

Application of EGPT in the analysis of small-sample reactivity worth experiments

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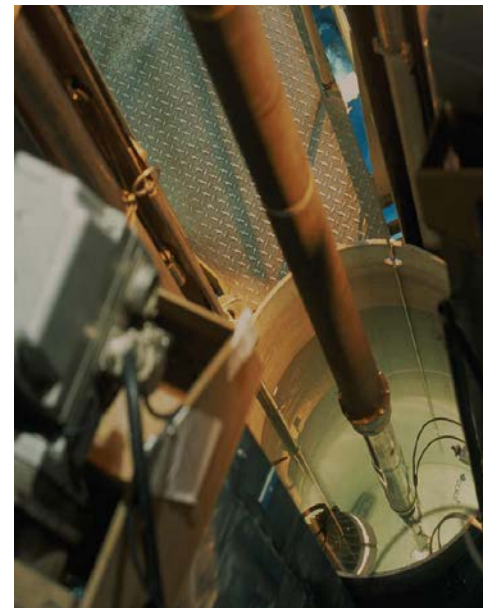
16/05/2017, OECD/NEA, WPEC/SG39.

OUTLINE

- Introduction
- Selected experiments
- Analysis methodology
- Application to ^{103}Rh capture
- Conclusions and perspectives

■ **Specificities of *small-sample reactivity worth* (SSRW) experiments with respect to other kinds of RW experiments (void coefficient, doppler, absorber efficiency...)**

- Small in terms of geometrical size ($\varnothing \approx 1\text{cm}$. $L \approx 10\text{cm}$)
⇒ Low sensitivity to flux gradients
- Small in terms of reactivity worth (1-10 pcm)
⇒ No influence on the global production of neutrons in a critical assembly (<0.1%)
- Limited number of isotopes / elements
- Under special spectral conditions, possibility to emphasis one type of reaction (capture, scattering)



⇒ In suitable conditions, SSRW can be related to limited number of parameters that make such experiments relevant for nuclear data improvement

■ **Computing SSRW can be a tricky issue**

$$\Delta\rho = \frac{k_2 - k_1}{k_2 k_1}$$

⇒ The more k_1 is close to k_2 , the higher convergence criteria must be required

■ **Moreover, SSRW is often the first step before computing sensitivity coefficients for nuclear data analysis / feedback**

$$S(\Delta\rho) = \frac{1}{\Delta\rho} \left(\frac{\delta\rho_2}{\frac{\delta\sigma_i}{\sigma_i}} - \frac{\delta\rho_1}{\frac{\delta\sigma_i}{\sigma_i}} \right) = \frac{S(\rho_2) - S(\rho_1)}{\Delta\rho}$$

⇒ In addition to the computation limits of $\Delta\rho$ in case of small RW, sensitivities to reactivities ρ can be several orders of magnitude higher than $\Delta\rho$

⇒ Potential issues of « zero / zero »

Various methods for calculating SSRW experiments

Methods for SSRW calculation	Deterministic code	Probabilistic code
Eigen-value difference (EV)	+ Easy to implement/use - Model simplifications (energy, geometry, leakage model...) - Numerical convergence issues	+ Exact method - Huge computation time
Standard perturbation theory (SPT)	+ (Almost) no convergence issues ($\Delta\phi \Rightarrow \Delta\sigma$) - Not implemented in every code (sometimes, only 1st order SPT)	+ Best method in case of exact SPT - Mostly 1st order SPT - Convergence issues with scattering effects

⇒ Recent implementation of IFP-based perturbation methods in Monte-Carlo codes (TRIPOLI, SERPENT, MCNP...) is a huge improvement for an accurate calculation of SSRW

What about the sensitivity analysis of SSRW?

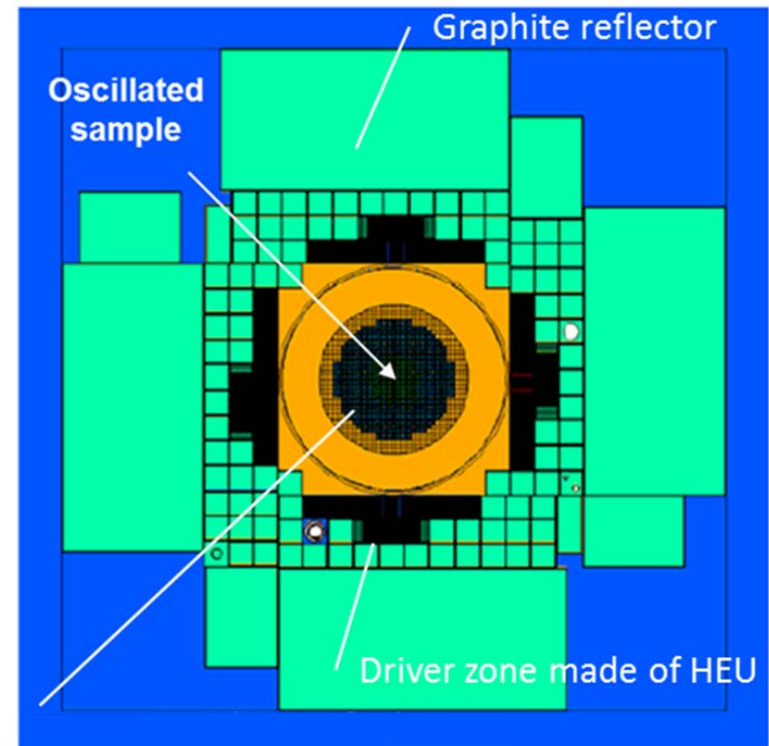
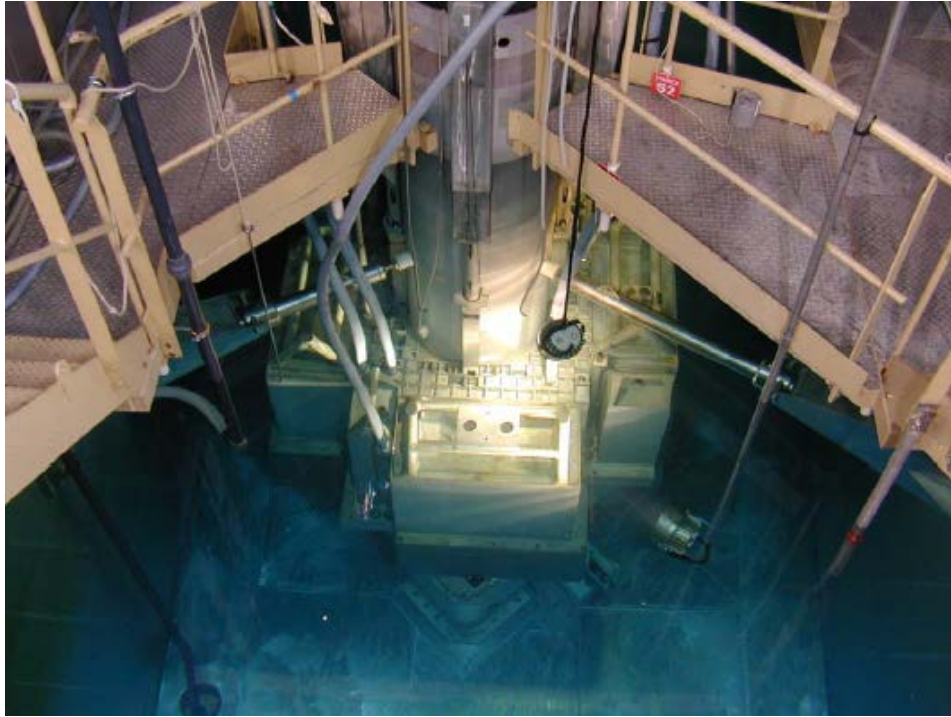
Methods for sensitivity analysis of SSRW	Deterministic code	Probabilistic code
Equivalent Generalized Perturbation Theory (EGPT)	+ All sensitivity vectors available in a single calculation - Numerical convergence issues linked to the computation of $\Delta\rho$ and $\Delta S(\rho)$	- Convergence issues due to the difference of two sensitivity computations
Direct Perturbation (DP)	+ Easy to implement/use + Can be applied at several stages (ENDF files, micro-lib, macro-lib...) - Required home-made scripts to perturbate the data	- Convergence issues - No available methods for doing « perturbations of perturbations »

