

WIR SCHAFFEN WISSEN – HEUTE FÜR MORGEN



Stefan Radman, Mathieu Hursin, Gregory Perret :: Paul Scherrer Institut

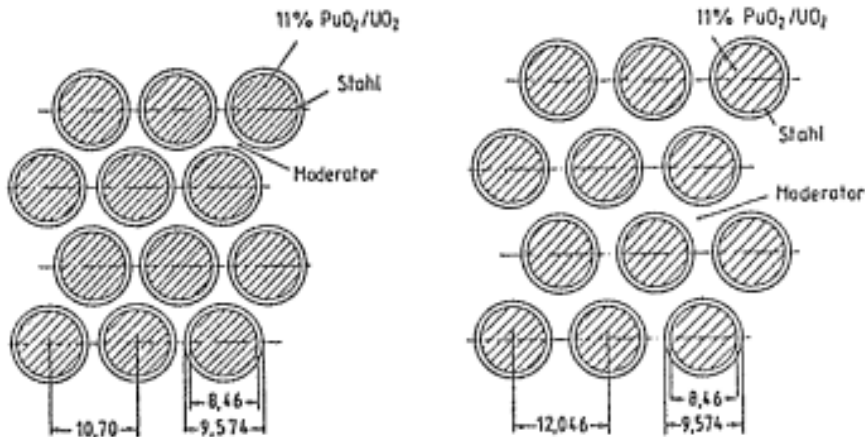
# PROTEUS FDWR-II (HCLWR) program Contribution to SG-39

WPEC SG39 meeting, Paris, France

- Reminder of FDWR Experiments at PROTEUS
- Summary of PSI experimental data contribution to SG39
  - K-inf C/E and sensitivities
  - Issue with infinitely dilute inelastic scattering cross sections
  - Elastic scattering sensitivity coefficients
- Additional responses
  - Void coefficients
  - Spectral indices
- Conclusion and outlook

