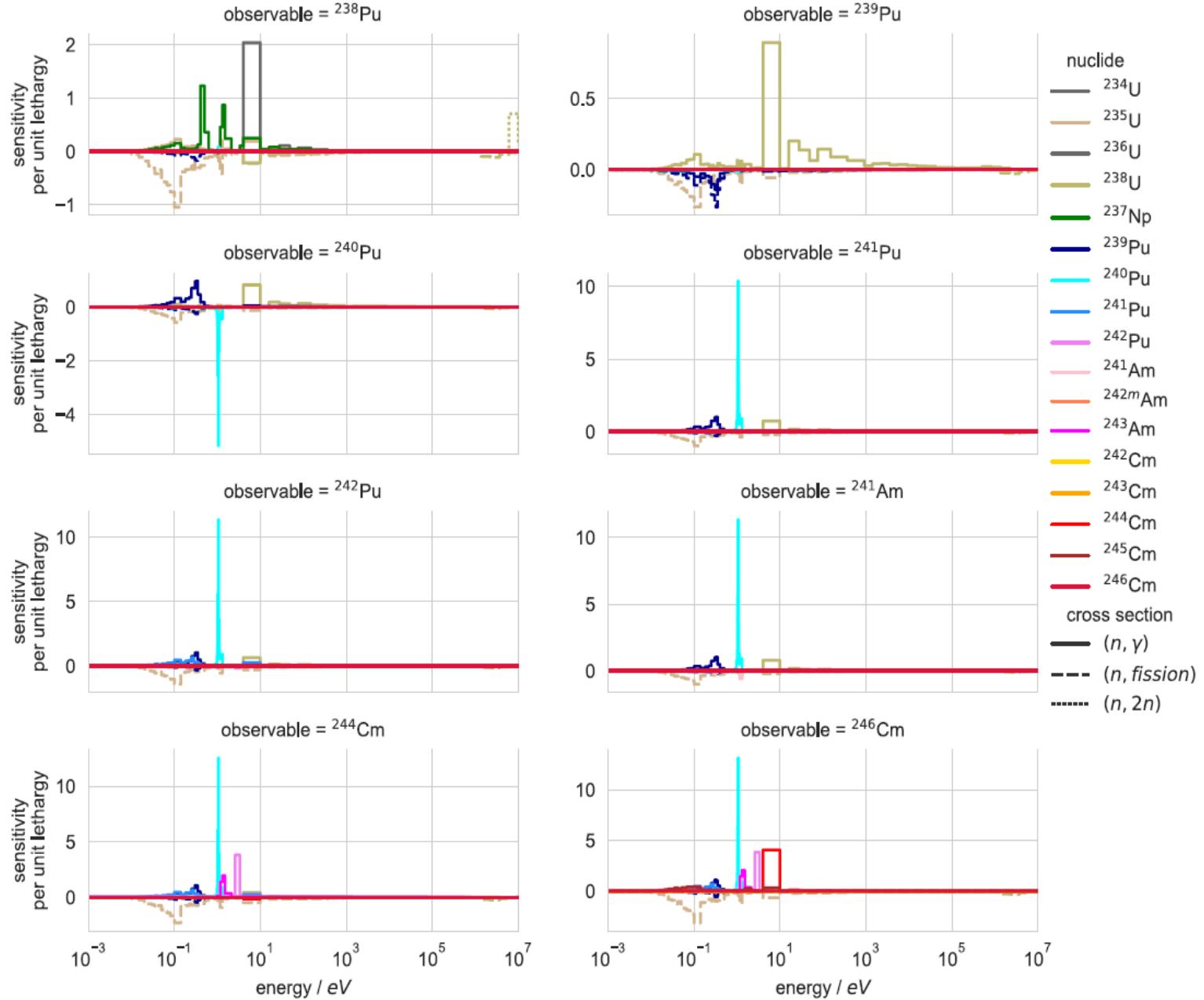
$$\begin{bmatrix} x_1^{(1)} & x_2^{(1)} & \dots & x_M^{(1)} \\ x_1^{(2)} & x_2^{(2)} & \dots & x_M^{(2)} \\ \vdots & \vdots & \ddots & \vdots \\ x_1^{(N)} & x_2^{(N)} & \dots & x_M^{(N)} \end{bmatrix} \rightarrow \boxed{\text{model}} \rightarrow \begin{bmatrix} y^{(1)} \\ y^{(2)} \\ \vdots \\ y^{(N)} \end{bmatrix}$$

$$\mathbf{y} = \mathbf{X}\boldsymbol{\beta} + \boldsymbol{\epsilon} \quad \hat{\boldsymbol{\beta}} = (\mathbf{X}^T \mathbf{X})^{-1} \mathbf{X}^T \mathbf{y}$$