⇒ Reliability of the EGPT method in the analysis of SSRW experiments?

See P. Ros et al., « A revision of sensitivity analysis for small reactivity effects in ZPRs », Proc. Of ICAPP, avril 2017 conference, Kyoto, Japan

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MINERVE Characteristics

- Pool-type reactor (100W max)
- Light Water at ambient temperature
- Reflector: large graphite blocks
- Driver zone: MTR elements (UAl plates, >90% ^{235}U)
- Test zone: thermal or fast spectrum configurations

Validation of nuclear on a large range of materials used in GEN-II/GEN-III reactor cores

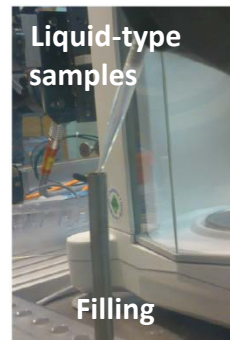
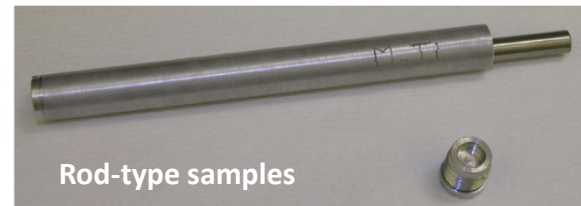
More than 60 samples :

- Moderating materials: H_2O , $^{\text{nat}}\text{Be}$, $^{\text{nat}}\text{C}$, CH_2
- Structural materials: $^{\text{nat}}\text{Mg}$, $^{\text{nat}}\text{Al}$, $^{\text{nat}}\text{Cl}$, $^{\text{nat}}\text{Ca}$, $^{\text{nat}}\text{Ti}$, $^{\text{nat}}\text{Cr}$, $^{\text{nat}}\text{Fe}$,
 $^{\text{nat}}\text{Ni}$, $^{\text{nat}}\text{Cu}$, $^{\text{nat}}\text{Zn}$, $^{\text{nat}}\text{Zr}$, $^{\text{nat}}\text{Mo}$, $^{\text{nat}}\text{Sn}$
- Detection materials: $^{\text{nat}}\text{V}$, $^{\text{nat}}\text{Mn}$, $^{\text{nat}}\text{Co}$, $^{\text{nat}}\text{Nb}$, $^{\text{nat}}\text{Rh}$
- Absorbing materials: $^{\text{nat}}\text{Ag}$, $^{\text{nat}}\text{In}$, $^{\text{nat}}\text{Cd}$, $^{\text{nat}}\text{Eu}$, $^{\text{nat}}\text{Gd}$, $^{\text{nat}}\text{Dy}$, $^{\text{nat}}\text{Er}$, $^{\text{nat}}\text{Hf}$
 ^{153}Eu , ^{107}Ag , $^{\text{nat}}\text{Cs}$
- Industrial alloys: Zy4 , M5 , SS304 , SS316 , Inconel-800
- Calibration materials: $^{\text{nat}}\text{Au}$, ^6Li , ^{10}B

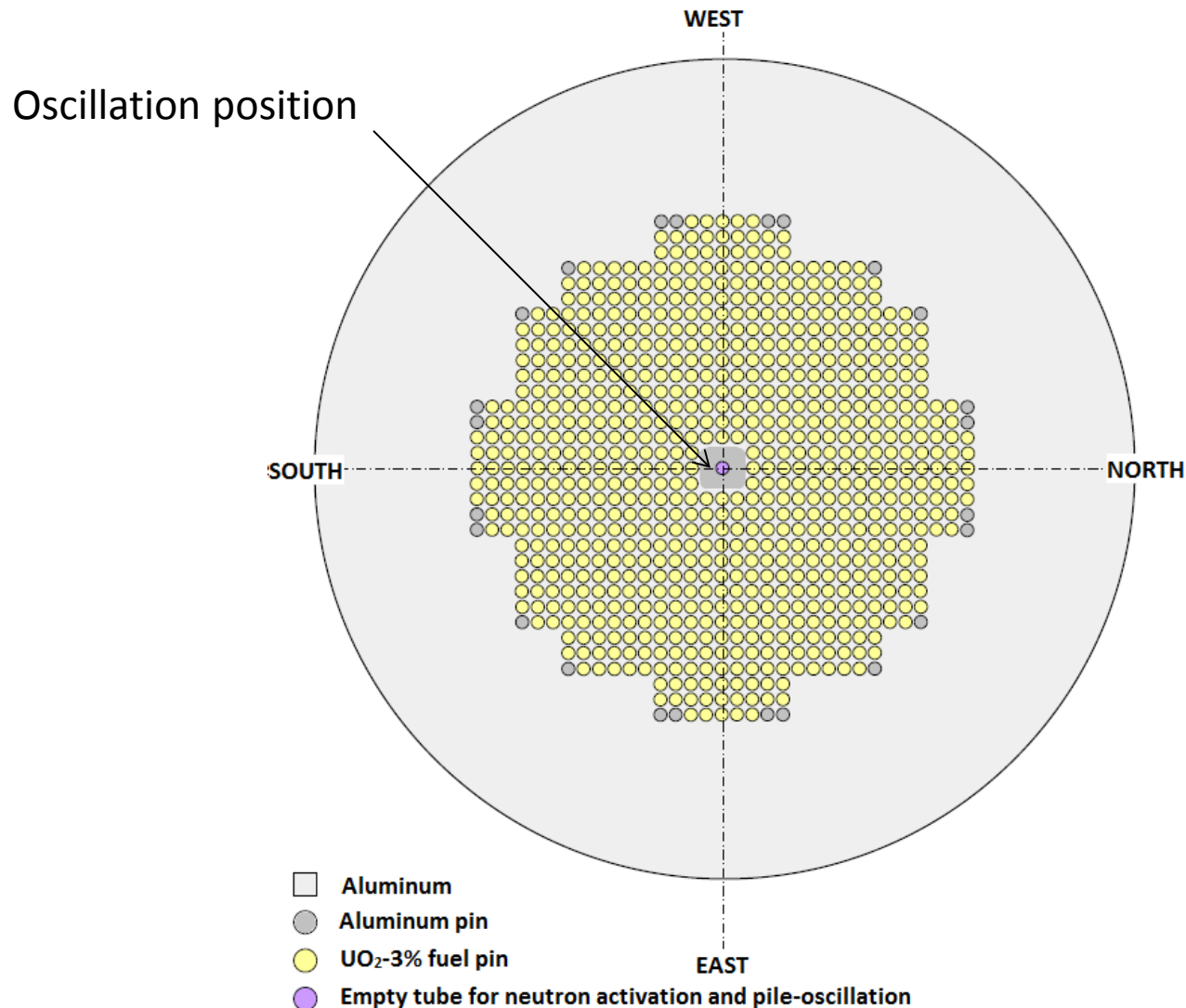
■ Both pile oscillation and neutron activation experiments