# FDWR-II – Experimental Configurations

## Phase II



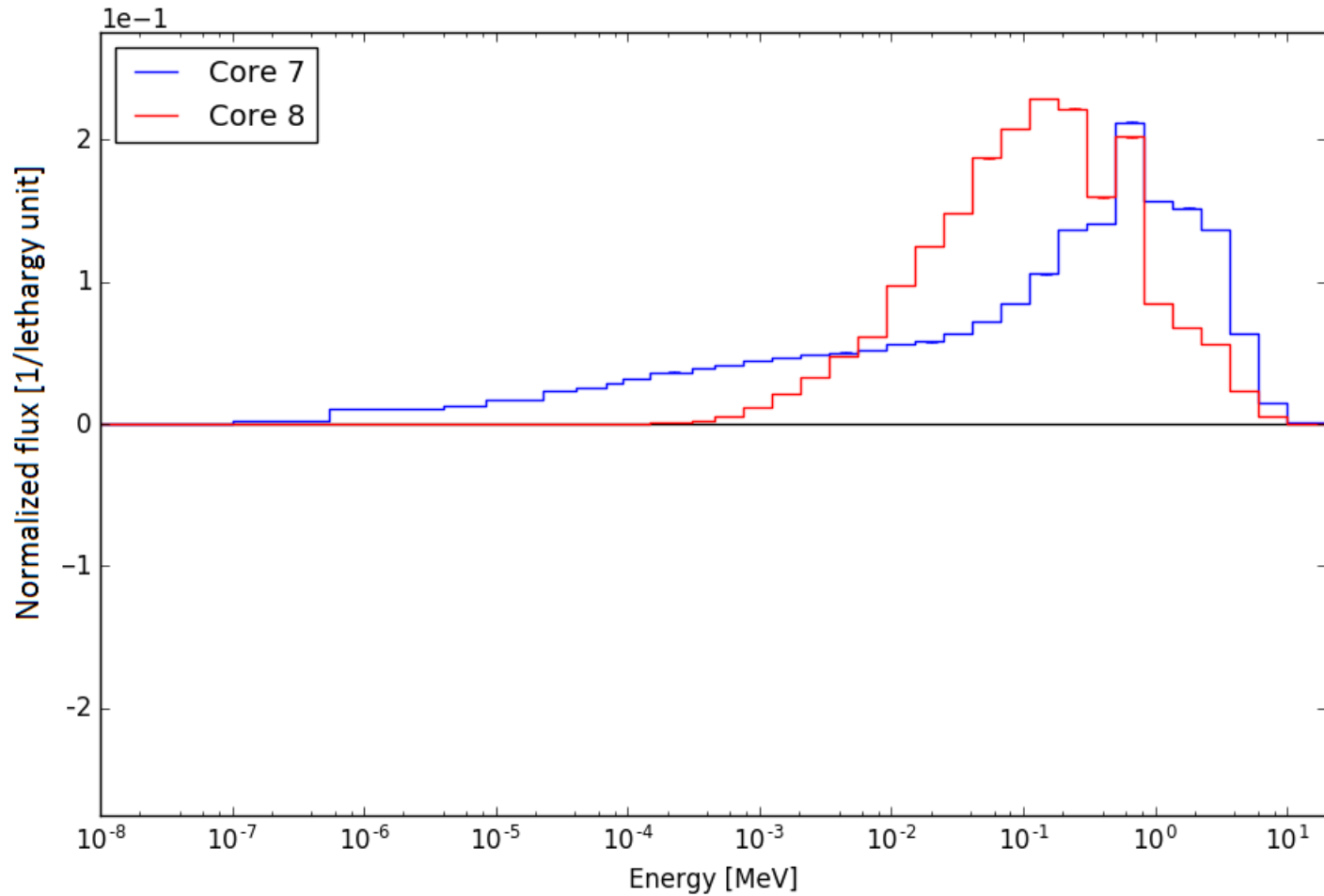
## FDWR Phase II

- From 1985 to 1990 in PROTEUS reactor
- PROTEUS is a driven system whose test zone contains the FDWR lattices
- $\text{UO}_2/\text{PuO}_2$  pellets with 11%  $\text{PuO}_2$
- $\text{Pu}(8/9/0/1/2)$ : 1%, 64%, 23%, 8%, 4%
- Fuel diameter: 8.46mm
- Fuel total height: 84 cm
- 2 axial blankets:
  - Udep. 0.224w%  $^{235}\text{U}$
  - 28-cm high each

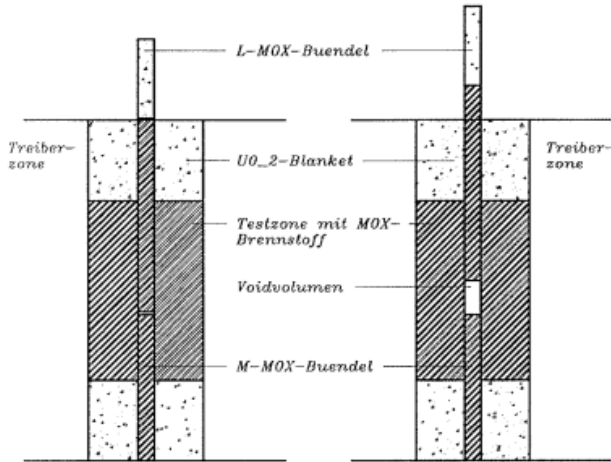
Kern	p/d	$V_M/V_F$	Moderator	Eff. Moderation
7	1.12	0.48	$\text{H}_2\text{O}$	0.48
8	1.12	0.48	ohne	0.00
9	1.12	0.48	Dowtherm	0.28
10	1.12	0.48	Dowtherm	0.28
11	1.12	0.48	ohne	0.00
12	1.12	0.48	$\text{H}_2\text{O}$	0.48
13	1.26	0.95	$\text{H}_2\text{O}$	0.95
14	1.26	0.95	ohne	0.00
15	1.26	0.95	Dowtherm	0.55
16	1.26	0.95	$\text{H}_2\text{O}$	0.95
17	1.26	0.95	ohne	0.00
18	a)	2.07	$\text{H}_2\text{O}$	2.07
19	1.26	0.95	$\text{H}_2\text{O}$	0.95
20	1.26	0.95	$\text{D}_2\text{O}$	-

# FDWR-II - Spectrum Comparison

Flux comparison of Core 7 and Core 8



# FDWR-II – Measurement types

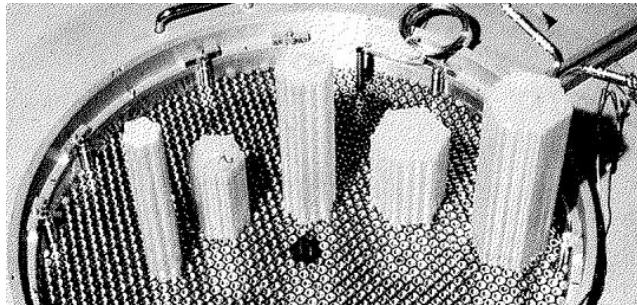


- $K_{\infty}$  measurements

$$k_{\infty} = 1 + B^2 \cdot M^2$$

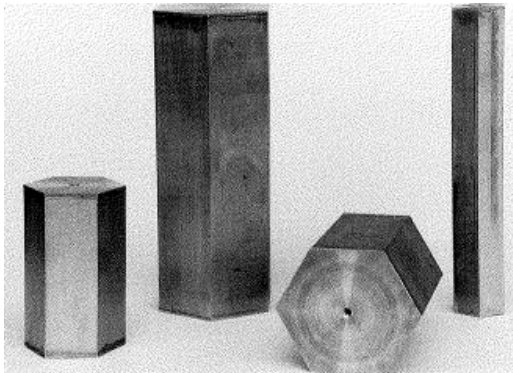
$$\frac{\rho_Z}{\rho_S} \frac{S}{R_f} = \bar{v} \frac{\overline{\Phi^{+X}}}{\overline{\Phi^{+S}}} \left( 1 - \frac{1}{k^+} \right)$$