Source: L. Fiorito *et al.* On the use of criticality and depletion benchmarks for verification of nuclear data. Annals of Nuclear Energy 161 (2021) 108415

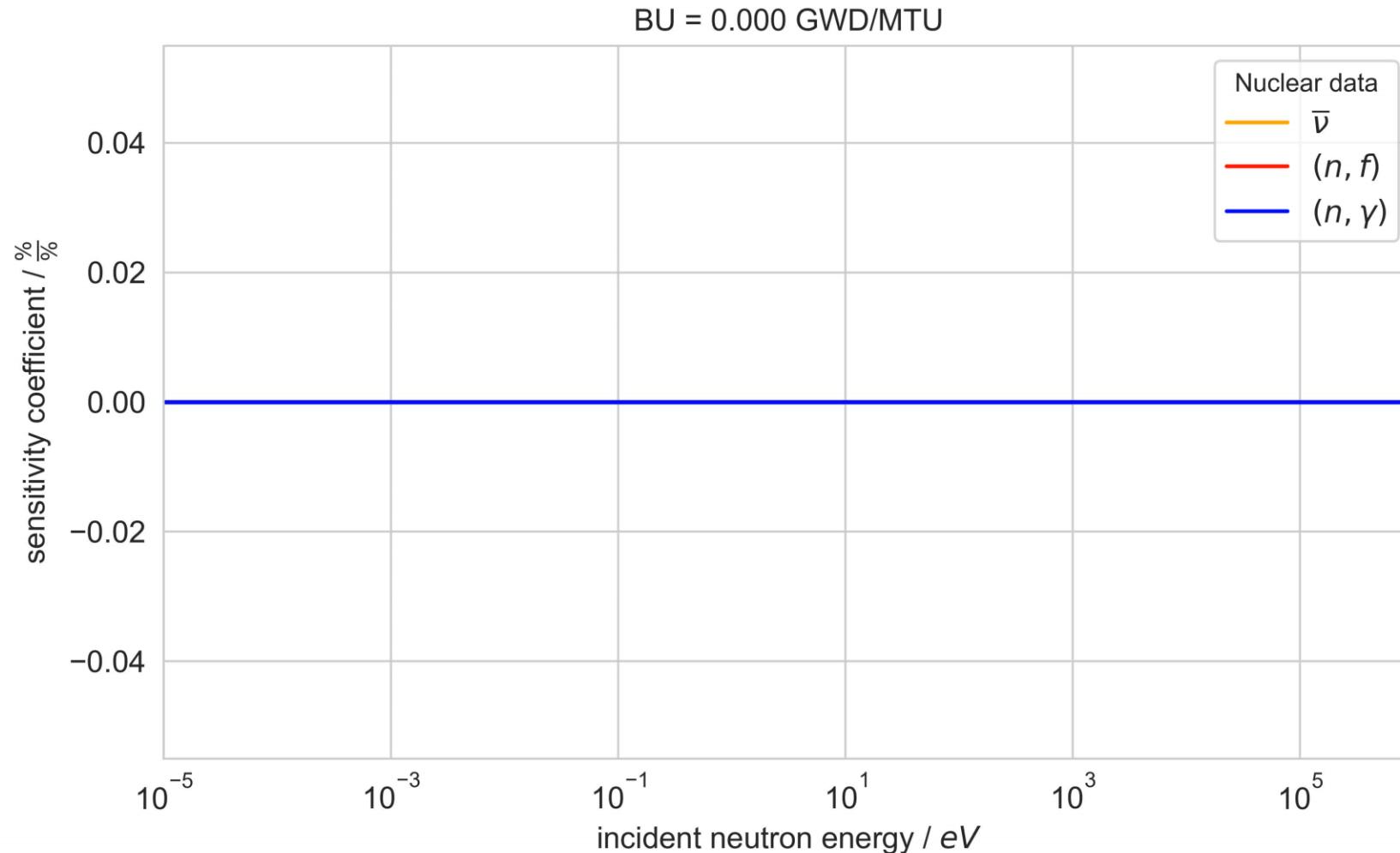
Sensitivities

- 10 GWd/MTU



Source: L. Fiorito *et al.* On the use of criticality and depletion benchmarks for verification of nuclear data. Annals of Nuclear Energy 161 (2021) 108415

Sensitivities



Acknowledgements

The research leading to these results has received funding from the European Union's Horizon 2020 research and innovation programme, Euratom research and training programme 2014-2018 under grant agreements No. 847552 (SANDA project) and No. 847593 (EURAD project)

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Registered Office:

Avenue Herrmann-Debrouxlaan 40 - 1160 BRUSSELS - Belgium

Research Centres:

Boeretang 200 - 2400 MOL - Belgium
Chemin du Cyclotron 6 - 1348 Ottignies-Louvain-la-Neuve - Belgium