■ 10-30cm long tubes filled with materials of different physical forms

- Pure rods
- Liquid solutions
- Powder mixed with Al_2O_3 diluant



The MAESTRO core configuration



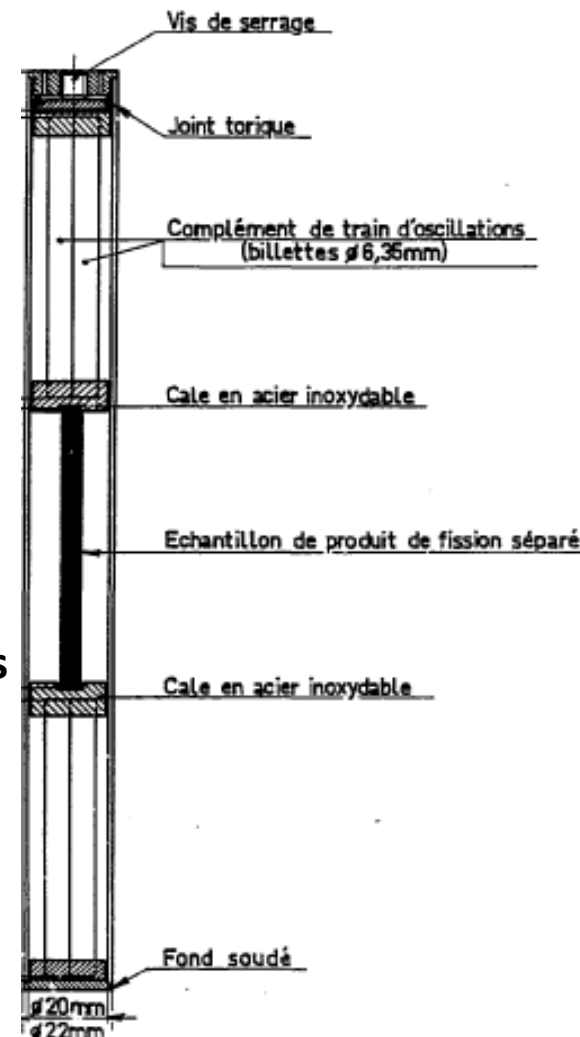
Validation of the integral capture of fission products in SCFR in support to SUPER-PHENIX

Various kinds of samples in 3-10cm long tubes:

- Individual fission products: ^{141}Pr , ^{133}Cs , ^{99}Tc , ^{103}Rh , ^{98}Mo , ^{100}Mo , ^{104}Ru , ^{108}Pd , ^{142}Ce , ^{146}Nd , ^{148}Nd , ^{150}Nd , ^{152}Nd
- Irradiated fuel pins from PHENIX and RAPSODIE

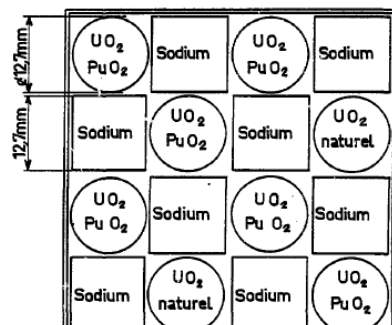
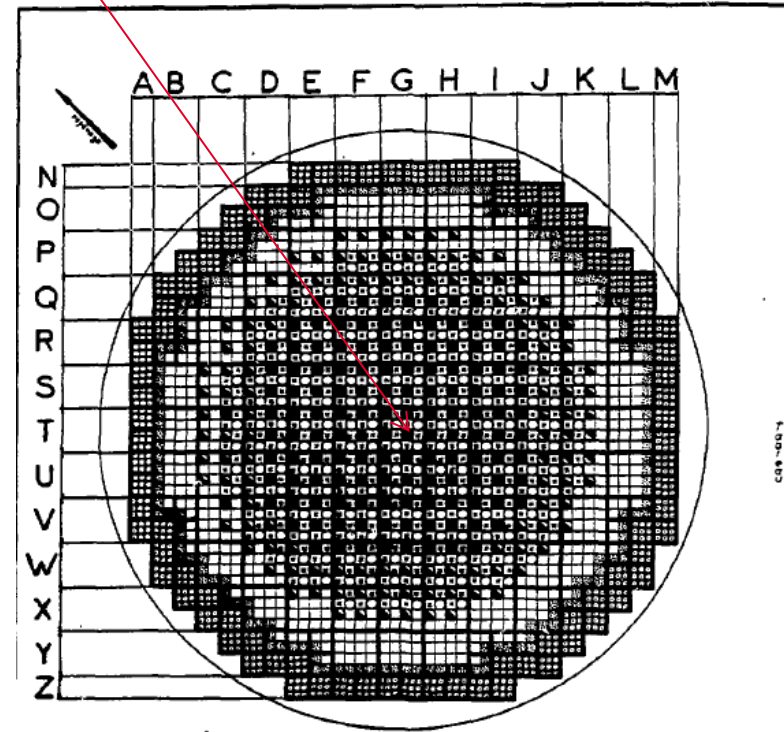
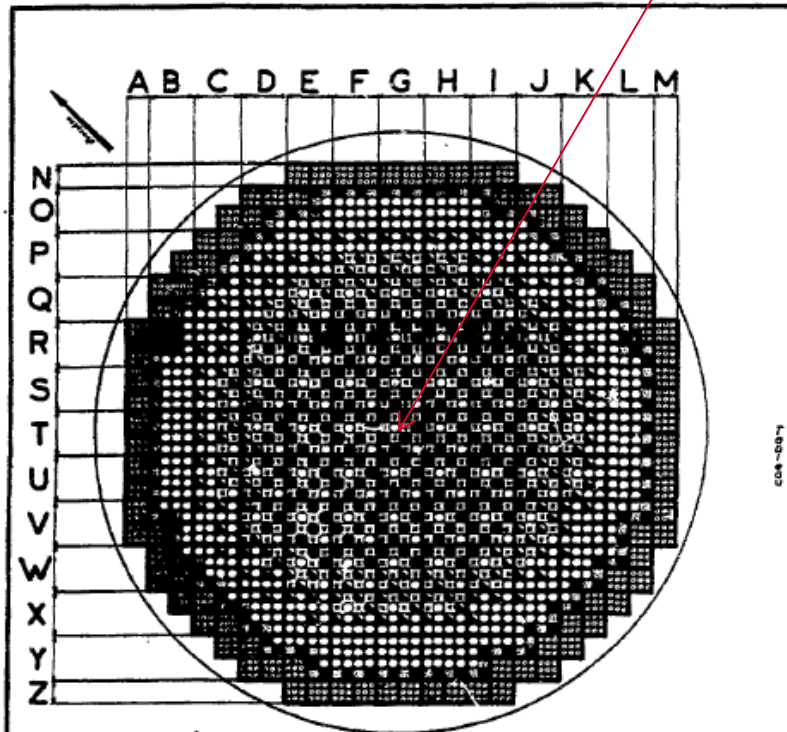
Both pile oscillation and neutron activation experiments