- Using axial and radial bucklings
- Using compensation methods with auto-rod and a  $^{252}\text{Cf}$  source



- Reactivity effects

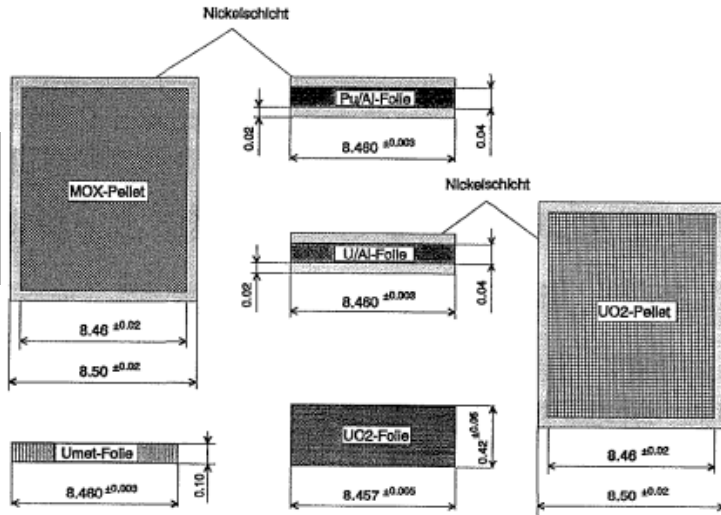
- Void volume



Absorber	Form	Durchmesser	Cladding	Bemerkung
B <sub>4</sub> C(nat)	Pellet	7.473	ja	Referenzabsorber
B <sub>4</sub> C(nat)	Pulver	7.430	ja	
B <sub>4</sub> C(93%) <sup>10</sup> B	Pellet	7.430	ja	
Ag15In5Cd	Legierung	8.830	nein	
Hafnium	Metall	8.350	ja	
Gd <sub>2</sub> O <sub>3</sub>	Pellet	8.310	ja	
Sm <sub>2</sub> O <sub>3</sub>	Pellet	7.000	ja	
Tantal	Metall	8.290	ja	
Eu <sub>2</sub> O <sub>3</sub>	Pellet	8.243	ja	
Zircaloy-2	Legierung	8.300	nein	Strukturmaterial
Stahl	Metall	8.240	nein	Strukturmaterial

