

# Sensitivity Computation with Monte Carlo Methods (Action C8, WPEC/Sg.39)

E. Ivanov  
T. Ivanova

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# General Remarks

- Objective of the exercise is to test continuous energy (CE) and continuous angular distribution sensitivity capabilities implemented in Monte Carlo codes
- Monte Carlo (MC) tools compute CE sensitivity coefficients in terms of Fréchet derivatives, i.e., physical meaning of the coefficient is linear response of  $k_{\text{eff}}$  on multiplication of cross sections profile on a scalar value
- In contrary with deterministic approaches, Monte Carlo perturbation theory does not use the following bi-orthogonal ration below, where  $i, j$  are orders of modes

$$\langle \lambda_i \cdot \hat{\mathbf{F}} \cdot \vec{\Phi}_i, \vec{\Psi}_j \rangle = \langle \lambda_j \cdot \hat{\mathbf{F}}^+ \cdot \vec{\Psi}_j, \vec{\Phi}_i \rangle = a_{i,j} \cdot \delta_{ij}$$

# Contributors

- | James Dyrda AWE
- | Evgeny Ivanov, Maria Brovchenko IRSN
- | Ian Hill NEA
- | Mathieu Hursin, Sandro Pelloni PSI
- | Brian Kiedrowski LANL
- | Ivan Kodeli IJS
- | Christopher Perfetti, Bradley Rearden ORNL

# Selected ICSBEP Benchmarks

- Popsy (Flattop-Pu) is a plutonium (94 wt%  $^{239}\text{Pu}$ ) sphere surrounded by a thick reflector of natural uranium.
  - PU-MET-FAST-006. Spherical model.
- Topsy (Flattop 25) is a highly enriched (93 wt% ) uranium sphere surrounded by a thick reflector of natural uranium.
  - HEU-MET-FAST-028. Spherical model.
- ZPR 9/34 loading 303 is a highly enriched uranium/ iron benchmark, reflected by steel.
  - HEU-MET-INTER-001. RZ model.
- ZPR 6/10 loading 24 is the core with heterogeneous plutonium metal fuel with carbon/stainless steel dilutions, and a steel reflector.
  - PU-MET-INTER-002. RZ model.

# Codes, Methods, Participants

- MONK: MC Fine-group Derivative operator sampling AWE
- SERPENT v2: MC CE Iterated Fission Probability (IFP) PSI
- ANISN/PARTISN: Deterministic MG IJS
- SCALE 6.1/TSUNANI-1D: Deterministic SN MG IRSN
- SCALE 6.1/TSUNAMI-3D: MC MG IRSN
- SCALE 6.2B: MC CE IFP ORNL, PSI, IRSN
- SCALE 6.2B: MC CE CLUTCH ORNL, PSI, IRSN
- MCNP6: MC CE IFP LANL, NEA, IRSN

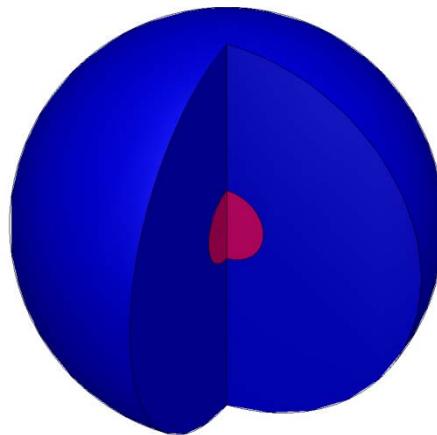
# Profiles Computations

Participant	Tool	Model	Cross sections	Method	Output, groups
AWE	MONK	3D	CE ENDF/B-VII.0 JEFF3.1	MC	33
PSI	SERPENT v2	3D	CE ENDF/B-VII	MC	33
NEA, LANL, IRSN	MCNP6	3D	CE, ENDF/B-VII.1	MC	238, 33
IRSN	SCALE 6.1	1D	MG, ENDF/B-VII.0	SN	238
PSI, ORNL, IRSN	SCALE 6.2B	3D	CE, ENDF/B-VII.1, 0	MC	238
JSI	ANISN/PARTISN	1D	See presentation by I. Kodeli	SN	33

- 238-gr. sensitivities converted into 33 gr. by IRSN BERING code (E. Ivanov)
- 33-gr. sensitivities converted to SCALE/sdf format by IRSN scripts (E. Ivanov)
- MCNP6 output converted into SCALE/sdf format by NEA script (I. Hill)
- Sensitivity profiles are presented using SCALE/Javapeno that reads \*.sdf

# PMF-006 (Flattop-Pu or Popsy)

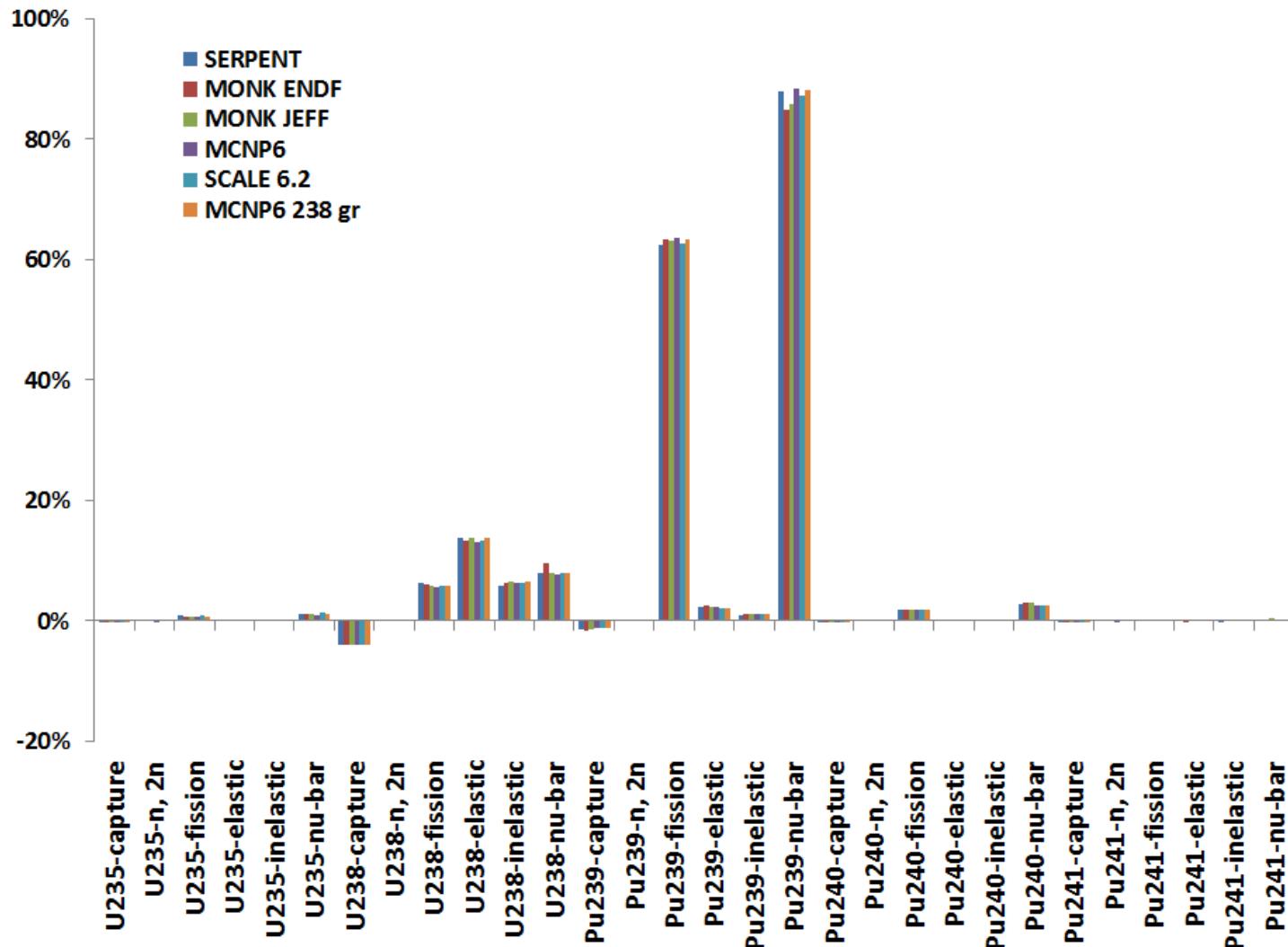
- Plutonium (94 wt  $^{239}\text{Pu}$ ) sphere surrounded by a thick reflector of natural uranium. Sensitive to scattering on heavy metals, and threshold reactions.
- $k_{\text{bench}} = 1.0000 \pm 0.0030$



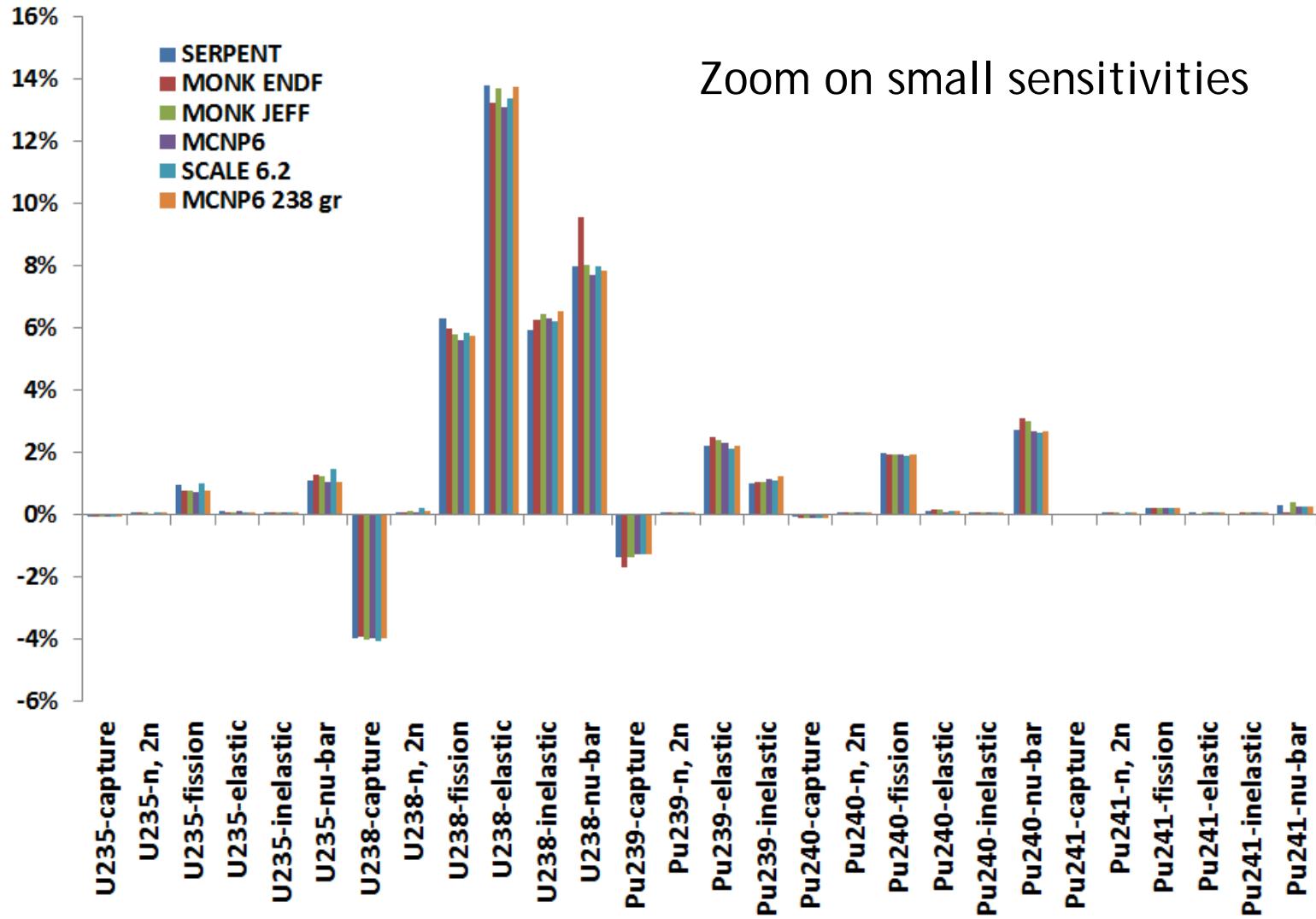
# Popsy: Integrated Sensitivities (1/3)

	SERPENT	MONK ENDF	MONK JEFF	MCNP6	SCALE 6.2	MCNP6 238 gr
U235-capture	-0,05	-0,06	-0,05	-0,05	-0,07	-0,05
U235-n, 2n	0,00	0,00	0,00	0,00	0,00	0,00
U235-fission	0,96	0,75	0,75	0,74	1,01	0,75
U235-elastic	0,09	0,07	0,08	0,12	0,08	0,08
U235-inelastic	0,03	0,03	0,03	0,02	0,02	0,03
U235-nu-bar	1,09	1,26	1,22	1,02	1,45	1,04
U238-capture	-4,00	-3,92	-4,04	-3,97	-4,08	-3,97
U238-n, 2n	0,08	0,07	0,10	0,06	0,19	0,10
U238-fission	6,30	5,99	5,81	5,62	5,82	5,73
U238-elastic	13,77	13,25	13,70	13,08	13,39	13,75
U238-inelastic	5,92	6,26	6,41	6,32	6,22	6,51
U238-nu-bar	7,95	9,58	8,03	7,71	7,98	7,83
Pu239-capture	-1,39	-1,71	-1,40	-1,28	-1,28	-1,29
Pu239-n, 2n	0,03	0,02	0,04	0,03	0,02	0,03
Pu239-fission	62,43	63,26	63,21	63,53	62,64	63,32
Pu239-elastic	2,22	2,49	2,37	2,32	2,13	2,19
Pu239-inelastic	1,01	1,06	1,04	1,13	1,10	1,24
Pu239-nu-bar	87,94	84,83	85,79	88,33	87,30	88,20
Pu240-capture	-0,09	-0,12	-0,10	-0,10	-0,10	-0,10
Pu240-n, 2n	0,00	0,00	0,00	0,00	0,00	0,00
Pu240-fission	1,95	1,94	1,91	1,91	1,88	1,91
Pu240-elastic	0,11	0,14	0,15	0,07	0,12	0,12
Pu240-inelastic	0,07	0,07	0,08	0,08	0,05	0,06
Pu240-nu-bar	2,73	3,10	3,00	2,66	2,62	2,65
Pu241-capture	-0,01	-0,01	-0,01	-0,01	-0,01	-0,01
Pu241-n, 2n	0,00	0,00	0,00	0,00	0,00	0,00
Pu241-fission	0,20	0,22	0,19	0,19	0,19	0,19
Pu241-elastic	0,01	0,00	0,01	0,01	0,01	0,01
Pu241-inelastic	0,00	0,00	0,00	0,01	0,00	0,01
Pu241-nu-bar	0,28	0,02	0,40	0,27	0,27	0,27