In parallel of the PROFIL and PROFIL-2 irradiation experiments in PHENIX



The ERMINE-5 experiment (1974-1979)

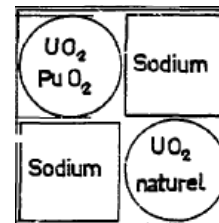
Oscillation position



- UO₂ - PuO₂ "Mix VI" . 12.7
- UO₂ enrichi à 23 % . 12.7
- UO₂ naturel . 12.7
- Sodium . 12.7
- U appauvri métal . 12.7
- Poudre graphite + bore . 11
- UO₂ enrichi à 3.5 % . 8

ZONA 1

Harder spectrum



Legend

- UO₂ - PuO₂ "Mix VI" . 12.7
- UO₂ enrichi à 23 % . 12.7
- UO₂ naturel . 12.7
- Sodium . 12.7
- UO₂ appauvri . 12.7
- U appauvri métal . 12.7
- UO₂ enrichi à 3.5 % . 8

ZONA 3

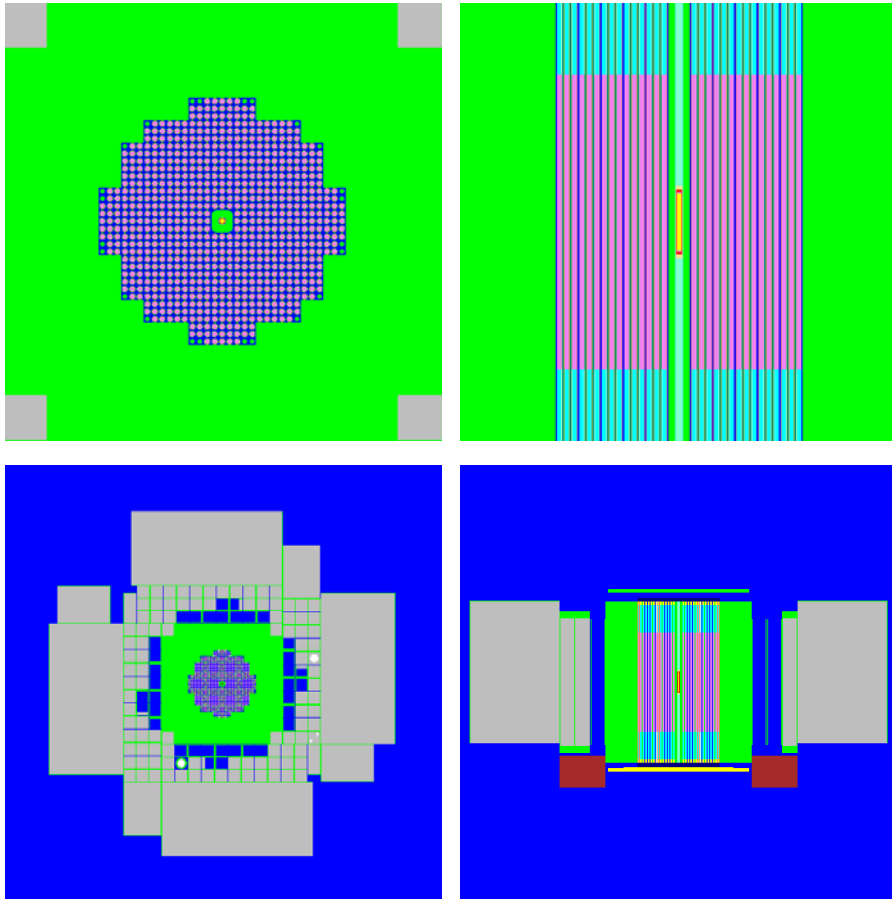
Softer spectrum

OUTLINE

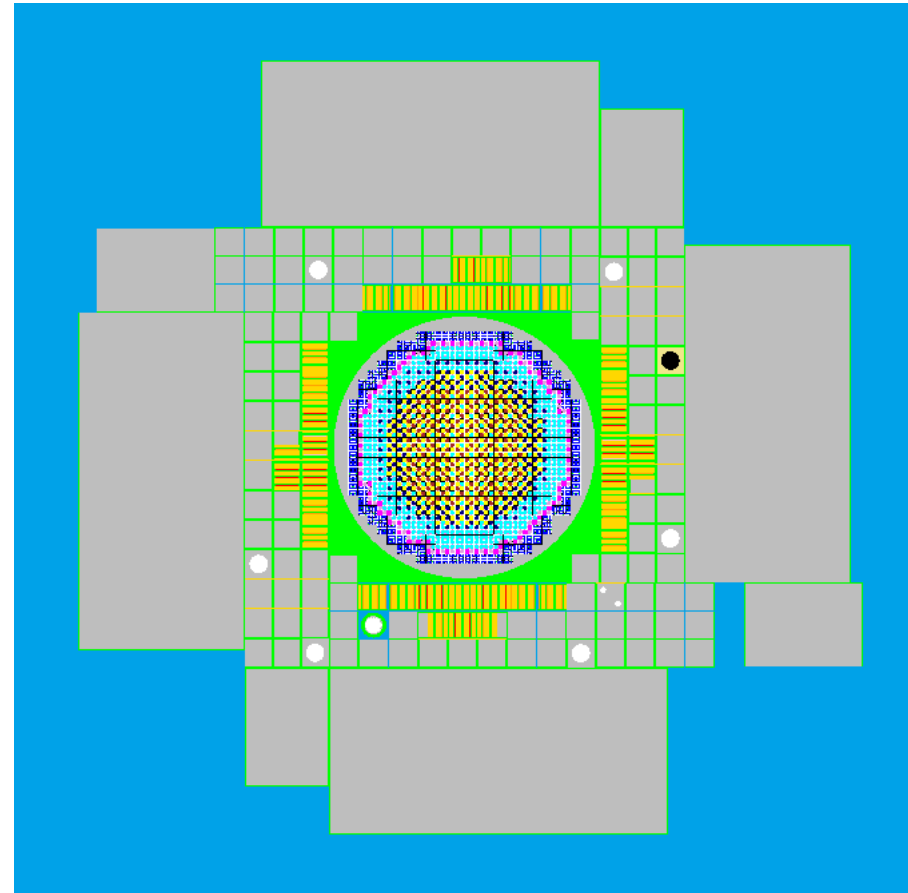
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TRIPOLI-4 modeling

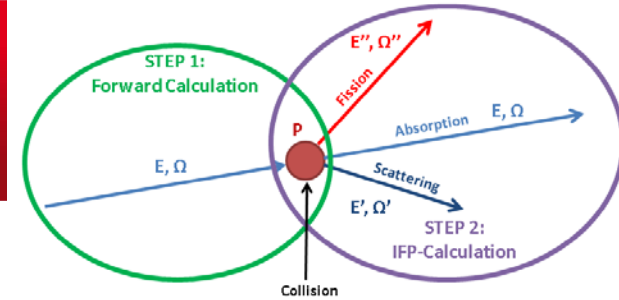
MAESTRO core



ERMINE-V / ZONA 1 core



Computation of SSRW



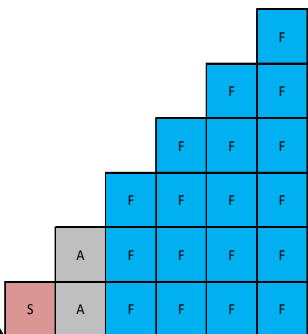
Exact SPT method in TRIPOLI-4

- Continuous energy forward flux calculation + collision locus storage
 - Continuous energy adjoint flux calculation for each stored collision
 - Computation of the reactivity worth with various collapsing options
- ⇒ **$10^3 - 10^4$ h.CPU per sample**

Computation of sensitivity coefficients to SSRW

Computation of sensitivities with deterministic methods

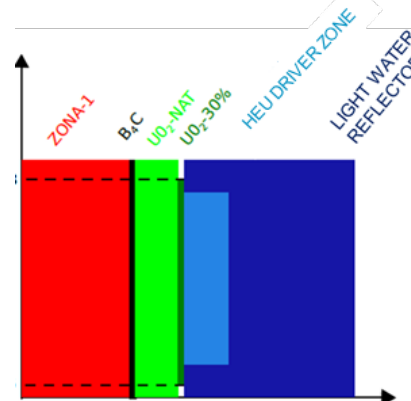
APOLLO-2.8



- 2D/XY 13x13 lattice
- Critical buckling
- 281g self-shielding
- P_{ij} -multicell method