# FDWR-II – Measurement types

## Spectral index measurements (core 7)



• F5/F9 ~ 0.91      F1/F9 ~ 1.68

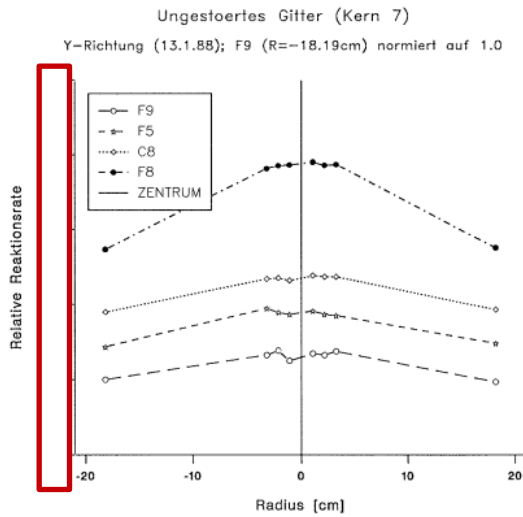
• F8/F9 ~ 1.14e-2      C2/F9 ~ 1.12

• C8/F9 ~ 7.8e-2

• Typical uncertainties

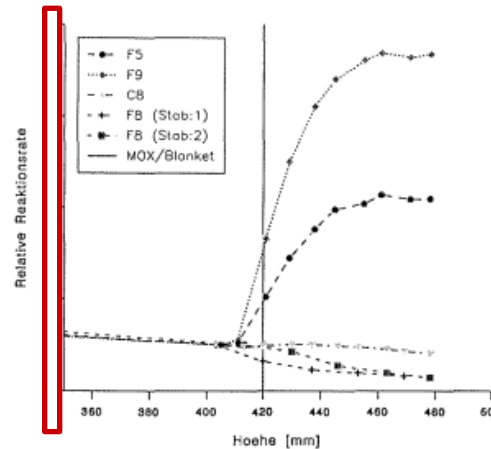
F5: 1.8%, F8: 1.9%, F9: 1.5%, C8: 1.8%

## Reaction rate radial and axial traverses



Axiale Traverse durch MOX-Blanket Interface

Folien (23.2.1988), normiert auf 1.0 bei 404 mm



# Data package provided to SG39 members

- C/E for k-inf of Core 7 and 8
  - Data provided
    - Pincell geometry
    - Fuel composition
    - C and E values
  - Calculation: MCNP and pincell models
  - Preferred measurement: cell method b/c smaller uncertainty
  
- Sensitivity coefficients generated from pincell models
  - MCNP6.1.1 & JEFF-3.1.1
  - Uncertainties are provided
  - Infinitely diluted cross sections are provided
  
- Sensitivity coefficients tables according to SG33 format
  - Generated with SERPENT-v2.1.15
  
- **Extra info (P1 moment sensitivities) will be generated with SERPENT-v2.1.19**

Data	Location
Kinf values, C/Es and uncertainties	Section 3
Sensitivity coefficients graphs	Core7.tar.gz Core8.tar.gz
Sensitivity coefficients tables	Core7_SC_MCNP.txt Core8_SC_MCNP.txt
Infinitely diluted cross sections	File J311.dat

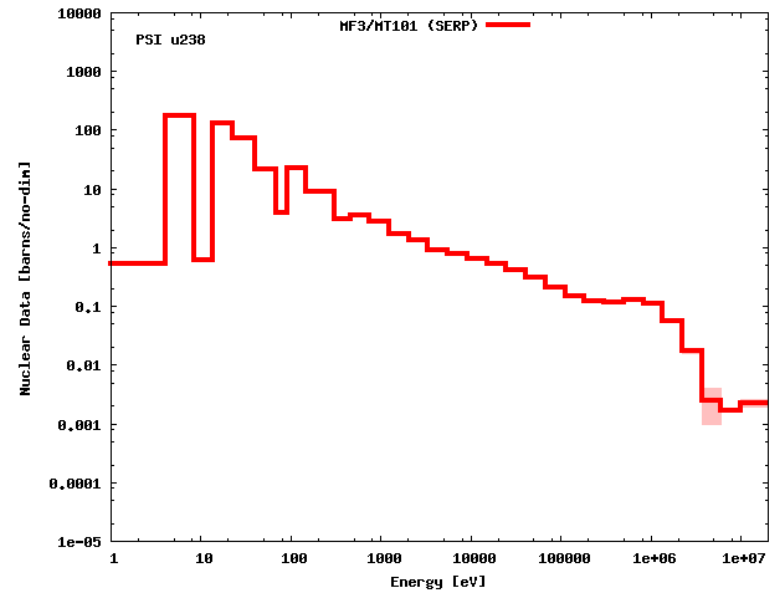
# Infinitely Dilute Cross Sections

- 20 MeV homogeneous source in infinite pure graphite medium

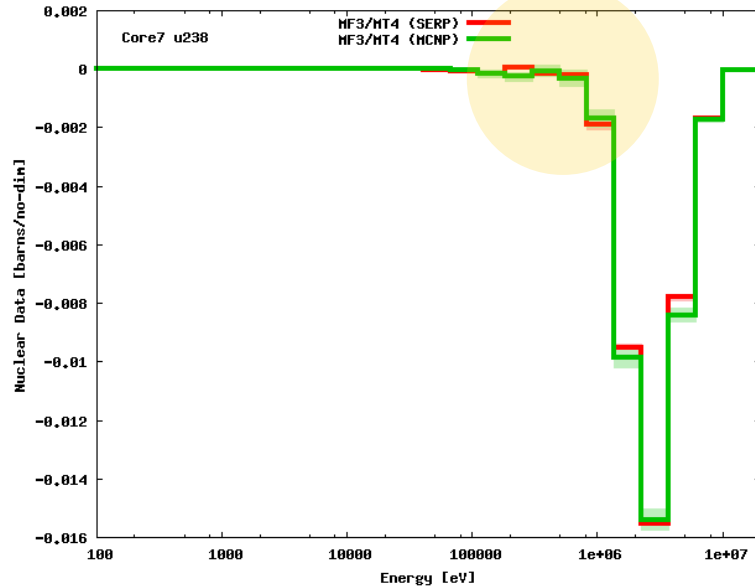
- MCNPX-2.4 & JEFF-3.1.1 library.
  - $10^6$  neutrons histories
  - The reaction rates and flux were tallied in the 33-energy group structure