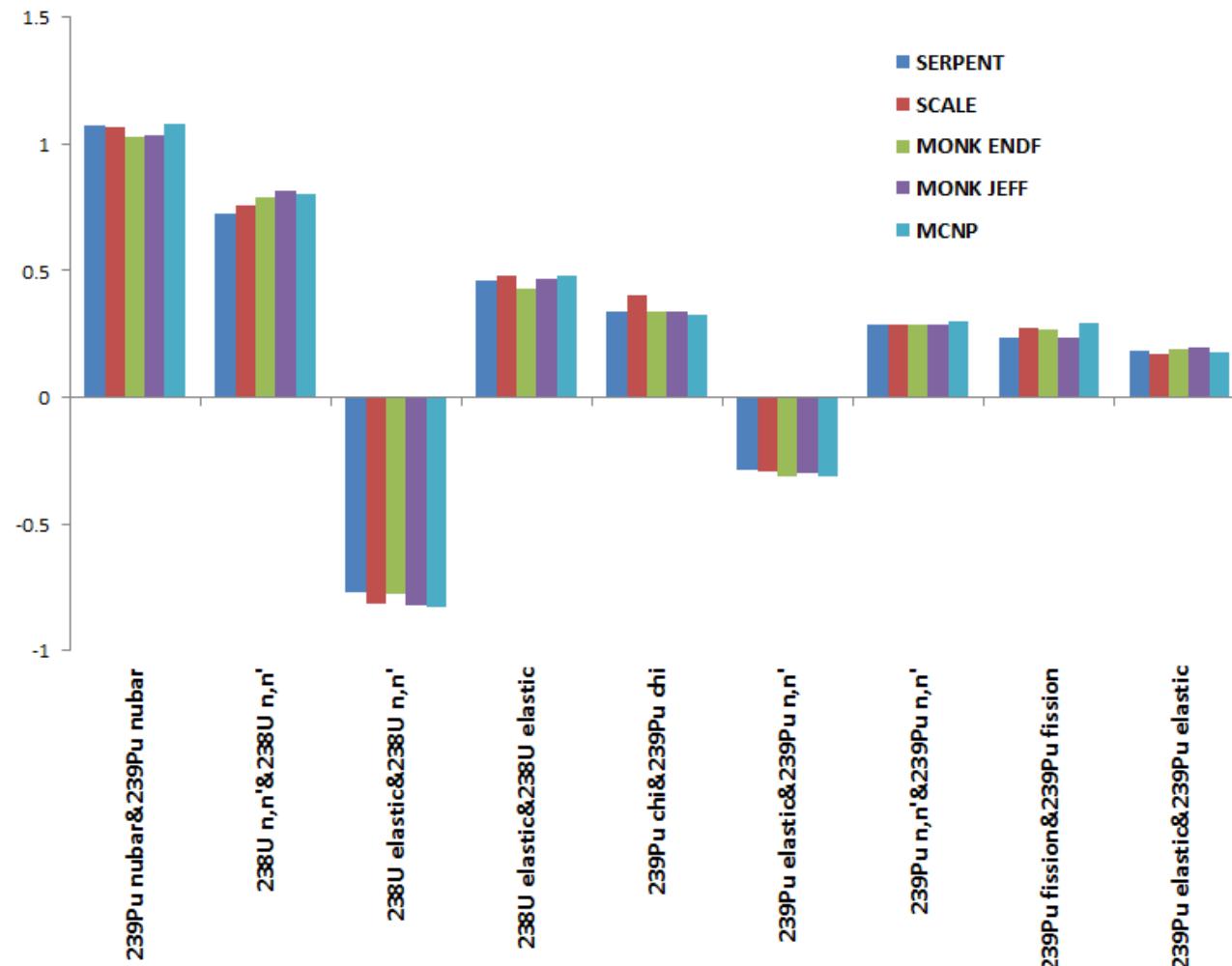
# Popsy: Integrated Sensitivities (2/3)



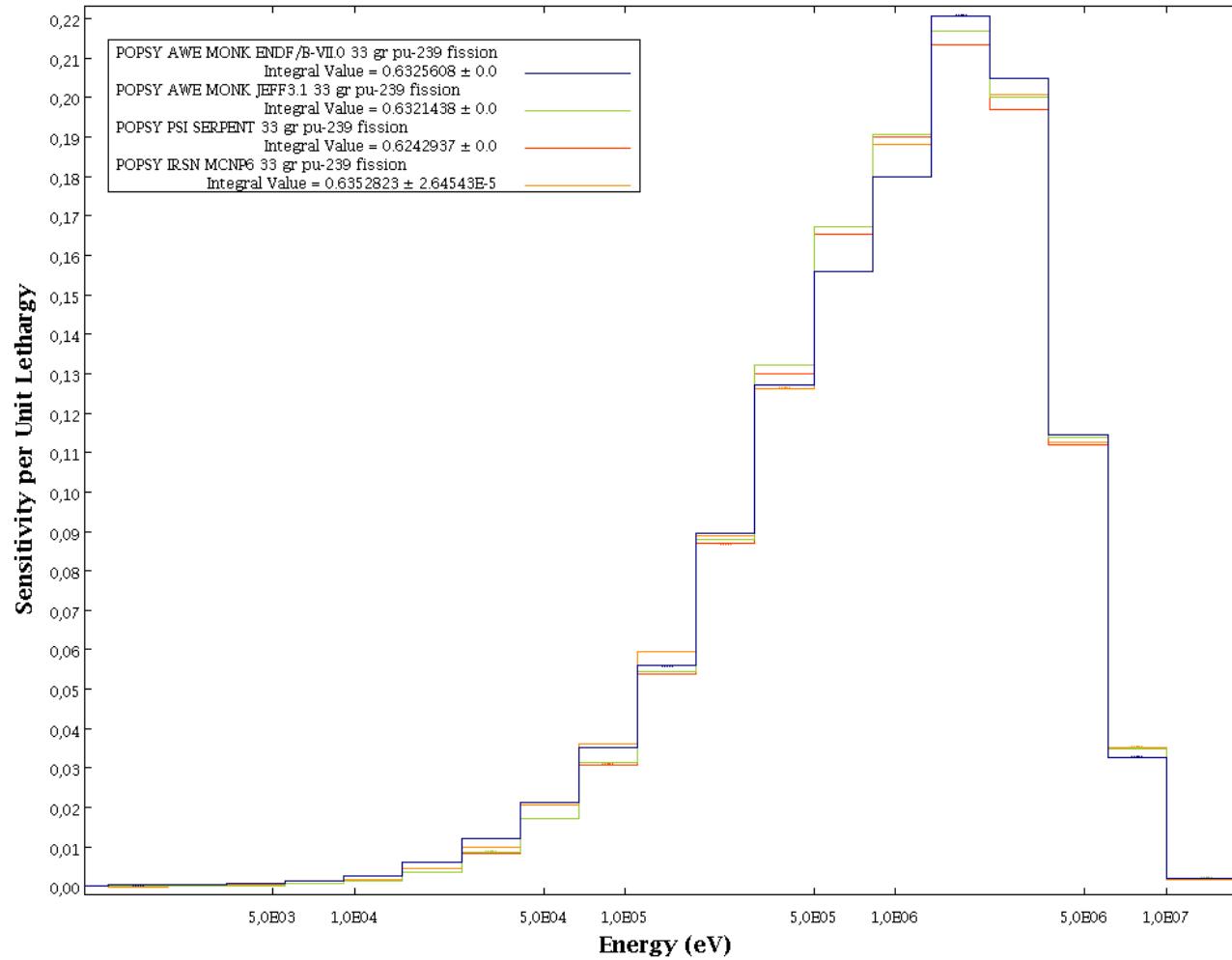
# Popsy: Integrated Sensitivities (3/3)



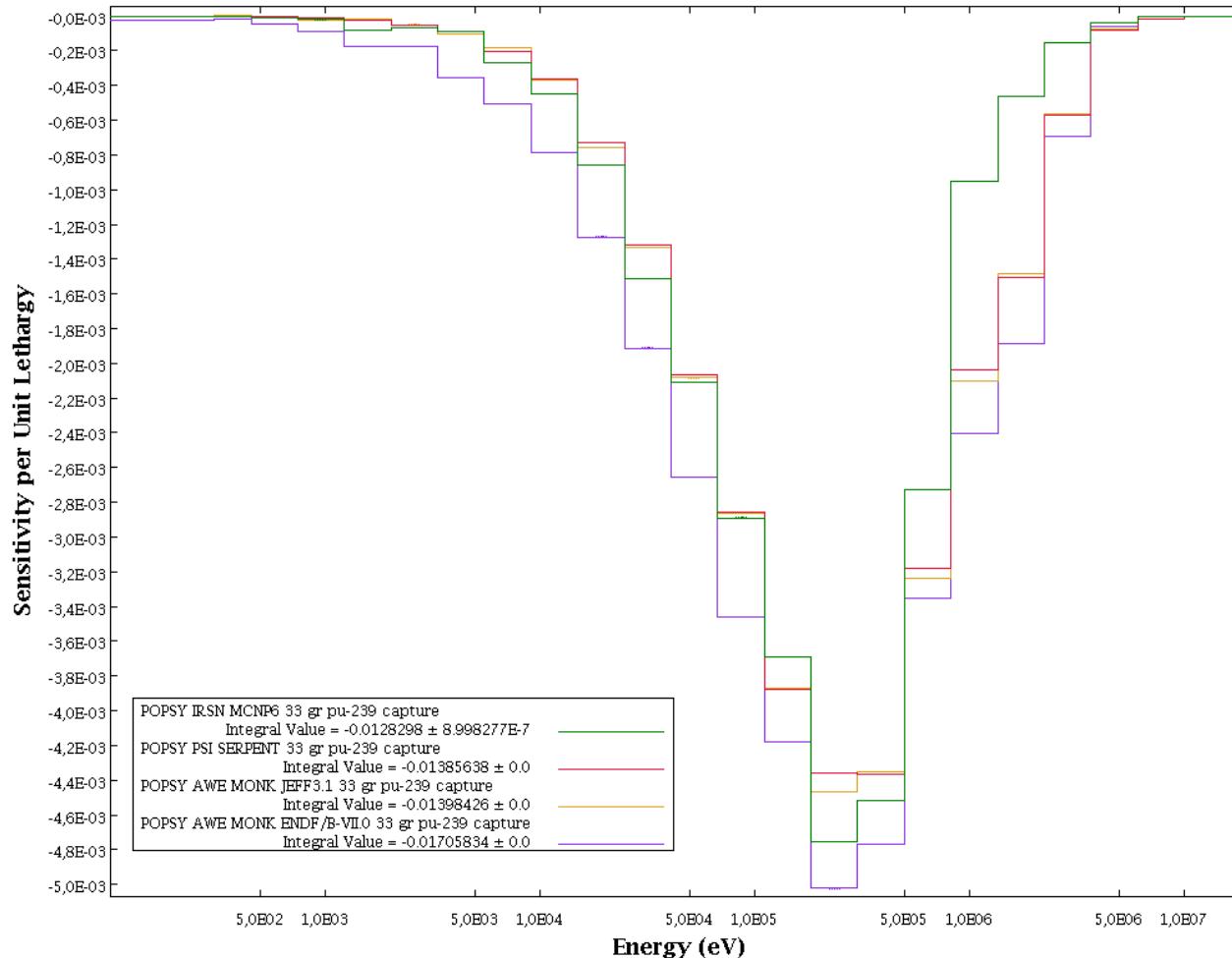
# Popsy: Uncertainties by reactions



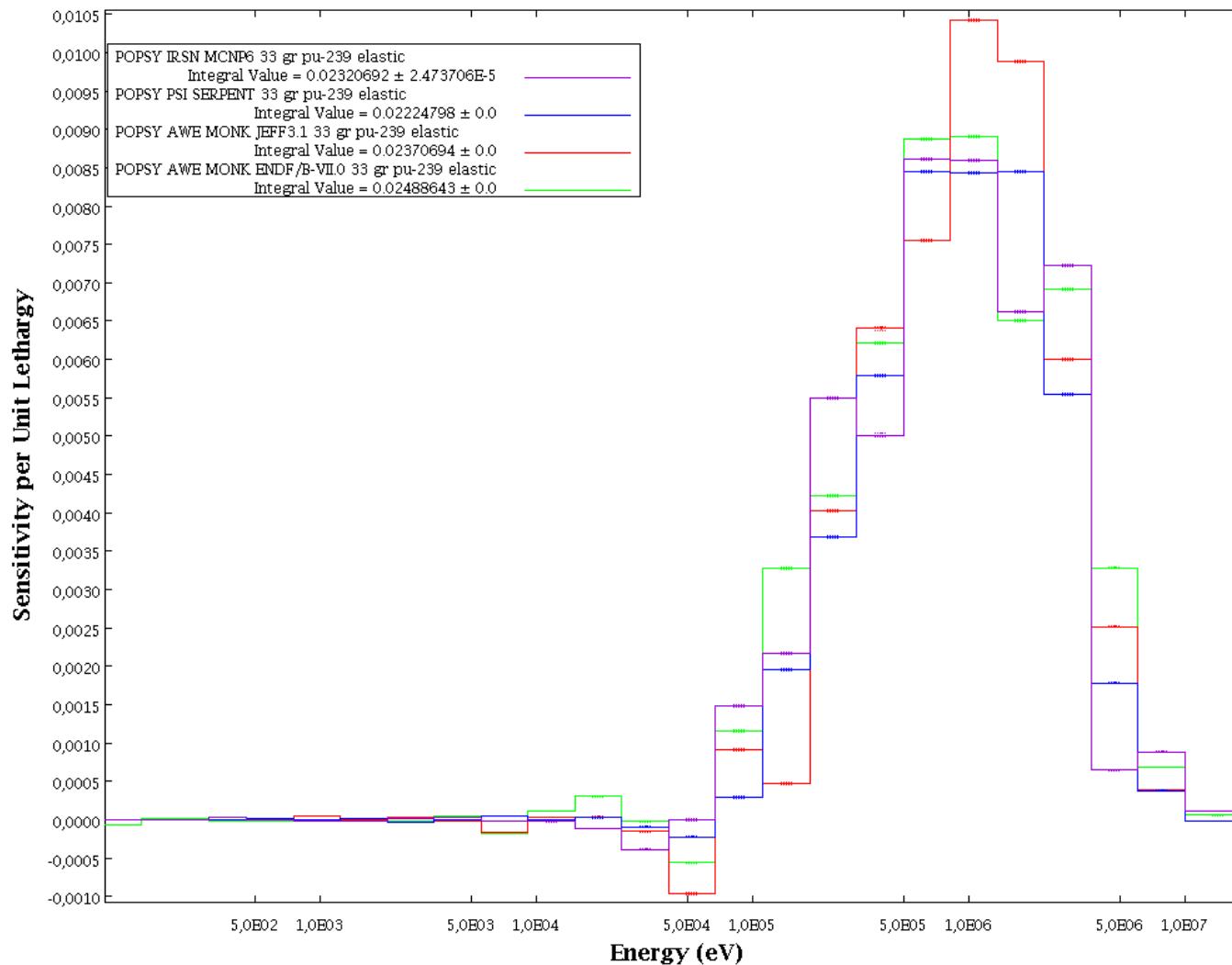
# Popsy: Pu-239 Fission Profiles



# Popsy: Pu-239 Capture Profiles



# Popsy: Pu-239 Elastic Profiles



# HMF-028 (Flattop-25 or Topsy)

- Highly enriched (93 wt%) uranium sphere surrounded by a thick reflector of natural uranium.
- $k_{\text{bench}} = 1.0000 \pm 0.0030$