- SPT computation for sensitivity to reactivity

⇒ **2 min per sample**

ERANOS-2.3



- 2D/RZ full core model
- 1968g XS self-shielding
- Collapsing to 33g
- S_n method (BISTRO)
- EGPT computation for sensitivity to RW

⇒ **10 min per sample**

EGPT method vs Direct Perturbation method

■ DP method

- 1 nominal RW calculation
- 1 RW calculation with modified XS

■ EGPT method

- 1 sensitivity calculation (fine mesh = 281G) for the unperturbed reactivity $S(\rho_1)$
- 1 sensitivity calculation (fine mesh = 281G) for the perturbed reactivity $S(\rho_2)$
- Computation of sensitivity coefficients by $S(\Delta\rho) = (S(\rho_2) - S(\rho_1)) / \Delta\rho$ in MATLAB
- Collapsing on various possible meshes (15, 26, 33...)

■ Application on $\Delta\rho_{Rh}$ in the MAESTRO experiment

Sensitivity method	1-group sensitivity coefficient (%/%)		
	Rh capture	^{235}U Nu_tot	^1H elastic scat.
EGPT	0.918	-0.855	-0.738
DP	0.930	-0.870	-0.834

⇒ The EGPT is consistent with the direct perturbation method

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Calculation / Experiment comparison

Experiment	C/E-1 TRIPOLI-4DEV + JEFF-3.2
MAESTRO	$1.4\% \pm 1.4\%$
ERMINE-V/ZONA1	$-5.5 \pm 1.5\%$
ERMINE-V/ZONA3	$0.2 \pm 1.5\%$

Preliminary

- ERMINE-V $\Rightarrow$ only measurement uncert + MC convergence
- In the current analysis, an arbitrary 3% uncertainty will be added to account for technological uncertainty (fuel composition, density, dimensions...)