- The cross sections and associated relative uncertainties (1 standard deviation) for the isotopes and reactions of the WPEC Subgroup 33

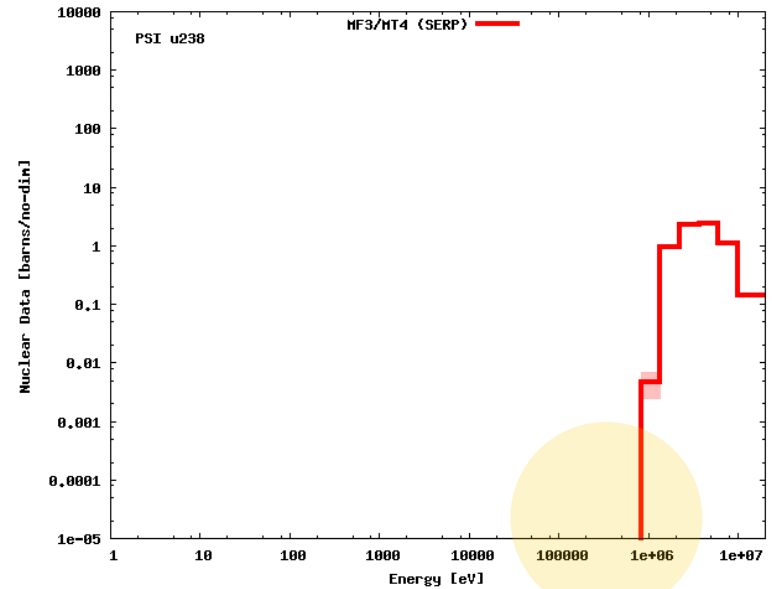
## U-238 Capture



# Infinitely Dilute Inelastic Cross Sections



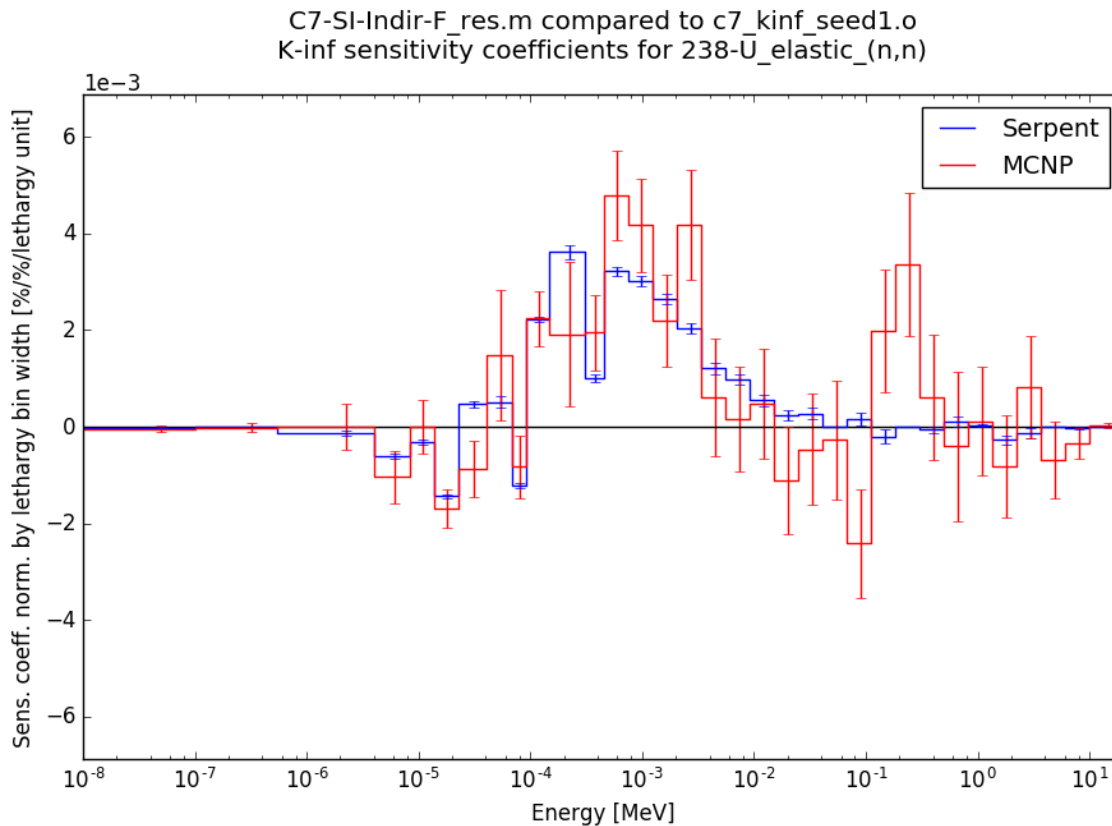
## Sensitivity



## Infinitely Dilute Cross Sections

- Stop well above the threshold.
  - Input error: only MT 91 was tallied.
  - MCNP will be rerun
- Sensitivity coefficients are correct though.
- New cross sections will be provided