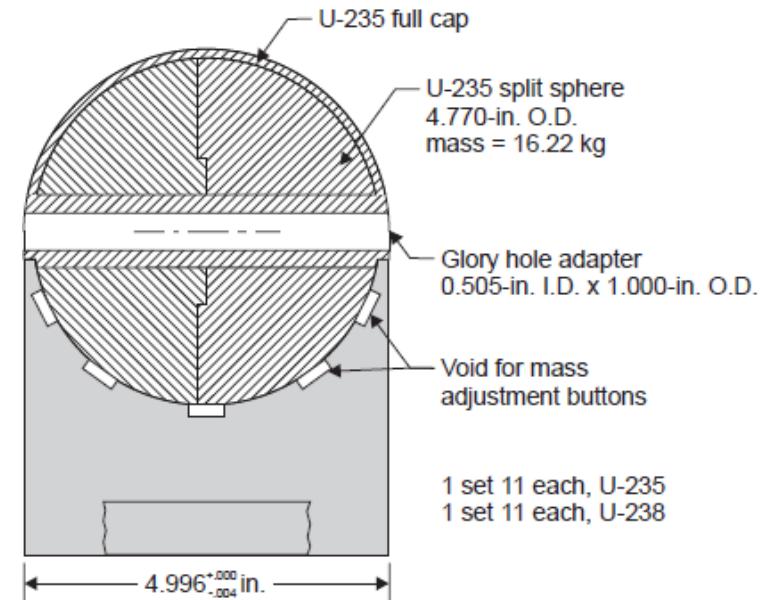
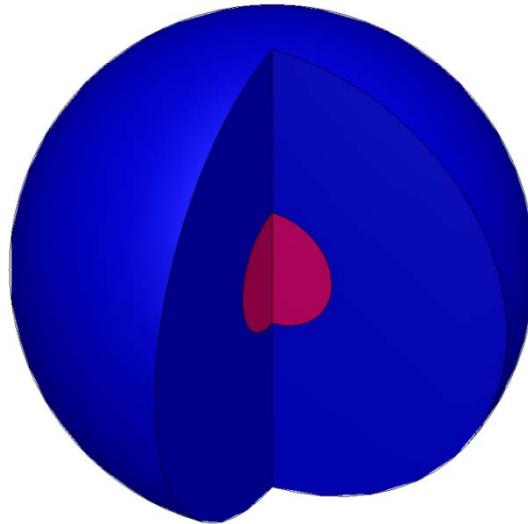
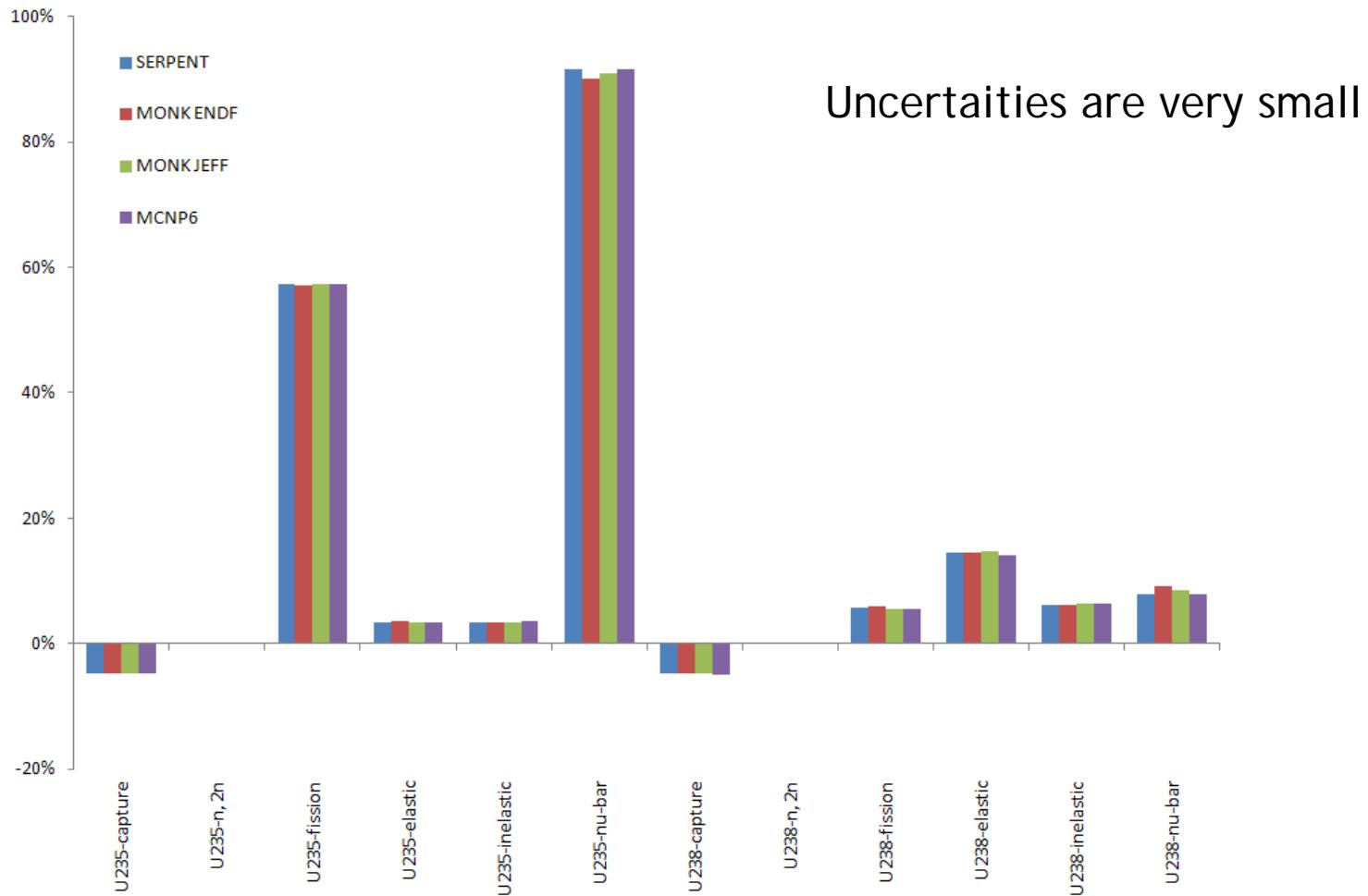


Figure 3. The HEU Sphere.

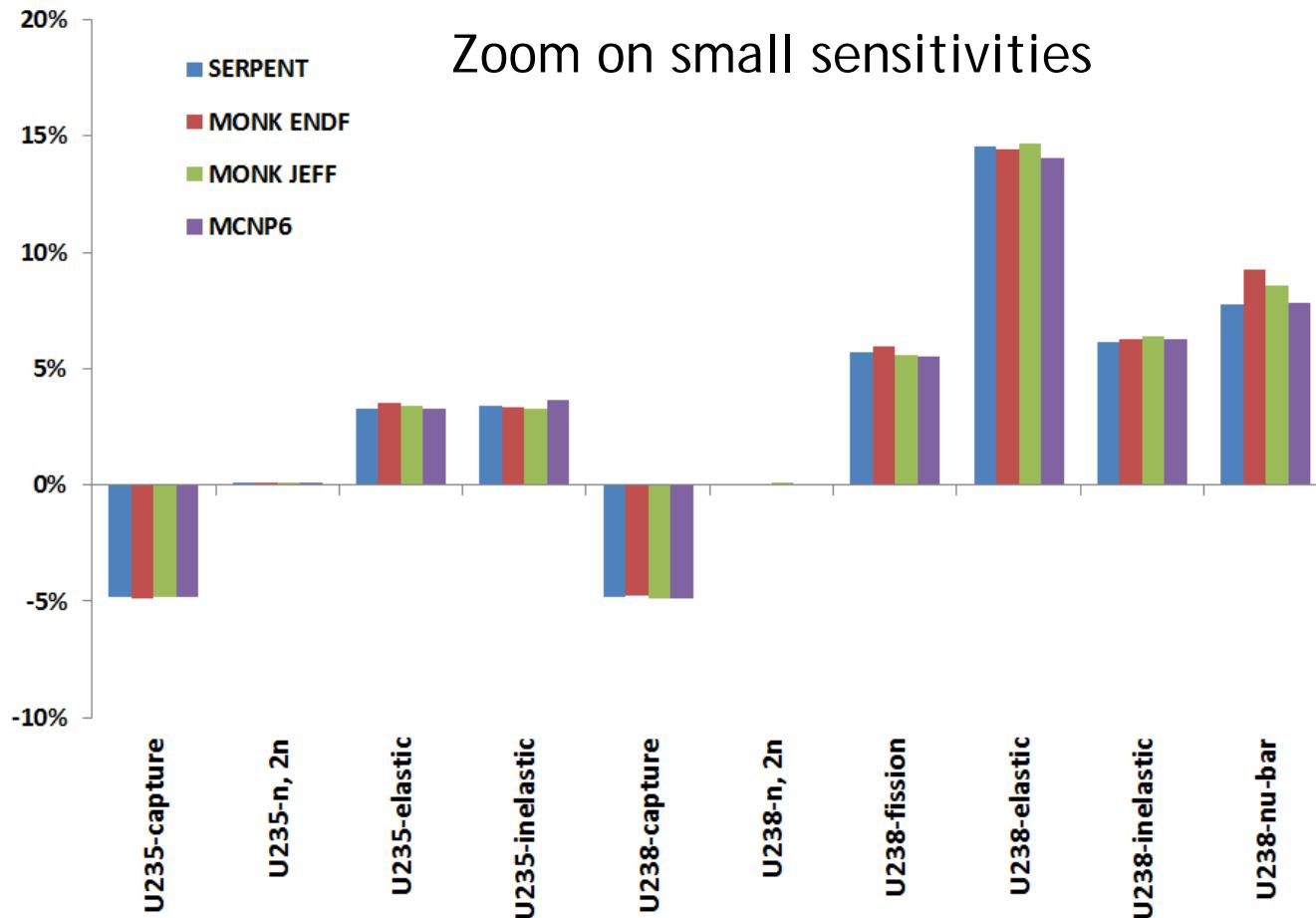
# Topsy: Integrated Sensitivities (1/3)

	SERPENT	MONK ENDF	MONK JEFF	MCNP6
U235-capture	-4,79	-4,87	-4,82	-4,84
U235-n, 2n	0,11	0,12	0,12	0,12
U235-fission	57,37	57,17	57,32	57,41
U235-elastic	3,30	3,54	3,43	3,30
U235-inelastic	3,39	3,34	3,28	3,63
U235-nu-bar	91,56	90,10	90,88	91,53
U238-capture	-4,83	-4,74	-4,88	-4,90
U238-n, 2n	0,07	0,05	0,08	0,04
U238-fission	5,72	5,95	5,61	5,54
U238-elastic	14,54	14,43	14,65	14,07
U238-inelastic	6,12	6,24	6,36	6,28
U238-nu-bar	7,78	9,23	8,57	7,81

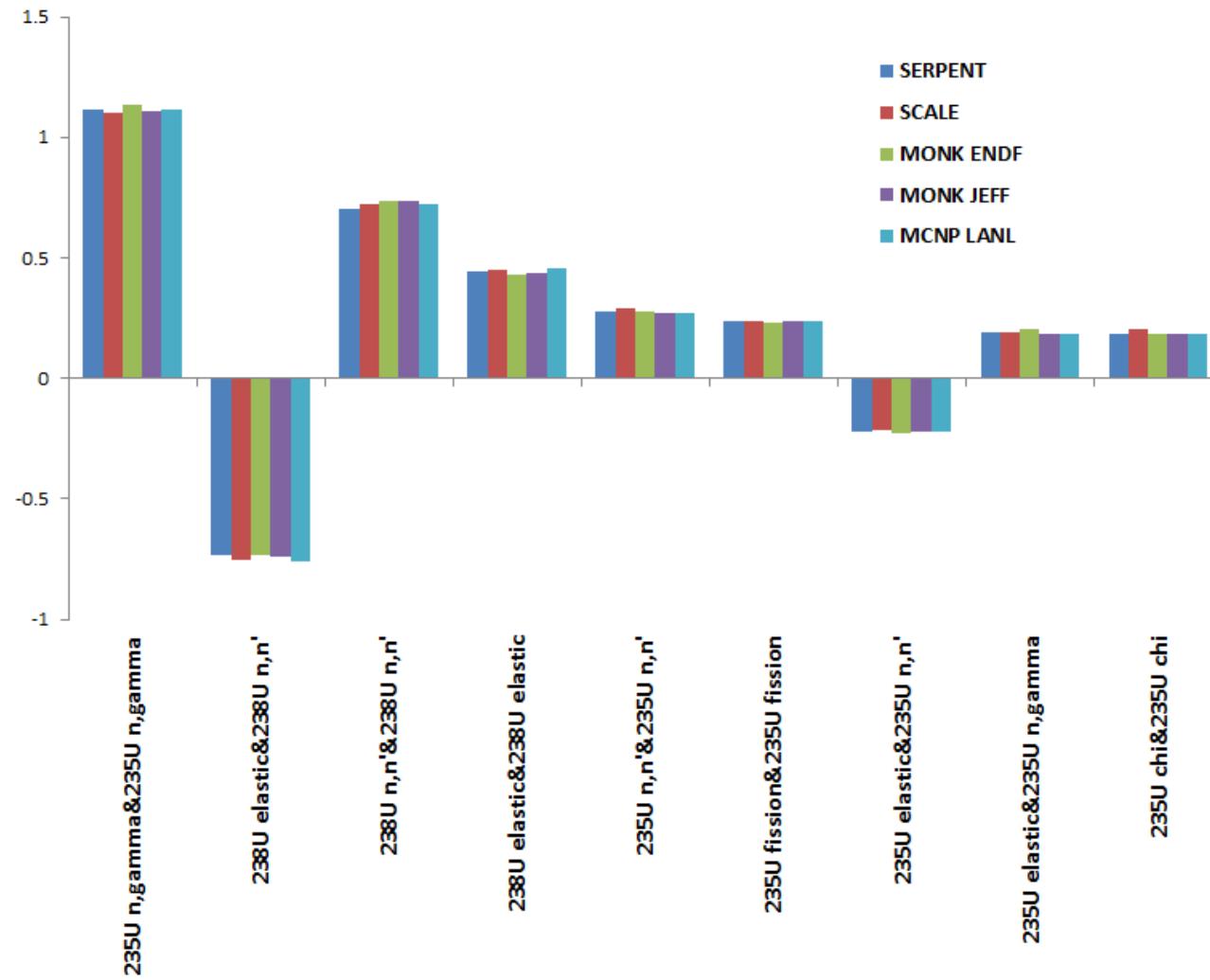
# Topsy: Integrated Sensitivities (2/3)



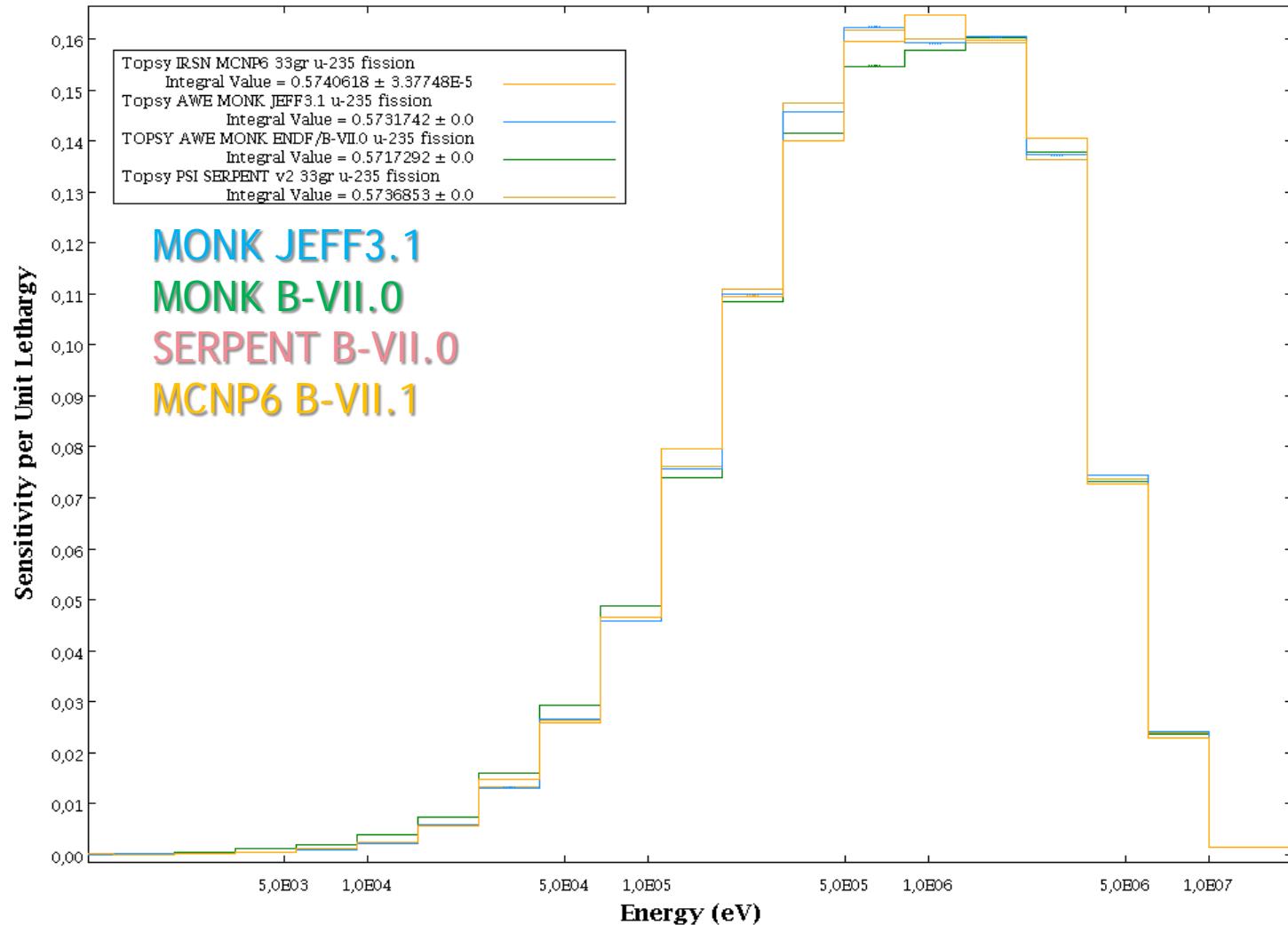
# Topsy: Integrated Sensitivities (3/3)