EGPT on ^{103}Rh RW – MAESTRO experimentSensitivity coefficients (%/%) on $\Delta\rho_{\text{Rh}}$

	CAPT	FISS	EL+INEL	NU	SUM
Rh103	0.902		-0.001		0.901
H1	0.014		-0.738		-0.724
O16	0.003		-0.010		-0.007
Al27	-0.031		0.005		-0.026
U235	0.067	-0.532	~0	-0.818	-1.283
U238	0.172	-0.104	-0.002	-0.127	-0.061

⇒ Large indirect effects due nuclear data influencing either:

- the number of neutrons at thermal energy: $^1\text{H}(n,\text{el})$, $^{235}\text{U}(n,\text{f})$, $^{238}\text{U}(n,\gamma)$
- the integral fission rate over the reactor core: $^{235,238}\text{U}(\nu)$, $^{235,238}\text{U}(n,\text{f})$

EGPT on ^{103}Rh RW : not the relevant indicator

- In most cases, reactivity worth are normalized to reference samples to cancel many sources of uncertainties on the evaluation of the fission integral:
 - Nuclear data
 - Core technological uncertainties (fuel enrichment, impurities, clad dimensions, lattice pitch...)
- So the EGPT should not be applied on single RW but on ratio of RW

$$S(\Delta\rho) = \frac{1}{\Delta\rho} \left(\frac{\delta\rho_2}{\frac{\delta\sigma_i}{\sigma_i}} - \frac{\delta\rho_1}{\frac{\delta\sigma_i}{\sigma_i}} \right)$$

$$S(\Delta\rho_{ref}) = \frac{1}{\Delta\rho} \left(\frac{\delta\rho_{ref,2}}{\frac{\delta\sigma_i}{\sigma_i}} - \frac{\delta\rho_{ref,1}}{\frac{\delta\sigma_i}{\sigma_i}} \right)$$

$$S\left(\frac{\Delta\rho}{\Delta\rho_{ref}}\right) = \frac{\delta\left(\frac{\Delta\rho}{\Delta\rho_{ref}}\right)}{\delta\sigma_i/\sigma_i} = S(\Delta\rho) - S(\Delta\rho_{ref})$$

Generalization with n reference samples

$$S\left(\frac{\Delta\rho}{\Delta\rho_{ref}}\right) = S(\Delta\rho) - \sum_{i=1}^n S(\Delta\rho_{ref,i}) \frac{\Delta\rho_{ref,i}}{\sum_j^n \Delta\rho_{ref,j}}$$

EGPT on individual RW – MAESTRO experiment

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{Rh}}$

	CAPT	FISS	EL+INEL	NU	SUM
Rh103	0.902		-0.001		0.901
H1	0.014		-0.738		-0.724
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U238	0.172	-0.104	-0.002	-0.127	-0.061

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{Li6}}$

	CAPT	FISS	EL+INEL	NU	SUM
Li6	0.892				0.892
H1	0.049		-0.460		-0.411
O16	0.003		-0.011		-0.008
Al27	-0.052		0.003		-0.049
U235	0.050	-0.718	~0	-0.858	-1.526
U238	0.192	-0.112	-0.003	-0.138	-0.061

EGPT on ratio of RW – MAESTRO experiment

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{Rh}} / \Delta\rho_{\text{Li6}}$

	CAPT	FISS	EL+INEL	NU	SUM
Rh103	0.902				0.902
Li6	-0.892				-0.892
H1	-0.035		-0.278		-0.313
O16	0.003		-0.011		-0.008
Al27	-0.052		0.003		-0.049
U235	0.017	-0.186	~0	-0.040	0.243
U238	-0.020	-0.008	~0	-0.011	0.000

EGPT on individual RW – ERMINE-V/ZONA3 experiment

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{Rh}}$

	CAPT	FISS	EL	INEL	NU	SUM
U235	-0.006	0.023	0.000	0.000	0.040	0.057
U238	-0.408	0.127	0.069	-0.013	0.205	-0.018
Pu239	-0.099	0.533	0.007	0.000	0.827	1.268
Pu240	-0.031	0.034	0.002	0.000	0.050	0.056
Pu241	-0.010	0.092	0.001	0.000	0.143	0.225
O16	-0.005		0.143	-0.001		0.138
Na23	-0.004		0.081	-0.001		0.075
Rh103	0.874		0.010	0.110		0.995

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{U235}}$

	CAPT	FISS	EL	INEL	NU	SUM
U235	-0.168	1.193	0.000	-0.019	1.798	2.804
U238	-0.236	0.184	0.063	-0.039	0.292	0.266
Pu239	-0.032	0.369	0.006	-0.001	0.597	0.940
Pu240	-0.011	0.045	0.002	0.000	0.066	0.101
Pu241	-0.005	0.043	0.001	0.000	0.075	0.113
O16	-0.006		0.123	-0.001		0.116
Na23	-0.002		0.072	-0.005		0.064
Rh103	0.000		0.000	0.000		0.000

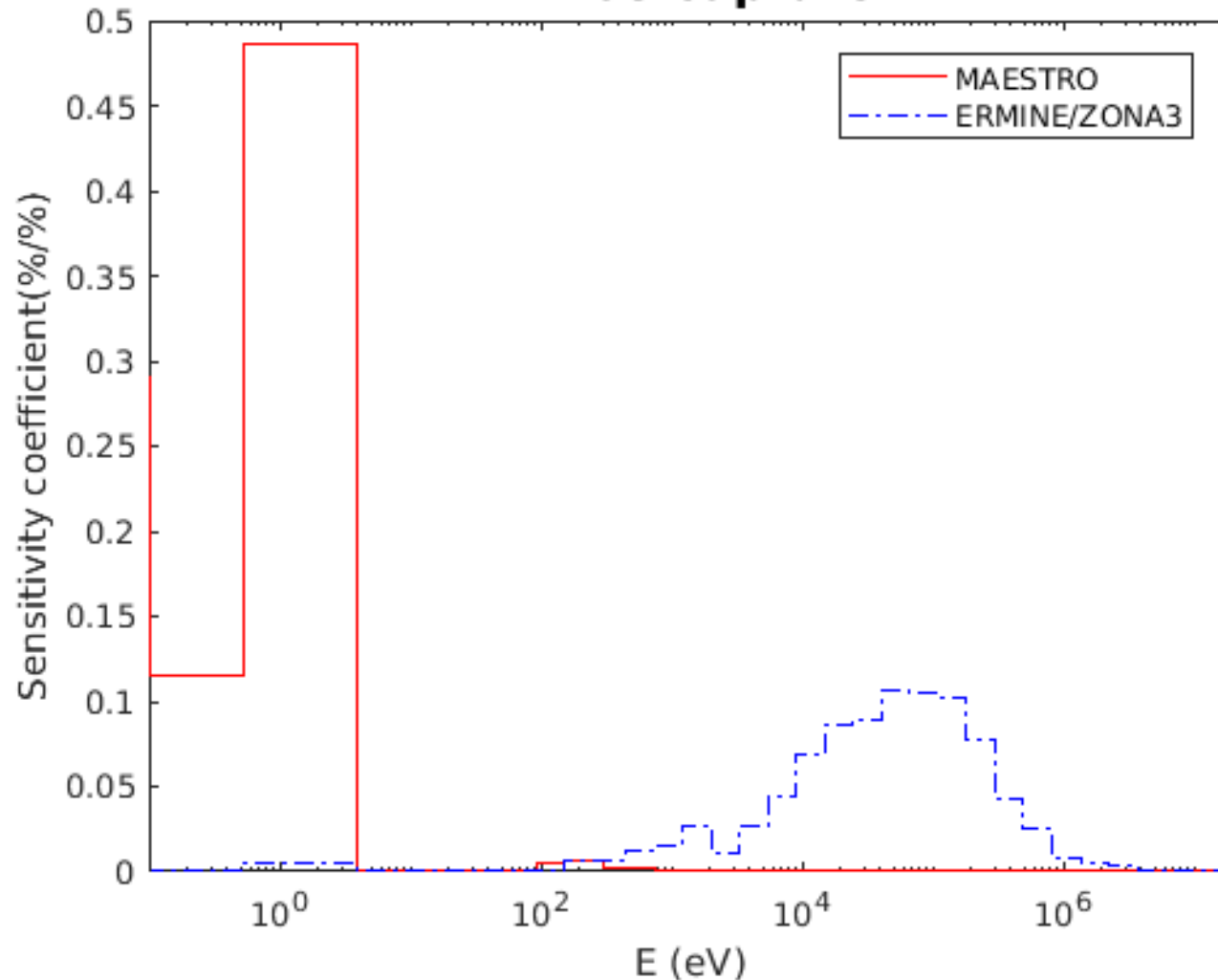
EGPT on ratio of RW – ERMINE-V/ZONA3 experiment