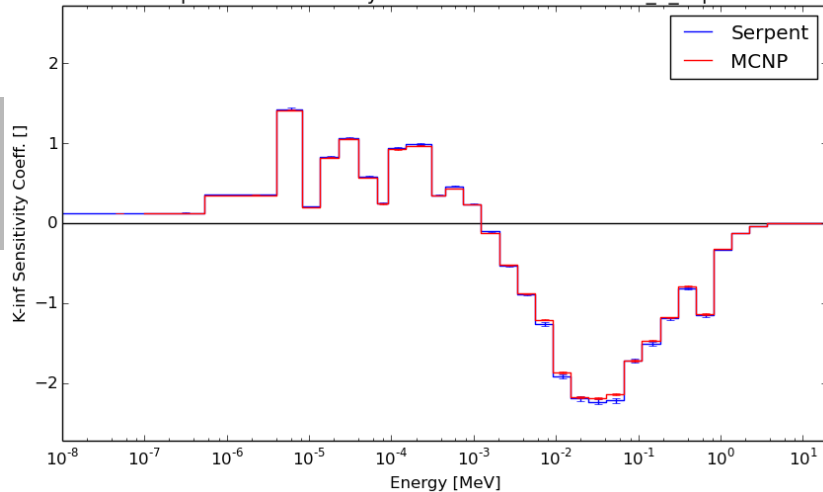
# Elastic scattering issue



- Good agreement between codes
  - Previously reported MCNP uncertainty was wrong
- Large uncertainties due to poor convergence of the estimator

# Void reactivity Sensitivity Coefficients

Comparison of reactivity coefficient's SCs for U-238\_n\_capture



$$\Delta\rho = \rho_1 - \rho_0 = \frac{k_1 - k_0}{k_1 k_0}$$

- C/E can be inferred from k-inf results.

- Sensitivity coefficients of void reactivity

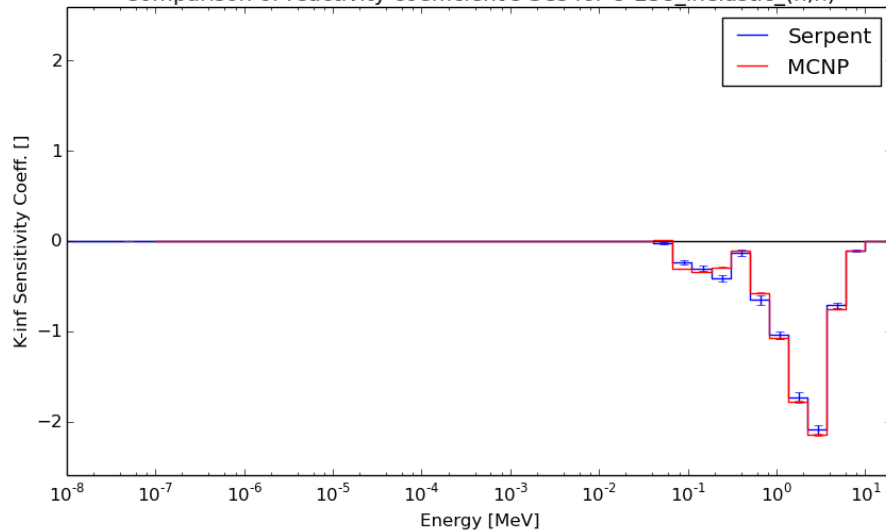
- Computed with EGPT

$$SC(\Delta\rho, \sigma) = \frac{1}{\Delta\rho} \left( \frac{SC(k_1, \sigma)}{k_1} - \frac{SC(k_0, \sigma)}{k_0} \right)$$

- Issue with MC based sensitivities

- SERPENT-V2.1.19 will be used in the future

Comparison of reactivity coefficient's SCs for U-238\_inelastic\_(n,n)



# Sensitivity coefficients for spectral indices

A spectral index is a ratio of reaction rates:

$$R = \frac{\langle \Sigma_1 \phi \rangle}{\langle \Sigma_2 \phi \rangle}$$

where «1» and «2» are the labels of the considered nuclide-reaction pairs. Brackets are to be intended as integral over the energy range of interest. The sensitivity of the spectral index to a change in a certain cross section ( $\Sigma_x$ ) can be expanded as:

$$S_{R,x} = \frac{\langle \frac{\partial \Sigma_1}{\partial \Sigma_x} \phi \rangle}{\frac{\Sigma_x}{\langle \Sigma_1 \phi \rangle}} - \frac{\langle \frac{\partial \Sigma_2}{\partial \Sigma_x} \phi \rangle}{\frac{\Sigma_x}{\langle \Sigma_2 \phi \rangle}} + \frac{\langle \Sigma_1 \frac{\partial \phi}{\partial \Sigma_x} \rangle}{\langle \Sigma_1 \phi \rangle} - \frac{\langle \Sigma_2 \frac{\partial \phi}{\partial \Sigma_x} \rangle}{\langle \Sigma_2 \phi \rangle}$$

The first two terms are referred to as the **direct part** of sensitivity coefficient, the last two as the **indirect part** of it.