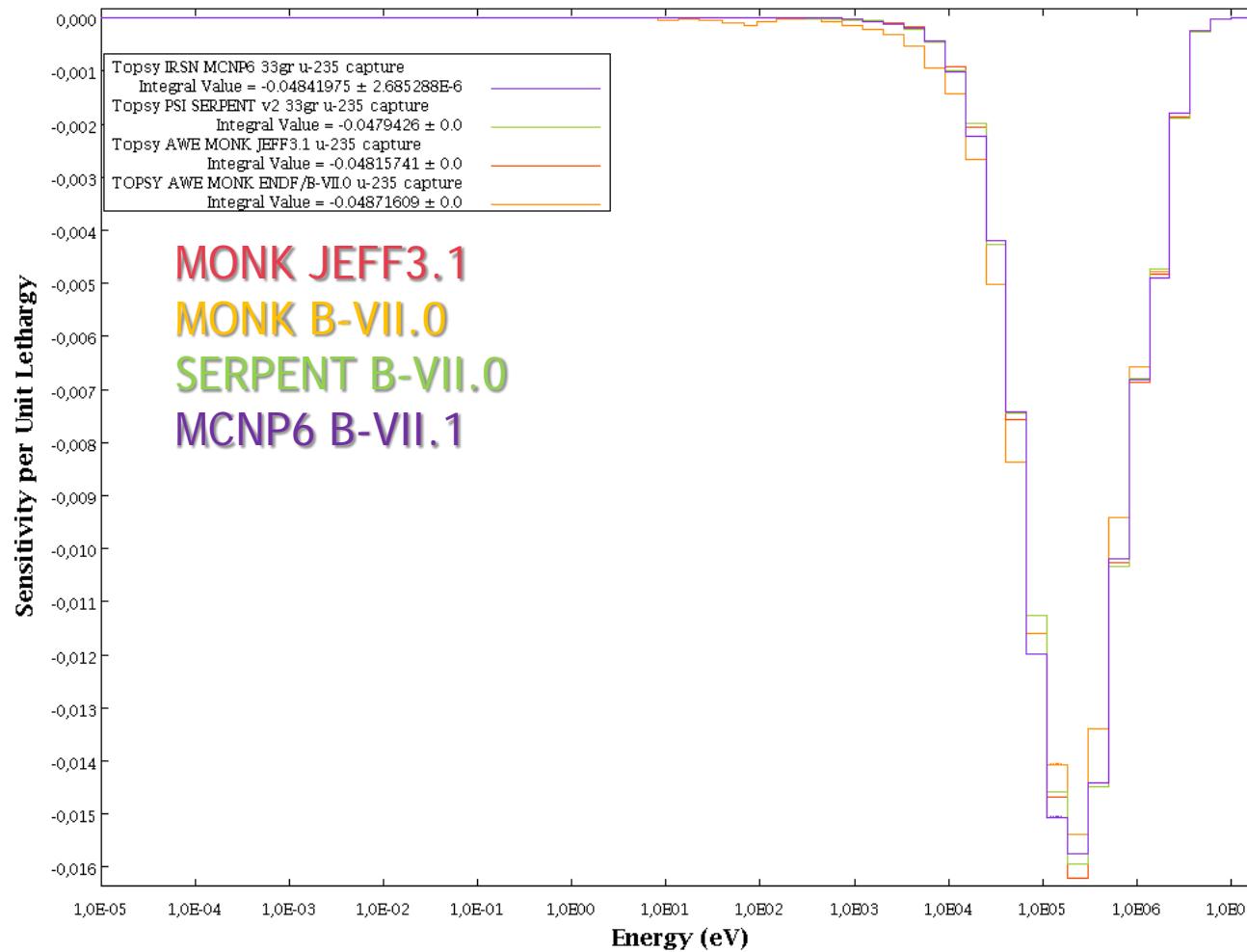
# Topsy: Uncertainties by reactions



# Topsy: U-235 Fission Profile



# Topsy: U-235 Capture Profile



# HMI-001 (ZPR 9/34 loading 303)

- Highly enriched uranium/ iron benchmark, moderated, reflected by steel. RZ model
- $k_{\text{bench}} = 0.9966 \pm 0.0026$
- $^{56}\text{Fe-tot}$  sensitivity in core = 0.0785, in reflector = 0.0166(0.015)

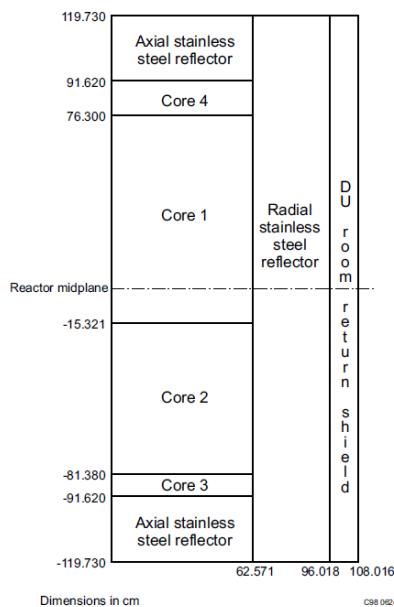


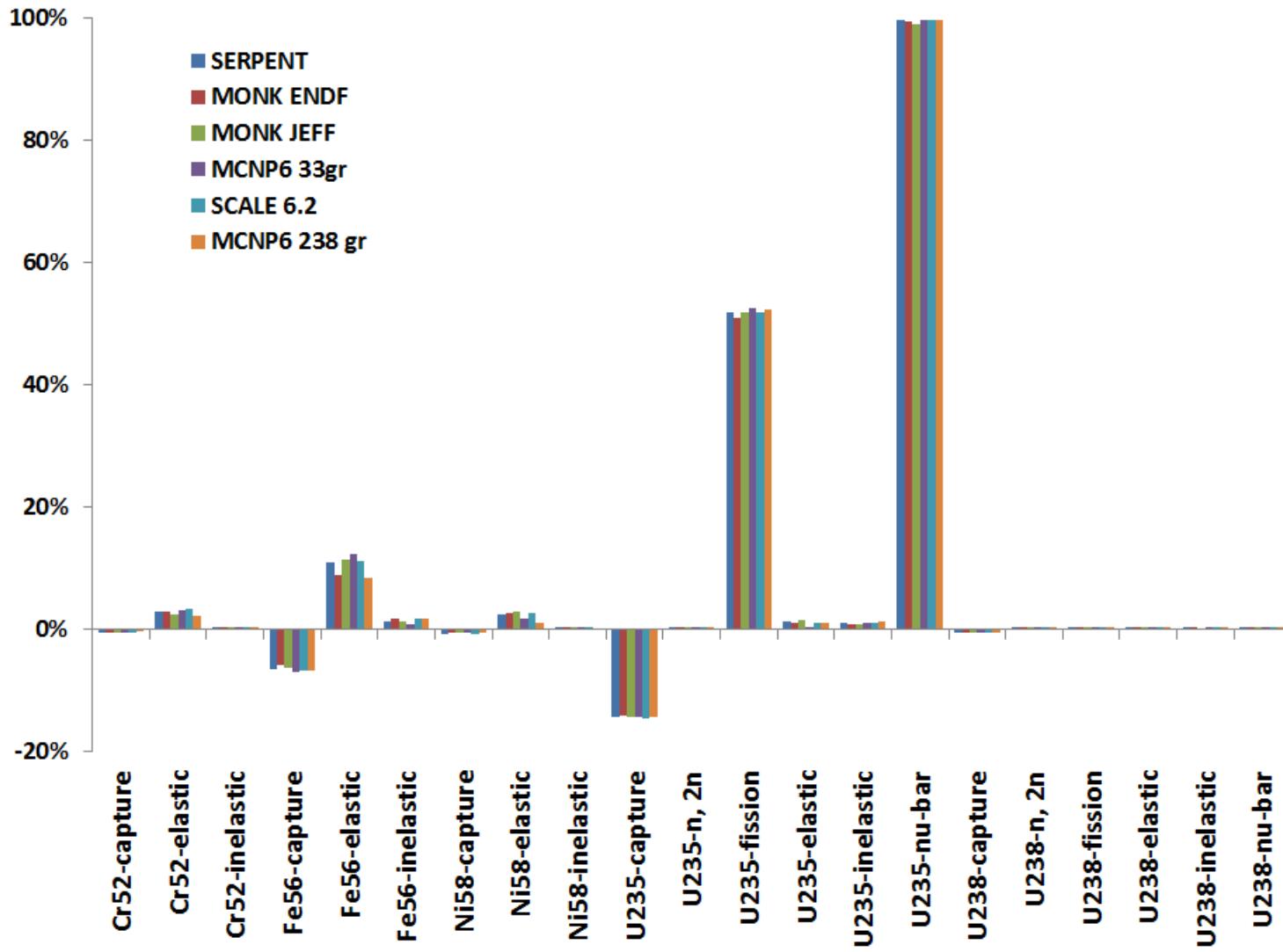
Figure 12. Benchmark Model Geometry.



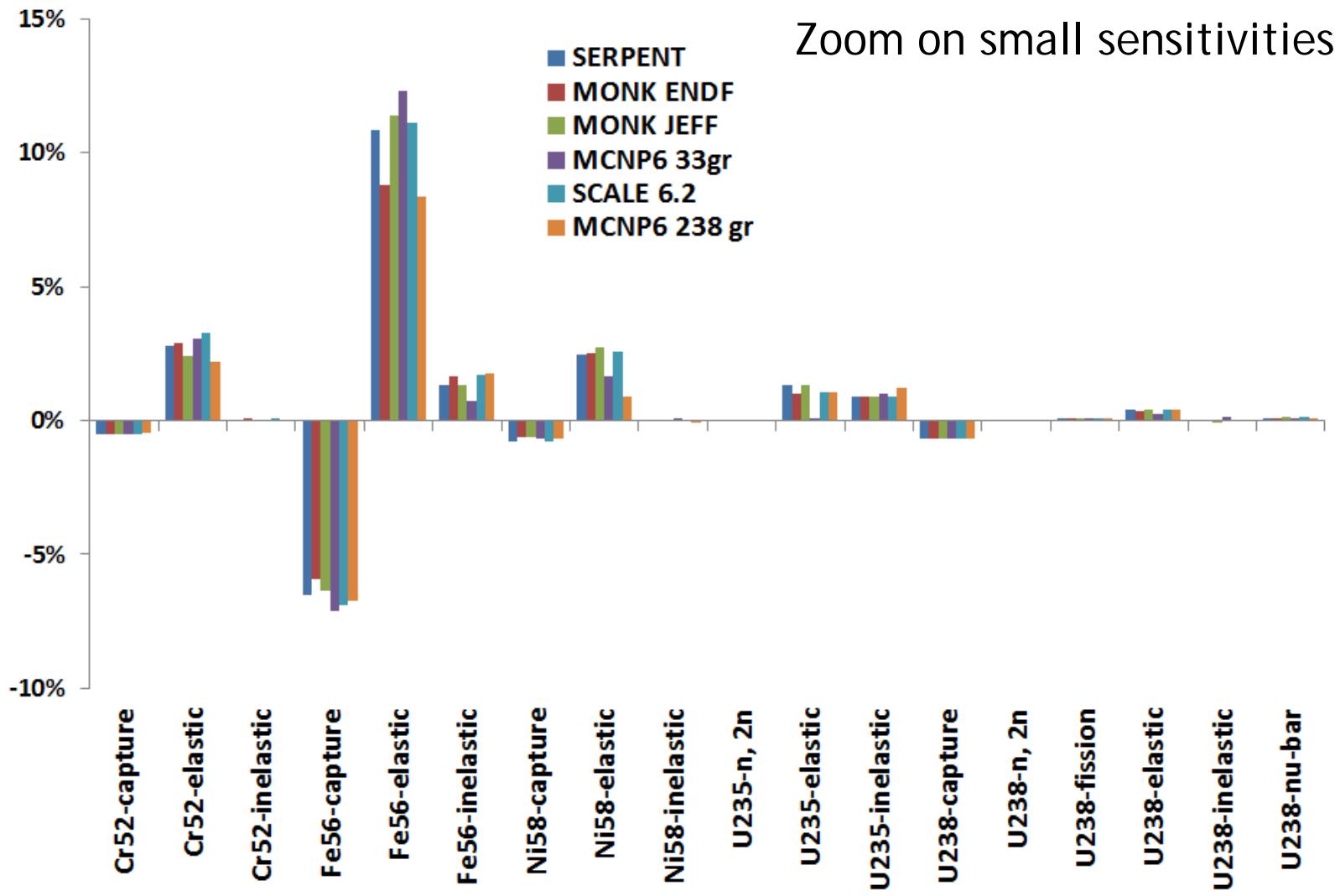
# ZPR-9/34: Integrates Sensitivities (1/3)

	SERPENT	MONK ENDF	MONK JEFF	MCNP6	SCALE 6.2	MCNP6 238 gr*
Cr52-capture	-0,53	-0,54	-0,52	-0,53	-0,52	-0,47
Cr52-elastic	2,76	2,91	2,40	3,04	3,26	2,22
Cr52-inelastic	0,05	0,09	0,03	0,04	0,08	0,04
Fe56-capture	-6,53	-5,95	-6,34	-7,11	-6,89	-6,75
Fe56-elastic	10,84	8,79	11,40	12,31	11,14	8,36
Fe56-inelastic	1,31	1,64	1,32	0,71	1,70	1,76
Ni58-capture	-0,78	-0,62	-0,64	-0,66	-0,77	-0,66
Ni58-elastic	2,47	2,51	2,75	1,66	2,55	0,90
Ni58-inelastic	0,02	0,01	0,03	0,07	0,02	-0,03
U235-capture	-14,45	-14,28	-14,42	-14,32	-14,54	-14,38
U235-n, 2n	0,01	0,01	0,01	0,02	0,01	0,00
U235-fission	51,83	50,79	51,82	52,54	51,85	52,29
U235-elastic	1,30	0,99	1,34	0,11	1,07	1,05
U235-inelastic	0,91	0,87	0,87	0,99	0,92	1,22
U235-nu-bar	99,71	99,42	99,04	99,72	99,71	99,71
U238-capture	-0,70	-0,68	-0,68	-0,69	-0,68	-0,67
U238-n, 2n	0,00	0,00	0,00	0,00	0,00	0,00
U238-fission	0,07	0,06	0,07	0,06	0,07	0,07
U238-elastic	0,41	0,36	0,39	0,23	0,39	0,41
U238-inelastic	0,01	0,02	-0,02	0,15	0,01	0,01
U238-nu-bar	0,11	0,08	0,12	0,10	0,11	0,11