Sensitivity coefficients (%/%) on $\Delta\rho_{\text{Rh}} / \Delta\rho_{\text{U235}}$

	CAPT	FISS	EL	INEL	NU	SUM
U235	0.163	-1.171	0.000	0.019	-1.759	-2.747
U238	-0.172	-0.057	0.007	0.026	-0.088	-0.284
Pu239	-0.067	0.164	0.001	0.001	0.230	0.328
Pu240	-0.020	-0.011	0.000	0.000	-0.015	-0.045
Pu241	-0.006	0.049	0.000	0.000	0.068	0.111
O16	0.002		0.020	0.000		0.022
Na23	-0.002		0.009	0.004		0.011
Rh103	0.874		0.010	0.110		0.995

Sensitivity profile

Rh103 capture

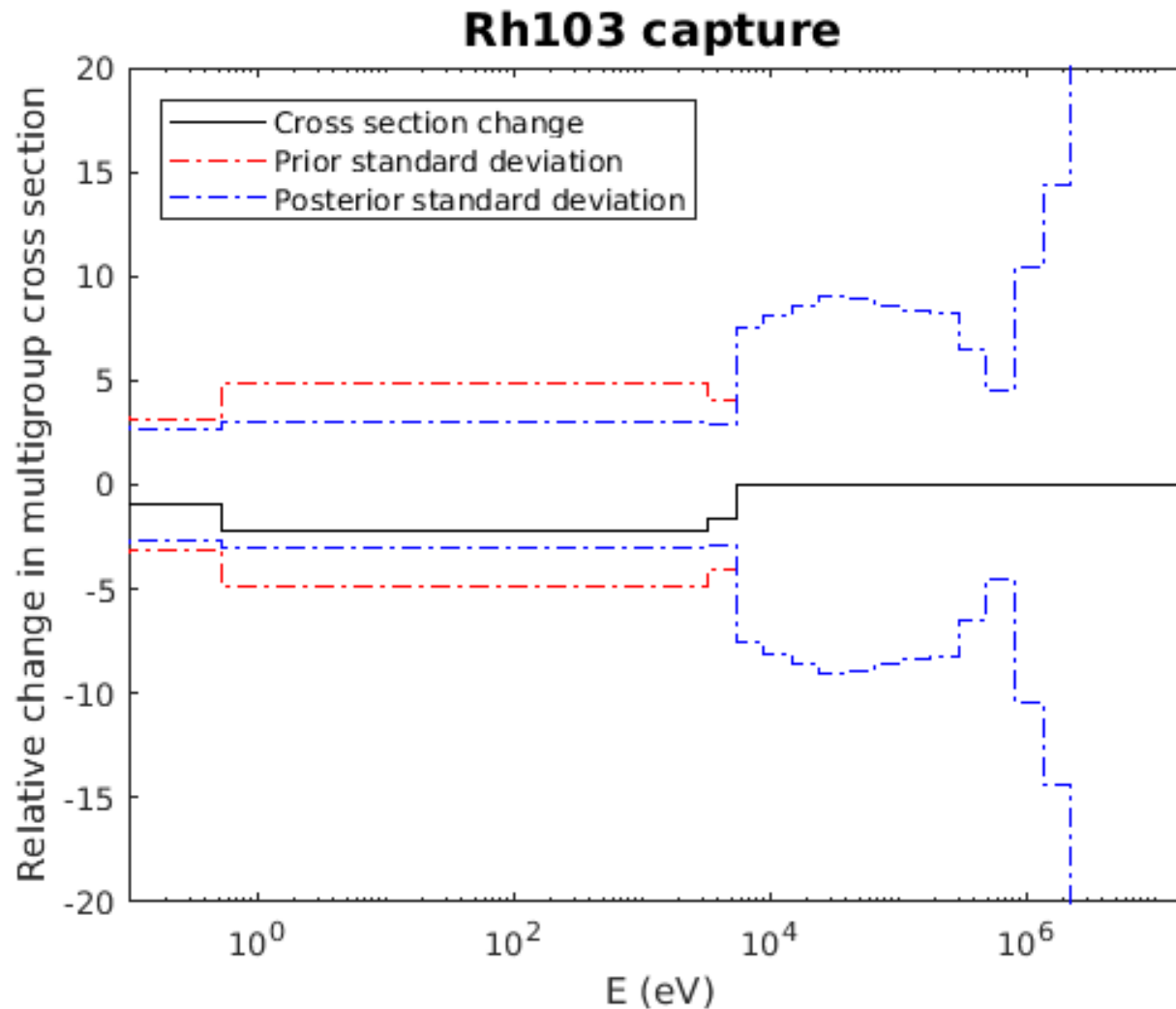


Prior nuclear data covariances

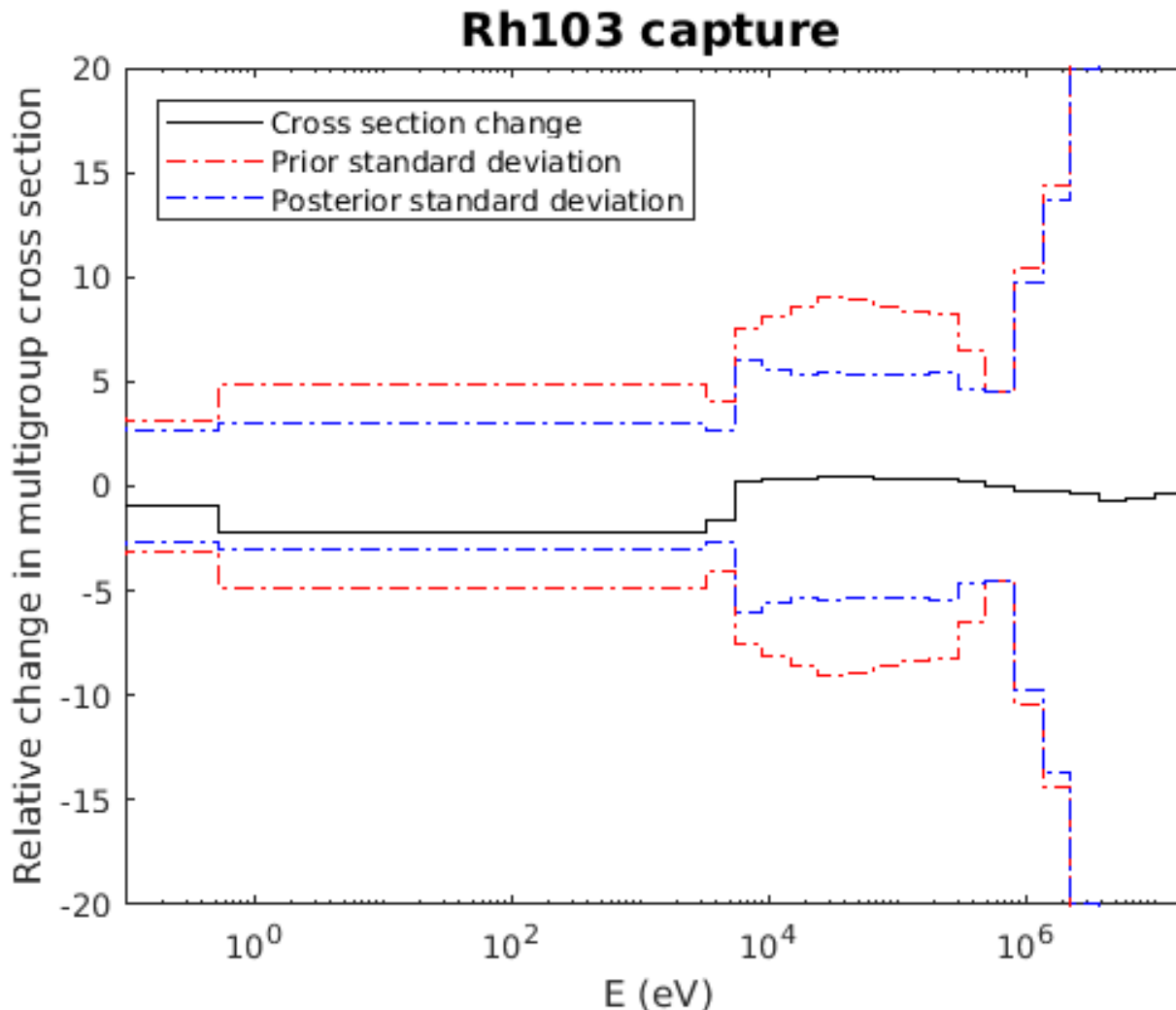
COMAC V2 set

Isotope	Origin of covariance files			
	Cross sections	Multiplicity	Thermal PFNS	Fast PFNS
U235	ENDF/B-VII.1	JENDL-4.0-up1	CEA	ENDF/B-VII.1
U238	CEA	JENDL-4.0-up1		JENDL-4.0-up1
Pu239	CEA	JENDL-4.0-up1	CEA	JENDL-4.0-up1
Pu240	CEA	JENDL-4.0-up1		JENDL-4.0-up1
Pu241	ENDF/B-VII.1	JENDL-4.0		JENDL-4.0
H1	ENDF/B-VII.1			
Li6	JEFF-3.2			
O16	JENDL-4.0			
Na23	CEA = JEFF32			
Zr90	ENDF/B-VII.1			
Zr91	ENDF/B-VII.1			
Rh103	ENDF/B-VII.1			

Result of the adjustment procedure MAESTRO experiment



**Result of the adjustment procedure
MAESTRO + ERMINE-V/ZONA3 experiment**



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Key-points

- Computing EGPT for SSRW experiments must account for the RW normalisation
- Using a reference sample of similar behavior minimizes the influence of indirect terms in the analysis of SSRW