# Sensitivity coefficients for spectral indices

$$S_{R,x} = \underbrace{\frac{\langle \frac{\partial \Sigma_1}{\partial \Sigma_x} \phi \rangle}{\Sigma_x} - \frac{\langle \frac{\partial \Sigma_2}{\partial \Sigma_x} \phi \rangle}{\Sigma_x}}_{S_{R,x}^{dir}} + \underbrace{\frac{\langle \Sigma_1 \frac{\partial \phi}{\partial \Sigma_x} \rangle}{\langle \Sigma_1 \phi \rangle} - \frac{\langle \Sigma_2 \frac{\partial \phi}{\partial \Sigma_x} \rangle}{\langle \Sigma_2 \phi \rangle}}_{S_{R,x}^{indir}}$$

The **direct term** quantifies the effect of the perturbation of  $\Sigma_x$  on the reaction rate itself. The direct part is zero whenever the cross section that is being perturbed is not  $\Sigma_1$  or  $\Sigma_2$ .

The **indirect term** quantifies the effect of the perturbation of  $\Sigma_x$  on the flux, which in turn affects the spectral index.

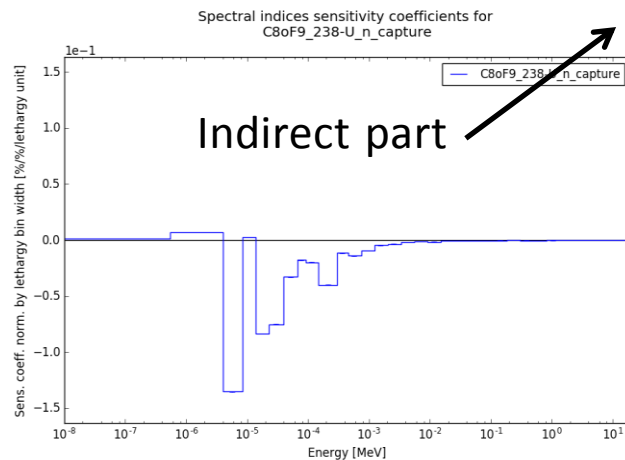
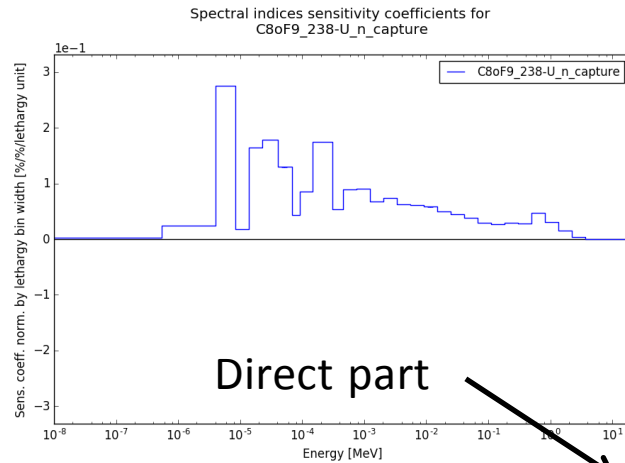
# Serpent sensitivity capability

The modified version of **Serpent 2.1.19** is able to **compute the indirect part** ( $S_{R,x}^{indir}$ ) of the sensitivity coefficients. The **direct part** of the sensitivity coefficients **has to be computed** separately through a standard SERPENT calculation.