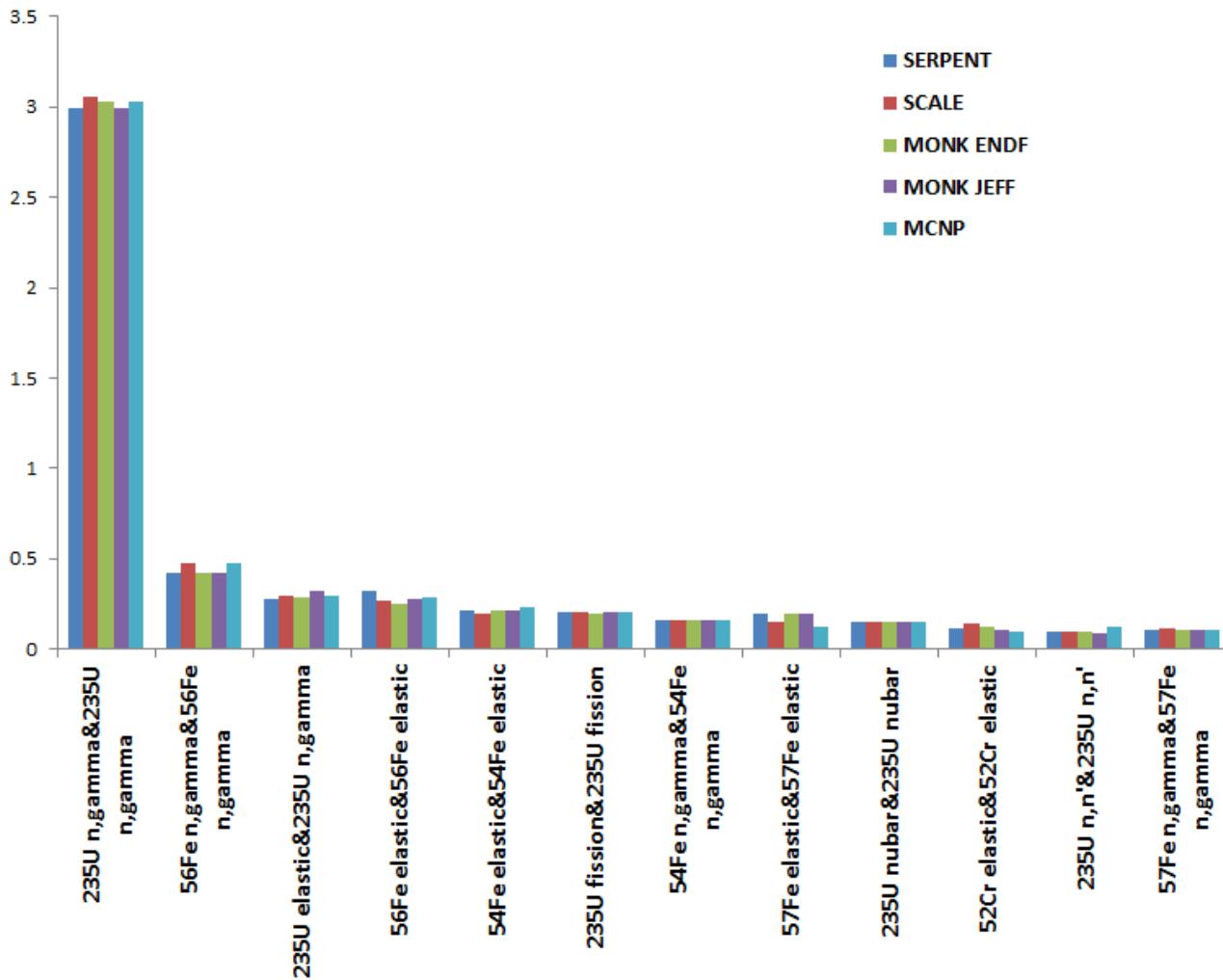
# ZPR-9/34: Integrates Sensitivities (2/3)



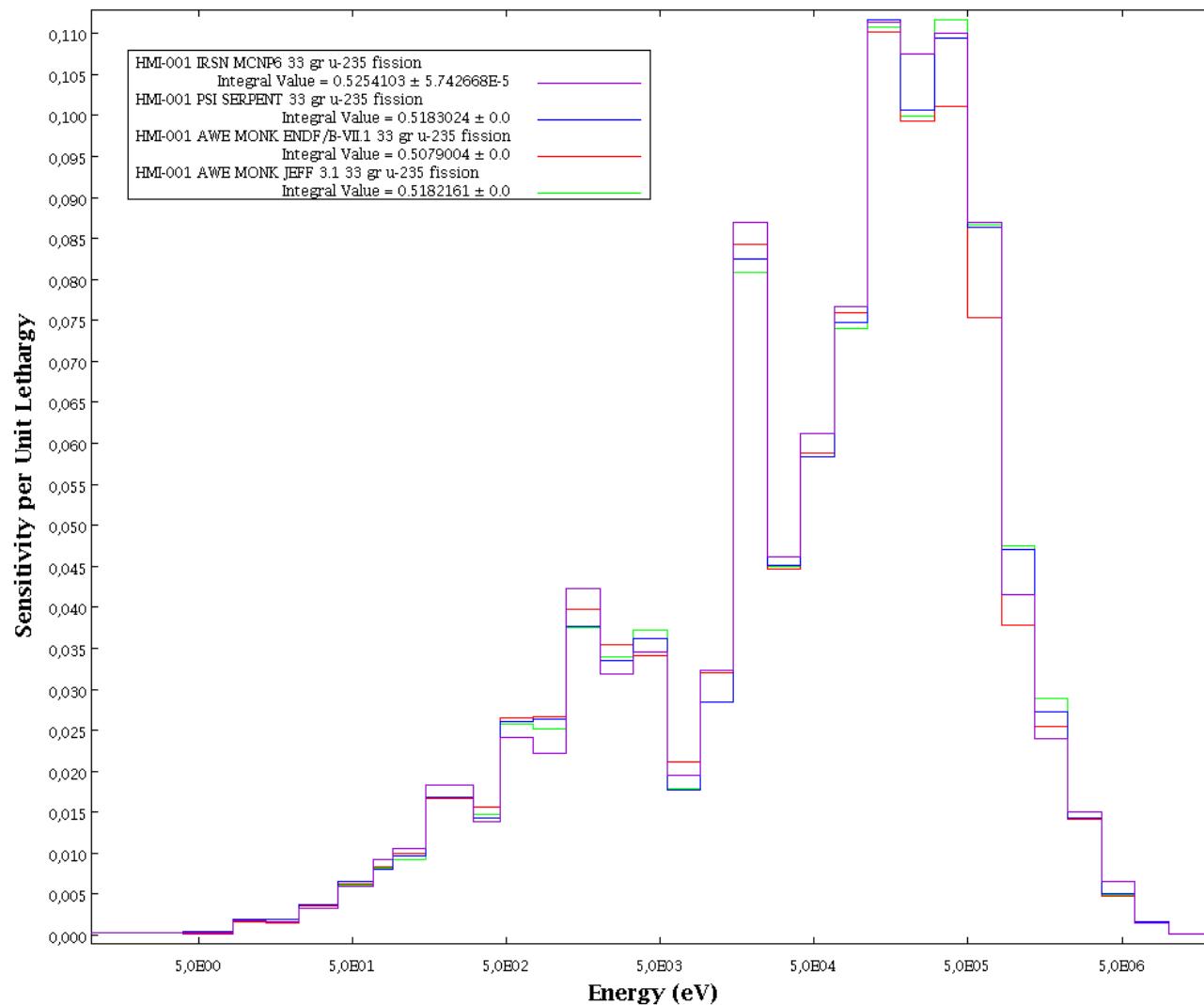
# ZPR-9/34: Integrates Sensitivities (3/3)



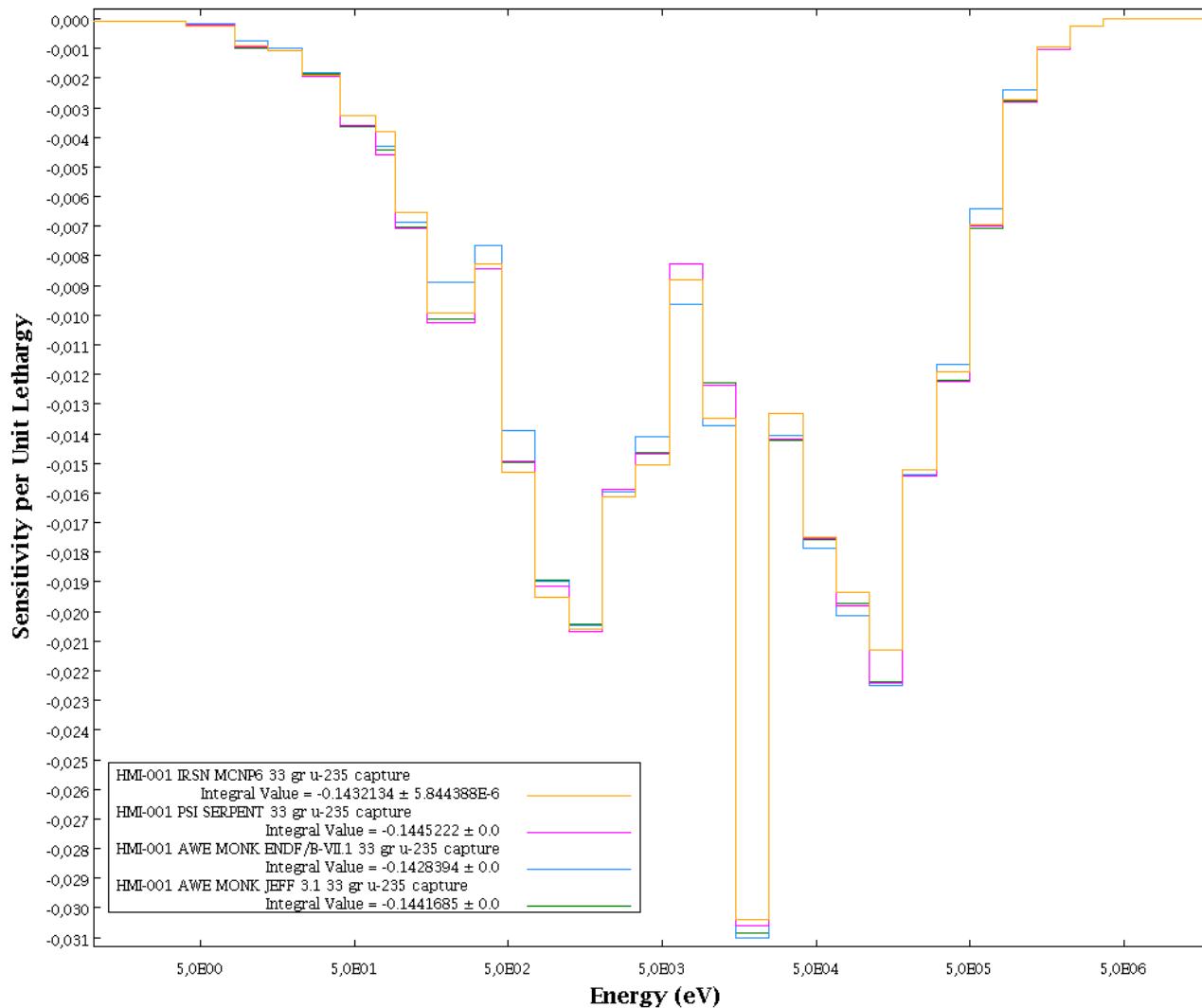
# ZPR 9/34: Uncertainties by reactions



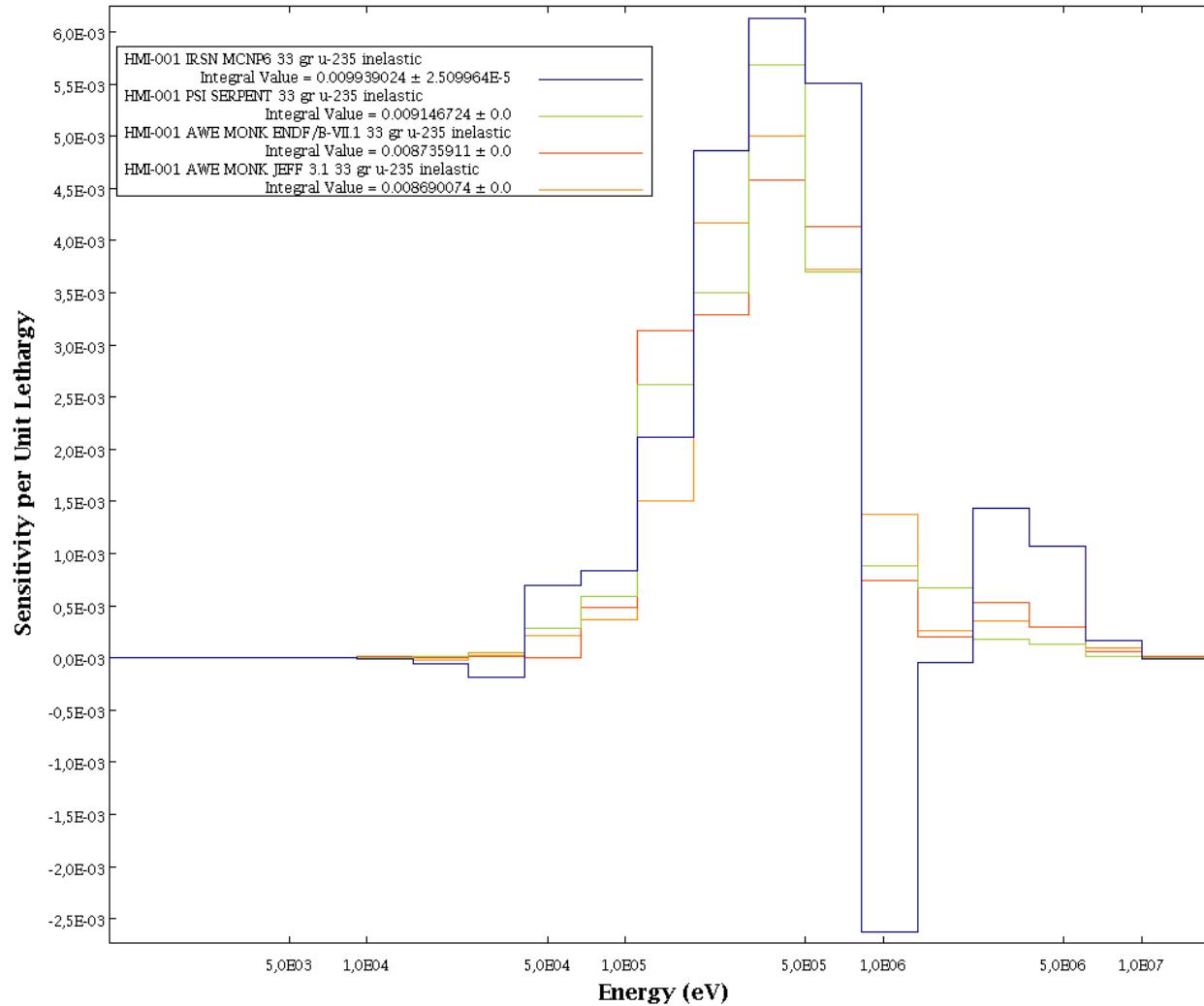
# ZPR 9/34: U-235 Fission Profiles



# ZPR 9/34: U-235 Capture Profiles



# ZPR 9/34: U-235 Inelastic Profiles



# PMI-002 (ZPR 6/10 loading 24)

- Core with heterogeneous plutonium metal fuel with carbon/stainless steel dilutions, and a steel reflector.
- $k_{\text{bench}} = 0.9862 \pm 0.0005$  ( $k_{\text{ZPR6/10}} = 1.0009 \pm 0.0007$ )