- Combining independant thermal and fast spectrum experiments was applied for a significant uncertainty reduction on the ^{103}Rh capture cross section
 - 1eV – 10 keV 5% $\Rightarrow$ 3%
 - 10 keV – 1MeV 8% $\Rightarrow$ 5%

Perspectives

- Finalisation of S/U analysis for ERMINE-V experiments
- Computation of ERANOS sensitivities for RRR/SEG experiments
- Consistent assimilation of MINERVE/MAESTRO + RRR/SEG experiments for the list of common isotopes: *Mo-95, Mo-98, Mo-100, Rh-103, Cs-133, Ag-109, Sm-149, Eu-153, Nb, Co, Cd, Fe, Ni, Mo, Mn, Au, Cu, Zr, C*

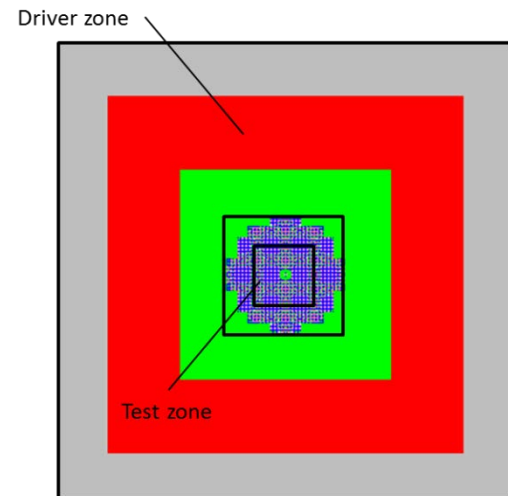
Open question to investigate

- In the case of experimental results reported as infinite diluted reactivity worth (e.g. RRR/SEG), which mass to consider to apply the EGPT? Is the balance between indirect and direct contributions sensitive to the magnitude of the RW? Limit range for linear assumption?
 - Large masses:
 - + no convergence issues
 - increase of self-shielding effects
 - Small masses:
 - + closer to the real experiment
 - convergence issues

⇒ Test of increasing concentrations for the sample mass
- In fast spectrum experiments, are the EGPT profiles influenced by the size of the geometrical model?

⇒ Test of various model sizes
- Can Monte-Carlo methods replace deterministic ones for SSRW sensitivities? Minimum acceptable RW value?

⇒ EGPT benchmark to be done between various deterministic (APOLLO2, ERANOS) and Monte-Carlo (SERPENT, TRIPOLI, MCNP) codes



THANK YOU FOR YOUR ATTENTION

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