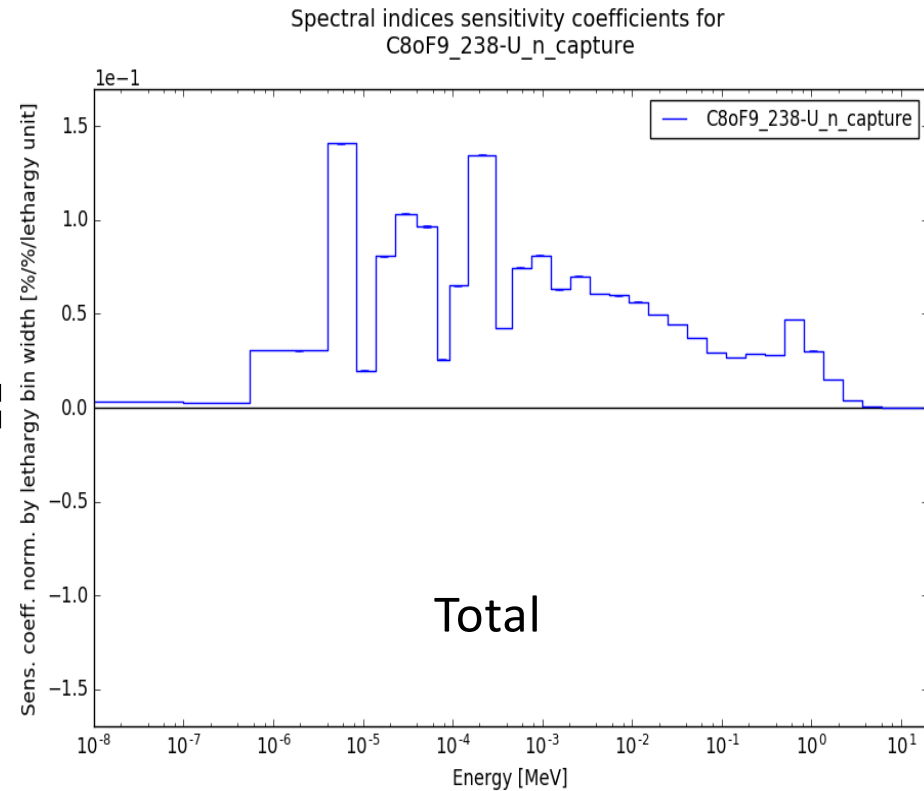
A MATLAB script has been written to generate the direct and indirect parts of the sensitivity based on 2 SERPENT calculations.

# Results for spectral indices sensitivity coeffs.

Example: sensitivity of  $^{238}\text{U}$ -capture over  $^{239}\text{Pu}$ -fission for a perturbation in the  $^{238}\text{U}$ -capture cross section.



+ =



# Results for spectral indices sensitivity coeffs.

The sensitivity coefficients have been obtained for the following spectral indices:

- $^{235}\text{U}$ -fission over  $^{239}\text{Pu}$ -fission
- $^{238}\text{U}$ -capture over  $^{239}\text{Pu}$ -fission
- $^{238}\text{U}$ -fission over  $^{239}\text{Pu}$ -fission
- $^{241}\text{Pu}$ -fission over  $^{239}\text{Pu}$ -fission
- $^{242}\text{Pu}$ -capture over  $^{239}\text{Pu}$ -fission

The perturbed cross sections for which sensitivities have been evaluated are all those of nuclides  $^1\text{H}$ ,  $^{16}\text{O}$ ,  $^{235}\text{U}$ ,  $^{238}\text{U}$ ,  $^{239}\text{Pu}$ ,  $^{240}\text{Pu}$ ,  $^{241}\text{Pu}$ ,  $^{242}\text{Pu}$  for the reactions of elastic scattering, inelastic scattering, capture, total fission and the parameter  $\nu_T$ .

# Outlook of Re-analysis work at PSI

- Master student currently working on HCLWR re-analysis
  - Sensitivity work on 1D models almost complete
    - K-inf
    - Void coefficient
    - Spectral indices
  - About to start the development of 3D models
- Previous delivery will be updated
  - Fixing infinitely dilute inelastic cross sections
  - Addition of sensitivities to P1 scattering moments
  - C/E + sensitivities for spectral indices
- Feedbacks on Data Delivery
  - Was it used?
  - Is it useful in terms of data assimilation?

# Wir schaffen Wissen – heute für morgen



# Serpent sensitivity capability

The modified version of **Serpent 2.1.19** is able to **compute the indirect part** ( $S_{R,x}^{indir}$ ) of the sensitivity coefficients. The **direct part** of the sensitivity coefficients **has to be computed separately**.

Assume that the direct part of the energy-resolved sensitivity coefficient of

$R = \frac{\langle \Sigma_1 \phi \rangle}{\langle \Sigma_2 \phi \rangle}$  to a perturbation of  $\Sigma_1$  is needed. Then, within a standard

Serpent 2 input:

- Define **integral** detector for  $\langle \Sigma_1 \phi \rangle$  (assume name is «R1»)
- Define **energy resolved** detector for  $\langle \Sigma_1 \phi \rangle$  (assume name is «R1E»)
- Add «dt 3 R1» option (i.e. divide by values of R1) to the «R1E» detector

The score of the «R1E» detector will be  $S_{R,1}^{dir}$  and will normalize to 1.