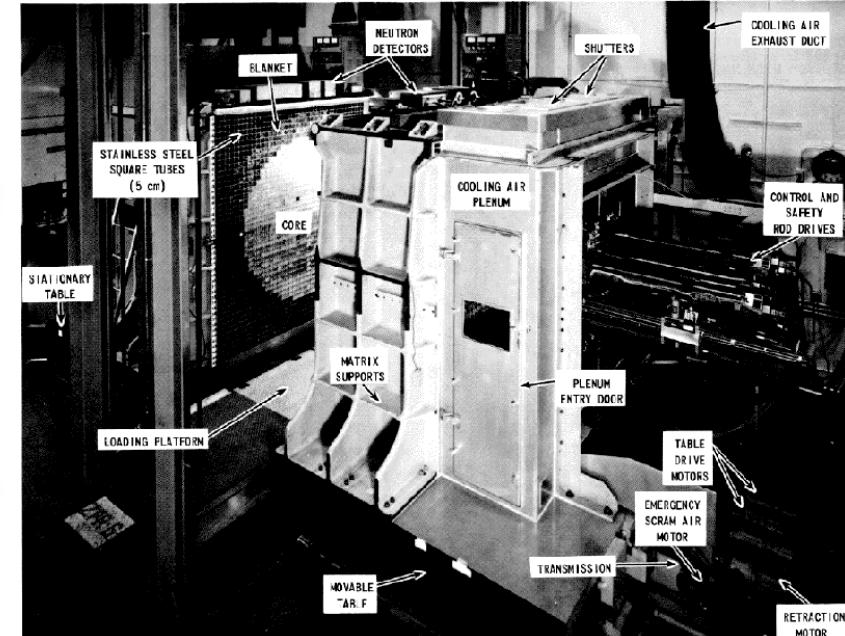
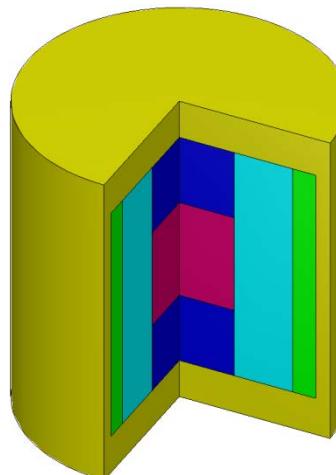
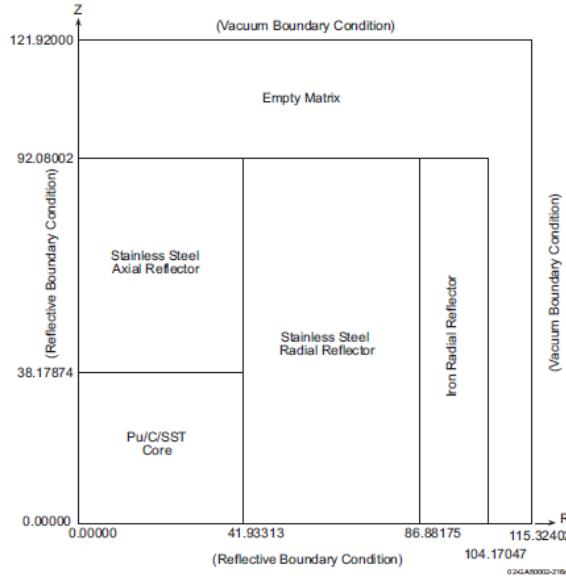
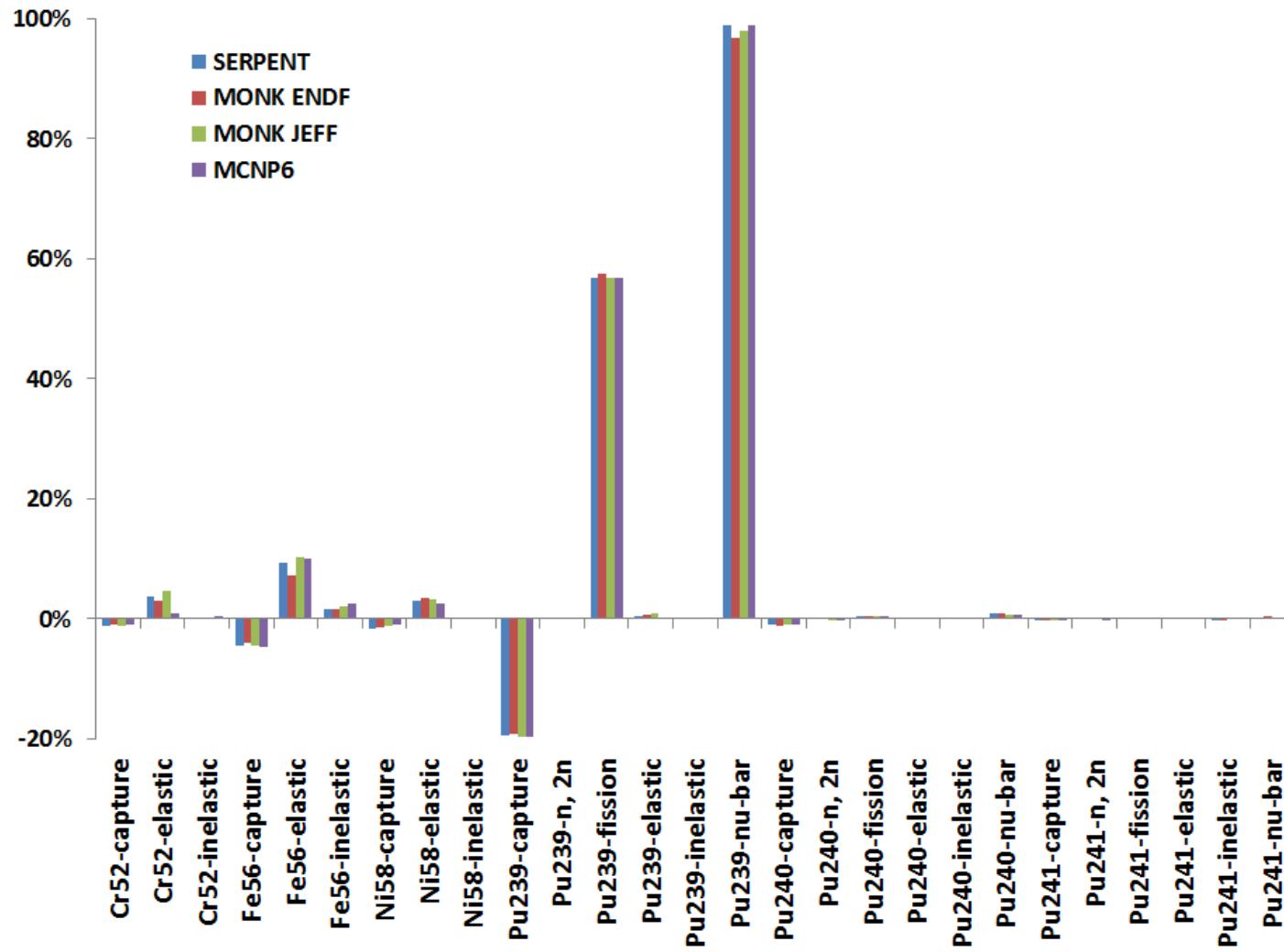


Figure 6. Benchmark-Model Geometry for ZPR-6/10.

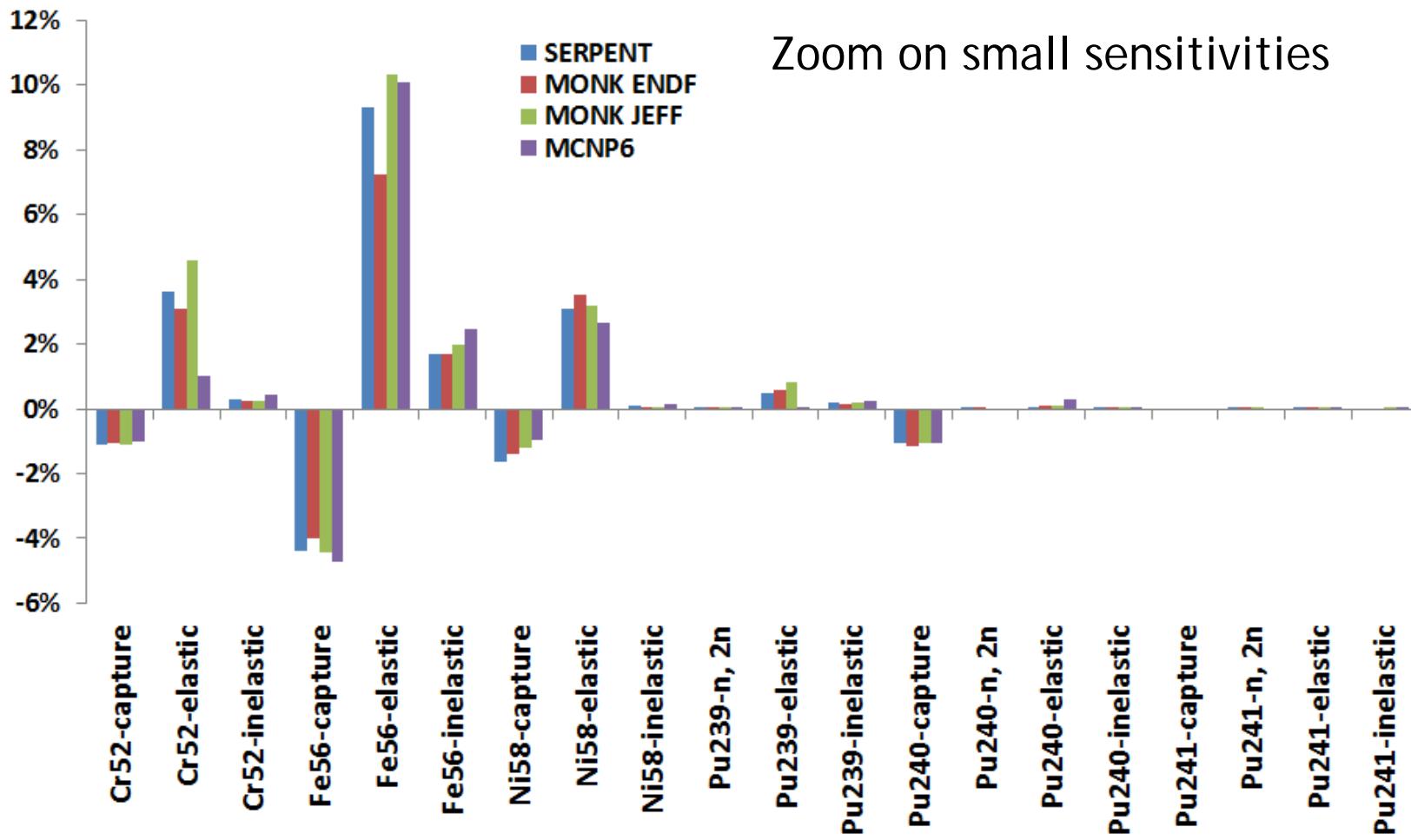
# ZPR 6/10: Integrated Sensitivities (1/3)

	SERPENT	MONK ENDF	MONK JEFF	MCNP6
Cr52-capture	-1,10	-1,06	-1,11	-0,99
Cr52-elastic	3,61	3,09	4,57	1,02
Cr52-inelastic	0,30	0,26	0,23	0,46
Fe56-capture	-4,39	-4,00	-4,45	-4,72
Fe56-elastic	9,33	7,24	10,34	10,11
Fe56-inelastic	1,69	1,72	1,99	2,46
Ni58-capture	-1,63	-1,37	-1,18	-0,98
Ni58-elastic	3,08	3,51	3,18	2,65
Ni58-inelastic	0,09	0,05	0,04	0,13
Pu239-capture	-19,42	-19,17	-19,58	-19,78
Pu239-n, 2n	0,01	0,00	0,01	0,01
Pu239-fission	56,78	57,41	56,82	56,81
Pu239-elastic	0,50	0,60	0,84	0,03
Pu239-inelastic	0,18	0,15	0,20	0,25
Pu239-nu-bar	98,91	96,80	97,98	98,93
Pu240-capture	-1,04	-1,14	-1,05	-1,05
Pu240-n, 2n	0,00	0,00	0,00	0,00
Pu240-fission	0,53	0,49	0,51	0,52
Pu240-elastic	0,05	0,11	0,10	0,28
Pu240-inelastic	0,00	0,04	0,03	0,01
Pu240-nu-bar	0,80	0,93	0,73	0,79
Pu241-capture	-0,03	-0,02	-0,03	-0,02
Pu241-n, 2n	0,00	0,00	0,00	0,00
Pu241-fission	0,14	0,14	0,15	0,14
Pu241-elastic	0,00	0,01	0,00	0,00
Pu241-inelastic	0,00	-0,01	0,00	0,01
Pu241-nu-bar	0,25	0,38	0,25	0,24

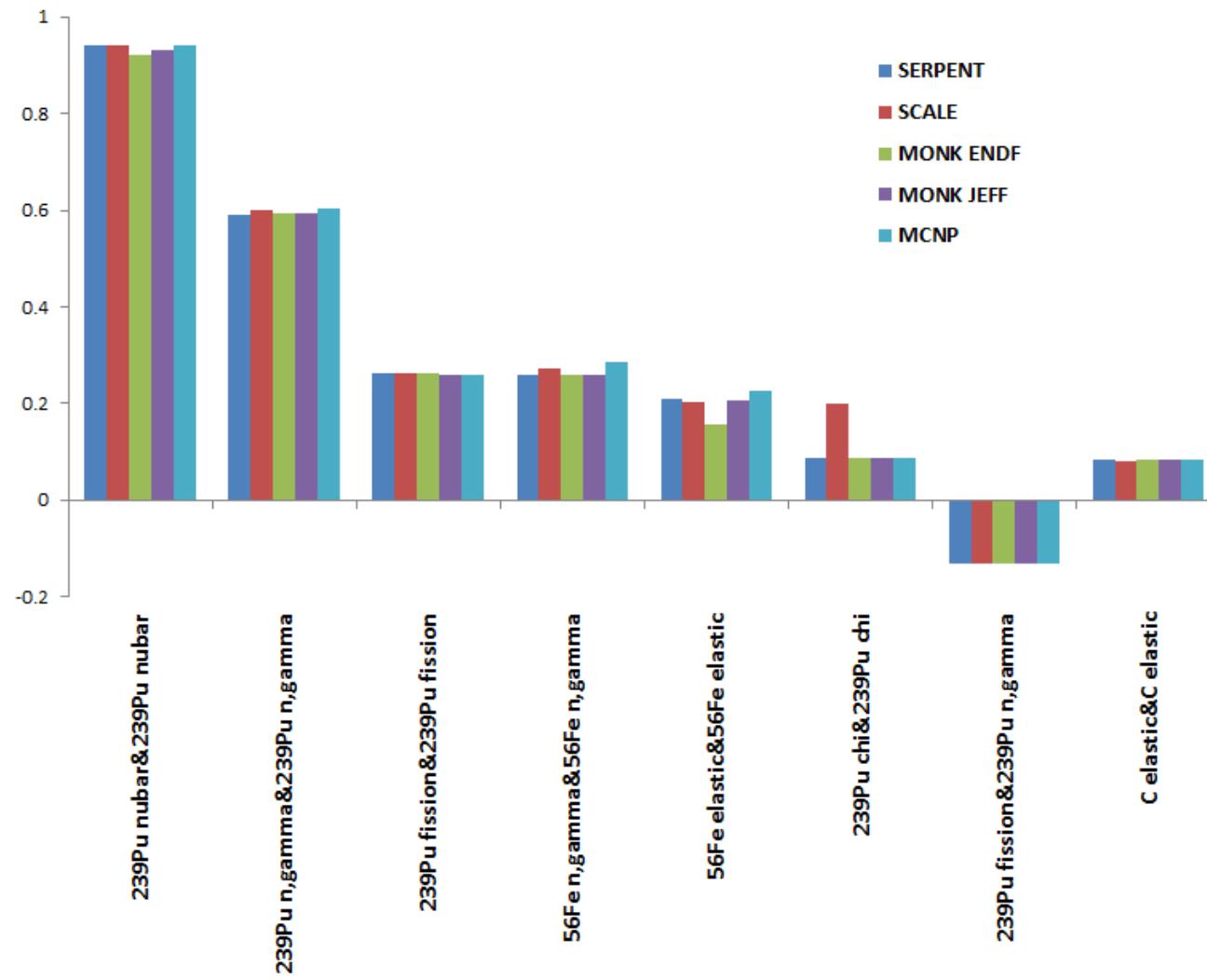
# ZPR 6/10: Integrated Sensitivities (2/3)



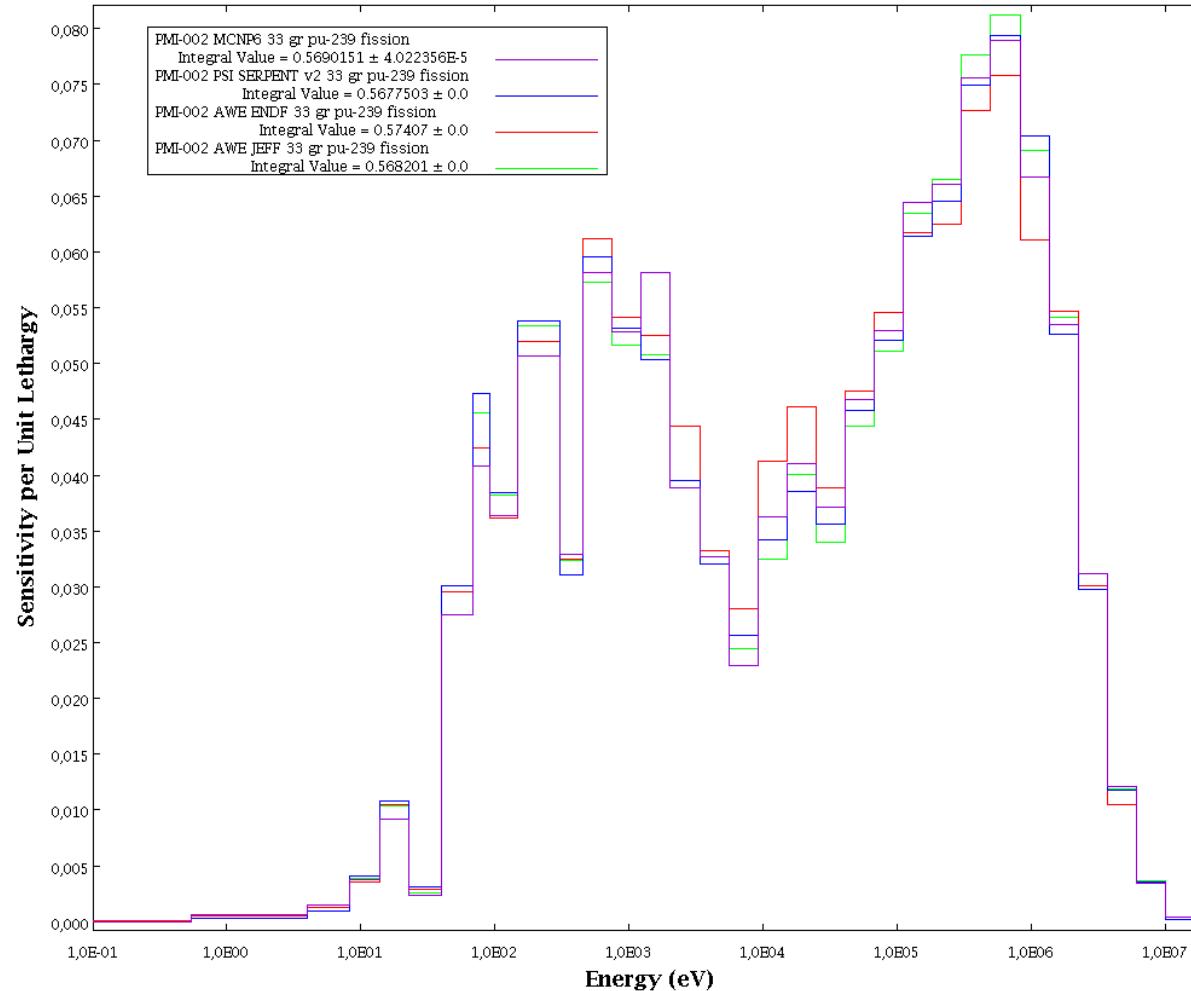
# ZPR 6/10: Integrated Sensitivities (3/3)



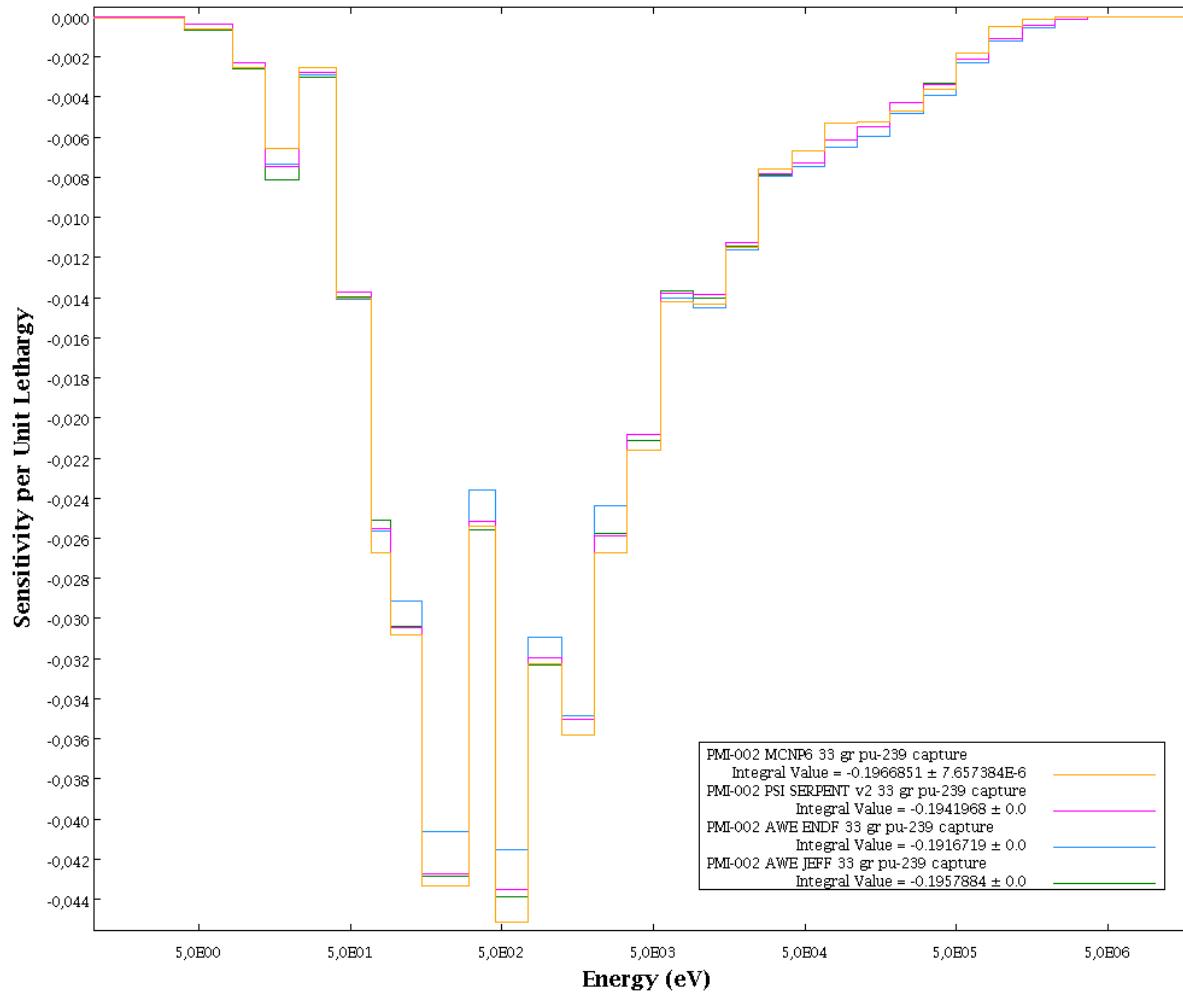
# ZPR 6/10: Uncertainties by reactions



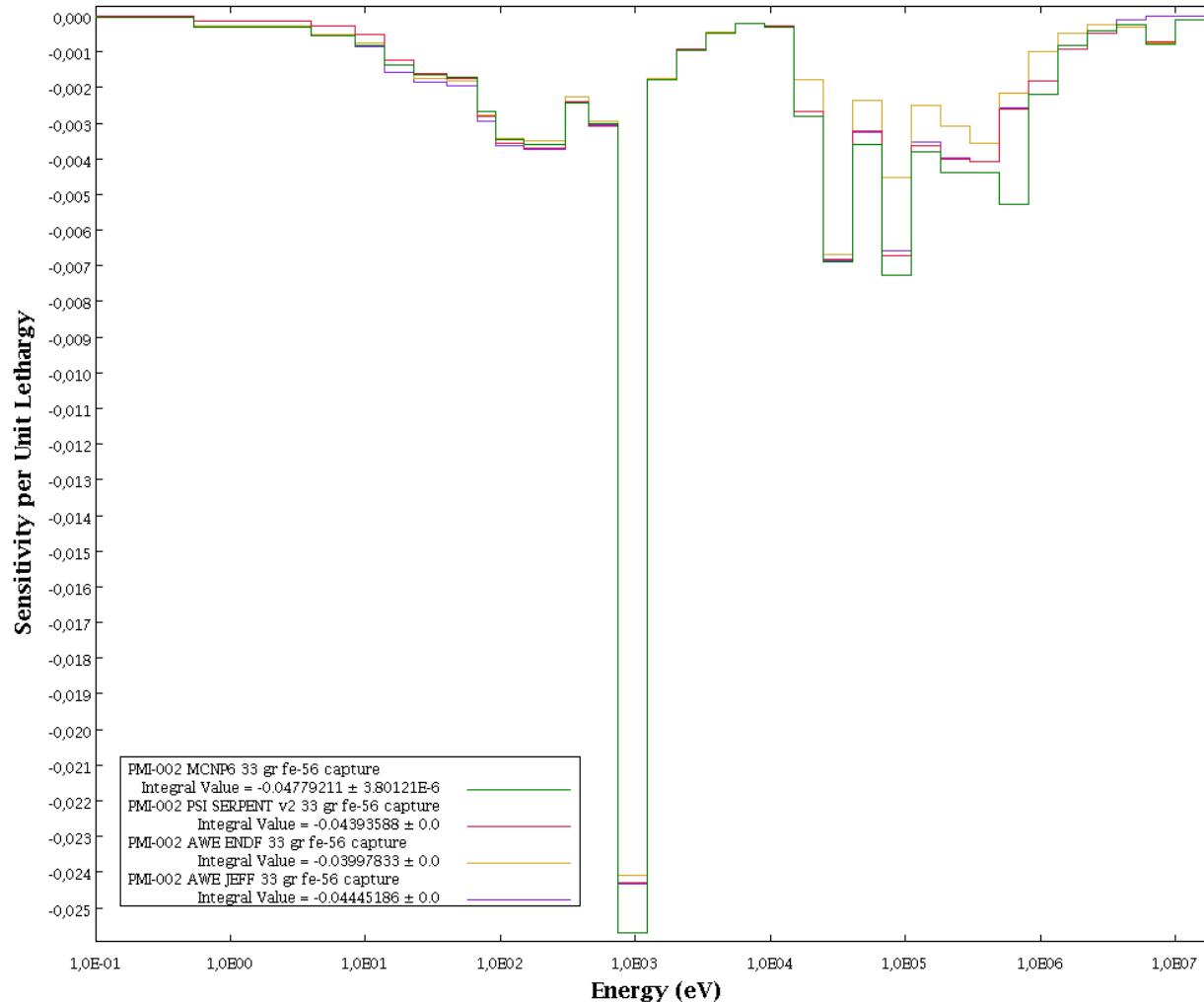
# ZPR 6/10: Pu-239 Fission Profiles



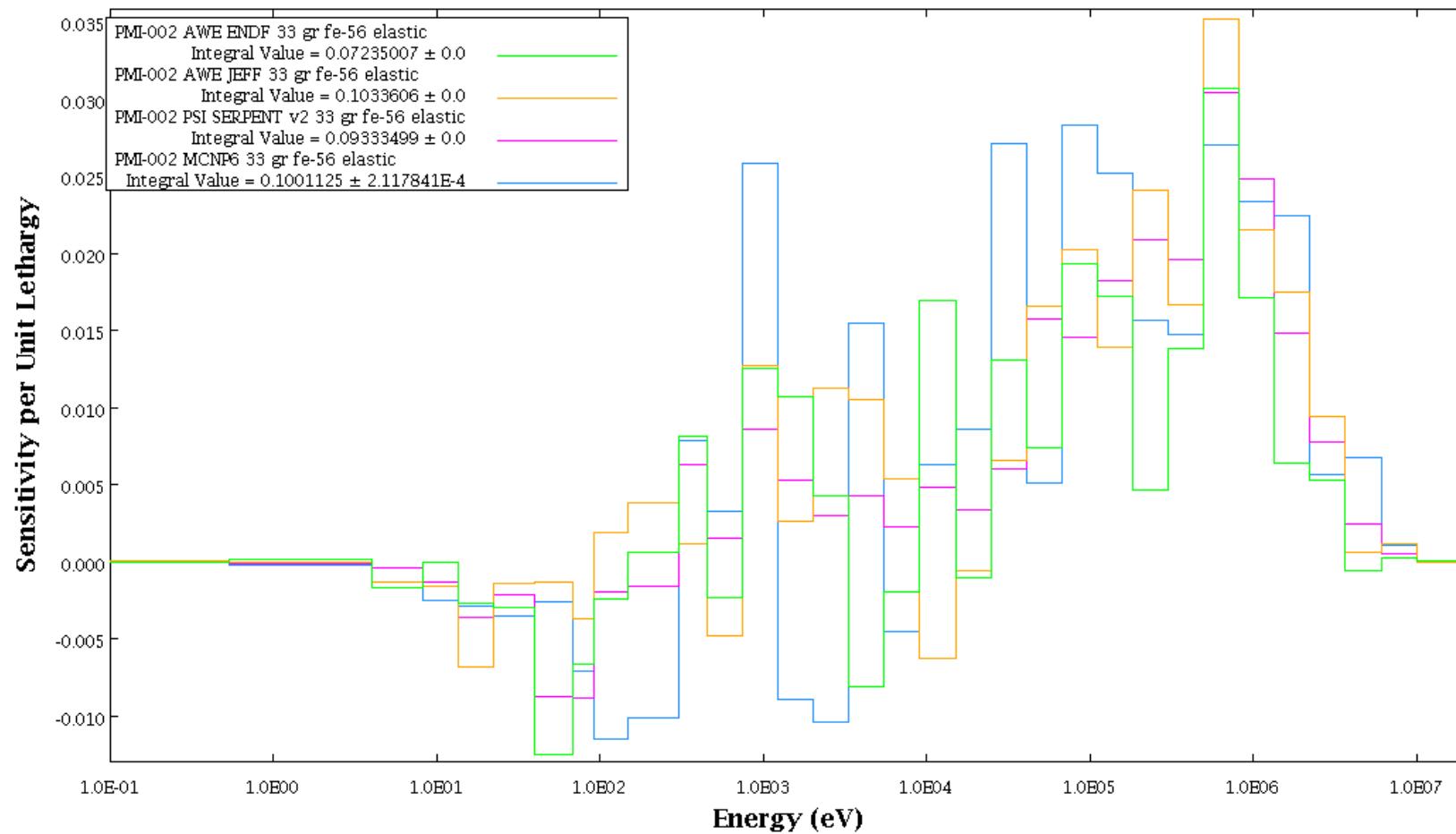
# ZPR 6/10: Pu-239 Capture Profiles



# ZPR 6/10: Fe-56 Capture Profiles



# ZPR 6/10: Fe-56 Elastic Profiles



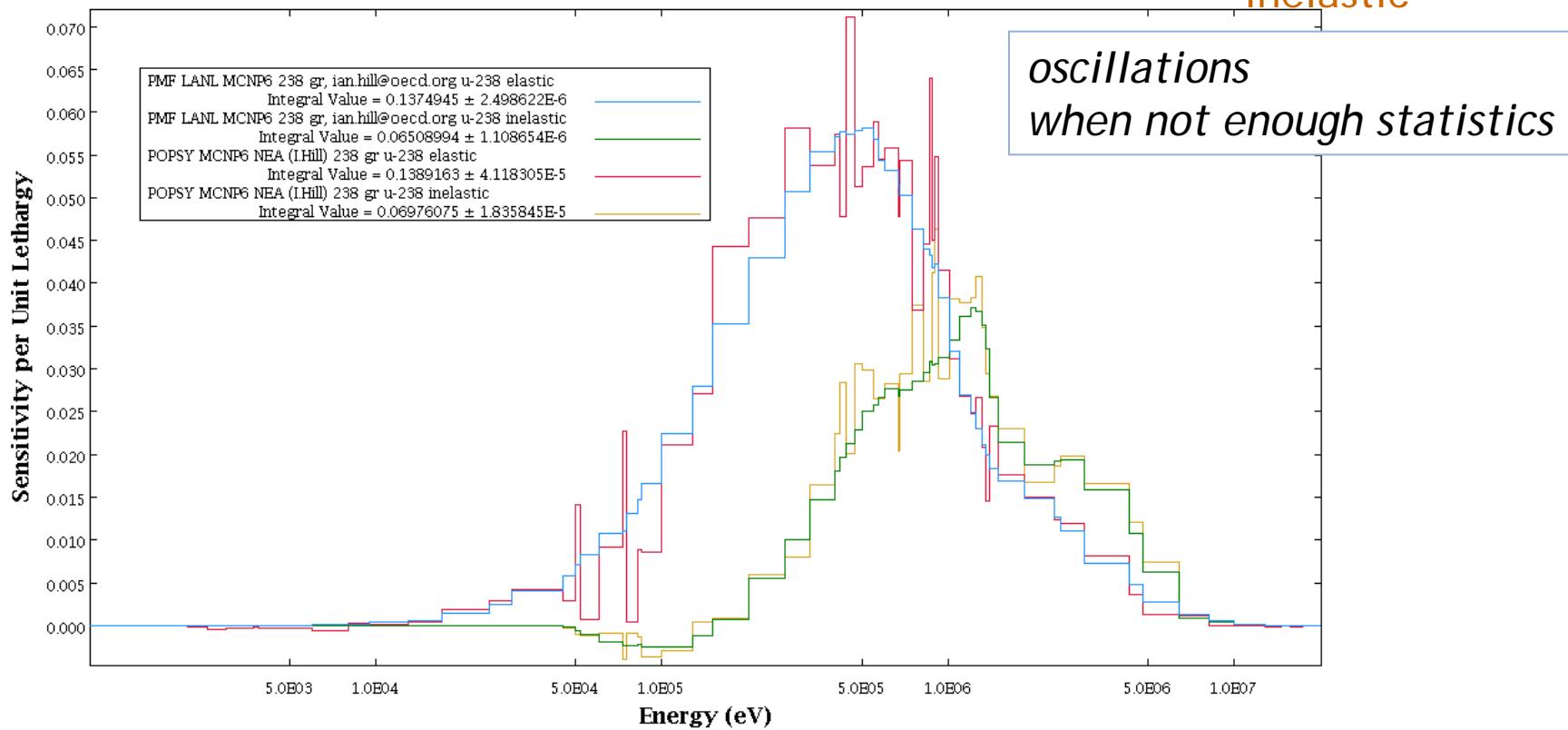
# Convergence Issues

- | Oscillations in sensitivity profiles (MCNP6 example) - addressed
- | Optimization of sensitivity algorithms acceleration (CLUTCH example) - addressed
- | Negative n,2n contributions

# Popsy: MCNP6 Convergence

MCNP6/ENDF/B-VII.1 5B histories (500000×10000) u-238 elastic  
(Results provided by B. Kiedrowski) inelastic

MCNP6/ENDF/B-VII.1 1.2M histories (2000×600) u-238 elastic  
inelastic



## E. Tsvetkov EMPIRICAL TESTING OF SOME PSEUDO-RANDOM NUMBERS GENERATORS/ Mathematical Modeling, v 23, #5, pp.81-94, 2011

Empirical testing of statistical properties of some pseudo-random numbers generators based on a partition of the unit hypercube with dimension from 1 to 15 was performed. Some CLHEP library pseudo-random numbers generators, Mersenne Twister generator and MCNP generator were tested. The results of tests allowed to determine the parts of the pseudo-random numbers sequences with bad statistical properties. The easy recoverable defects of two CLHEP generators were found.

$$I = \lim_{n \rightarrow \infty} S_n, \quad \mathbf{r}_1 = (x_1, x_2, \dots, x_k), \mathbf{r}_2 = (x_{K+1}, x_{K+2}, \dots, x_{K+k}), \dots,$$

$$S_n = \frac{V}{n} \sum_{i=1}^n f(\mathbf{r}_i), \quad \mathbf{r}_n = (x_{(n-1)K+1}, x_{(n-1)K+2}, \dots, x_{(n-1) \cdot K + k}), \dots,$$

$$\chi^2 = \frac{1}{MX} \sum_{i=1}^{S^k} (X_i - MX)^2$$

# E. Tsvetkov EMPIRICAL TESTING OF SOME PSEUDO-RANDOM NUMBERS GENERATORS/ Mathematical Modeling, v 23, #5, pp.81-94, 2011

	1	2	3	4	5	6	7	8	9	10
CLHEP::DualRand	<b>0.995323</b>	0.948053	0.340351	0.768940	0.987268	<b>0.998447</b>	0.947438	0.794921	0.865710	0.981127
CLHEP::HepJamesRandom	<b><u>1.000000</u></b>	0.699740	0.936632	0.966977	0.886762	0.928390	0.948037	0.874440	0.531962	0.831159
CLHEP::Hurd160Engine	0.981242	0.971623	0.958399	0.631339	0.863938	0.867428	0.974473	0.694394	0.906157	0.928675
CLHEP::Hurd288Engine	0.559912	0.792181	0.509890	0.757253	<b>0.999971</b>	0.976666	0.931154	<b>0.994599</b>	0.953089	0.946499
CLHEP::MTwistEngine	<b>0.994270</b>	0.946652	0.974972	0.899679	0.752039	0.944401	0.947856	0.951318	0.878380	0.871078
CLHEP::RanecuEngine	<b>0.998975</b>	<b>0.996958</b>	0.346334	0.709779	0.679632	0.900535	0.870693	0.705390	0.773634	0.619596
CLHEP::Ranlux64Engine	0.933658	0.874168	0.850137	0.974327	0.737928	0.960292	<b>0.997410</b>	0.917534	0.810551	<b>0.990689</b>
CLHEP::RanluxEngine	<b><u>1.000000</u></b>	0.642228	0.777547	0.841973	0.988477	0.908988	0.740307	0.493492	<b>0.999962</b>	0.937359
CLHEP::RanshiEngine	<b>0.993416</b>	0.707369	0.972229	0.910035	0.679360	0.921317	0.978640	0.977095	0.904776	0.934596
CLHEP::TripleRand	<b>0.995091</b>	0.398372	0.577427	<b>0.993931</b>	0.968364	0.962025	0.975680	0.988473	0.876030	0.983850
Matlab::twister	0.959231	0.702784	0.810525	0.569543	0.781814	0.982808	0.892043	0.864386	0.758089	0.882524
MersenneTwister	0.906981	0.939482	0.924331	0.906341	0.931654	0.652740	0.972370	0.123699	0.954542	0.881406
MCNP::rang	0.709312	<b>0.000000</b>	<b><u>1.000000</u></b>	<b>0.000000</b>	<b>0.000000</b>	<b>0.000000</b>	0.686396	<b>0.000000</b>	0.966349	<b><u>1.000000</u></b>
MCNP::rang, форм. (4), табл	0.887875	<b>0.000000</b>	<b><u>1.000000</u></b>	<b>0.000000</b>	0.000240	0.000170	0.716351	<b>0.000000</b>	0.447955	0.000460
MCNP::rang, форм. (4), табл	<b>0.992192</b>	0.895684	0.405542	0.701091	0.956045	0.970338	0.554682	0.974754	<b>0.997694</b>	0.809440

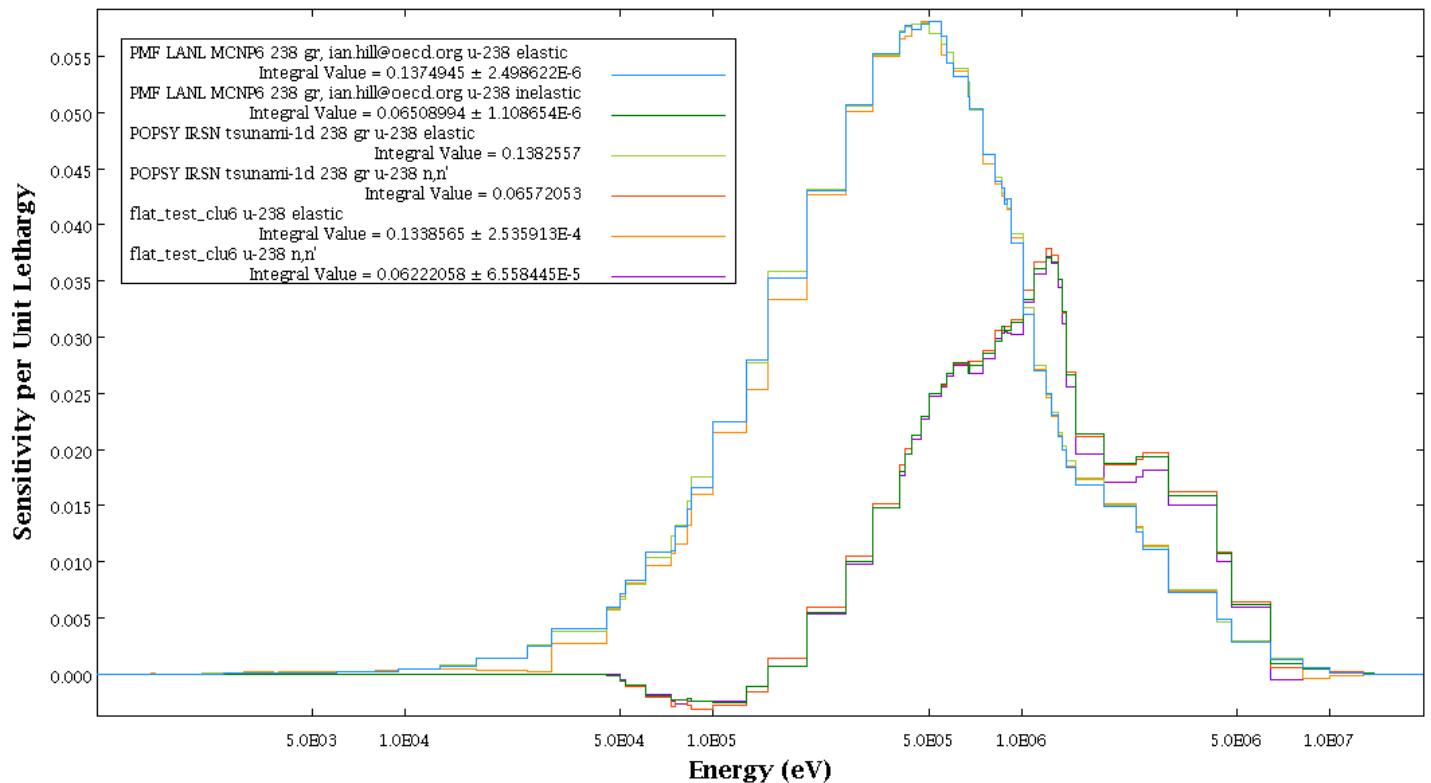
# Popsy: SCALE Convergence

MCNP6/ENDF/B-VII.1 5B histories (500000×10000) u-238

elastic  
inelastic  
elastic  
inelastic  
elastic  
inelastic

SCALE 6.1/TSUNAMI-1D/ENDF/B-VII u-238

SCALE 6.2B/CLUTCH/ENDF/B-VII u-238

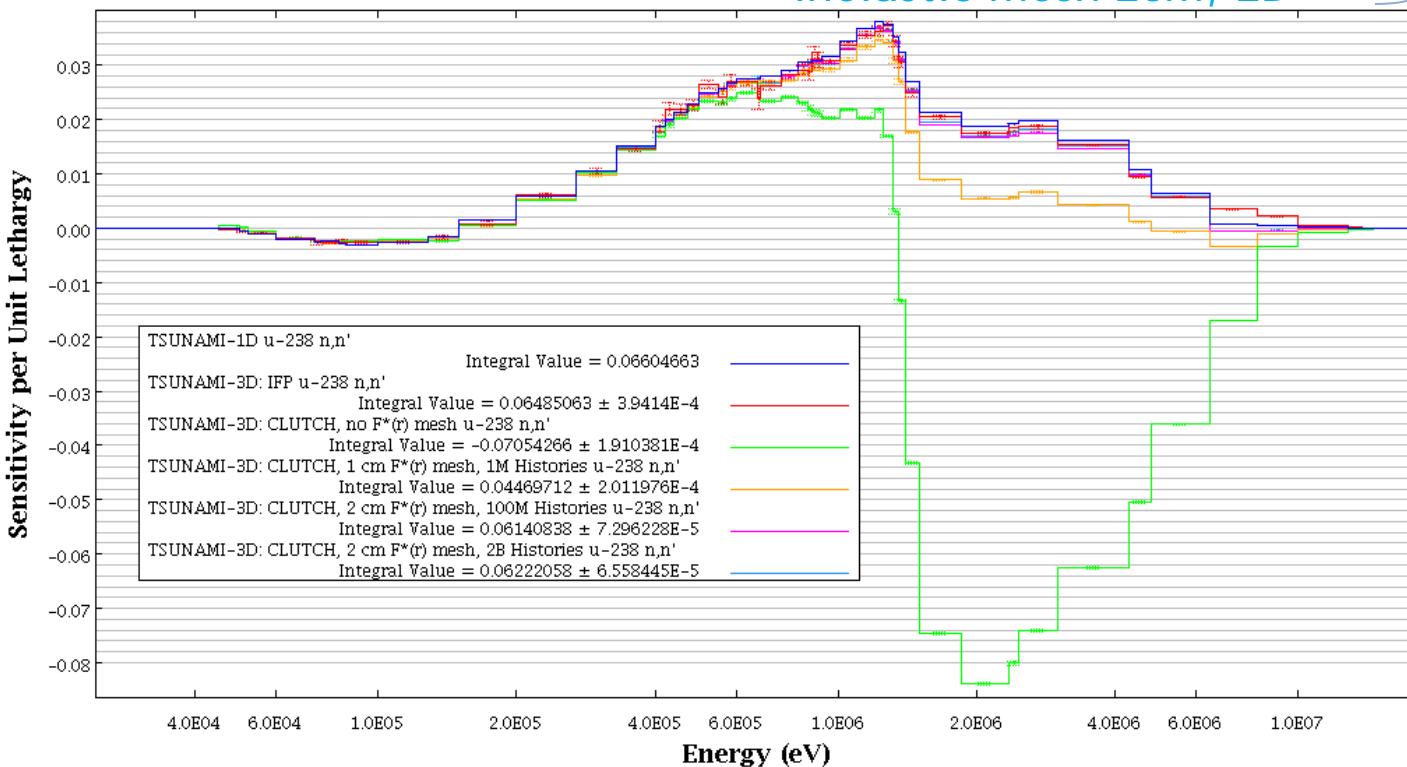


# Popsy: SCALE/CLUTCH Convergence

TSUNAMI-1D  
SCALE 6.2B IFP  
SCALE 6.2B CLUTCH

U-238    inelastic  
U-238    inelastic  
U-238    inelastic no mesh  
            inelastic mesh 1cm, 1M  
            inelastic mesh 2cm, 100M  
            inelastic mesh 2cm, 2B

C.Perfetti/  
ORNL



# Notes on MC Sensitivity Theory

$$k_{ef} \cdot Q(\mathbf{r}) = \int Q(\mathbf{r}') \cdot P(\mathbf{r}' \rightarrow \mathbf{r}) \cdot d\mathbf{r}'$$

$$k^+_{ef} \cdot Q^+(\mathbf{r}) = \int Q^+(\mathbf{r}') \cdot P(\mathbf{r} \rightarrow \mathbf{r}') \cdot d\mathbf{r}'$$

$$\frac{\partial k_{ef}}{\partial \alpha} = \frac{\iint Q^+(\mathbf{r}) \cdot Q(\mathbf{r}') \cdot \frac{\partial}{\partial \alpha} P(\mathbf{r}' \rightarrow \mathbf{r}) \cdot d\mathbf{r}' \cdot d\mathbf{r}}{\int Q^+(\mathbf{r}) \cdot Q(\mathbf{r}) \cdot d\mathbf{r}}$$

$$F(x) = \frac{v \Sigma_f(\mathbf{r}, E)}{k_{\Phi} \Sigma_a(\mathbf{r}, E)} Q^+(\mathbf{r})$$

$$\frac{1}{k_{\Phi}} \frac{\partial k_{\Phi}}{\partial \alpha}$$

$$\int F(x) \left\{ \frac{\Sigma_a(\mathbf{r}, E)}{v \Sigma_f(\mathbf{r}, E)} \Psi(x) \frac{\partial}{\partial \alpha} \left[ \frac{v \Sigma_f(\mathbf{r}, E)}{\Sigma_t(\mathbf{r}, E)} \right] + \frac{\Sigma_a(\mathbf{r}, E)}{\Sigma_t(\mathbf{r}, E)} \frac{\partial}{\partial \alpha} \Psi(x) \right\} dx$$

$$\int F(x) \frac{\Sigma_a(\mathbf{r}, E)}{\Sigma_t(\mathbf{r}, E)} \Psi(x) dx$$

$$P(\mathbf{r}' \rightarrow \mathbf{r})$$

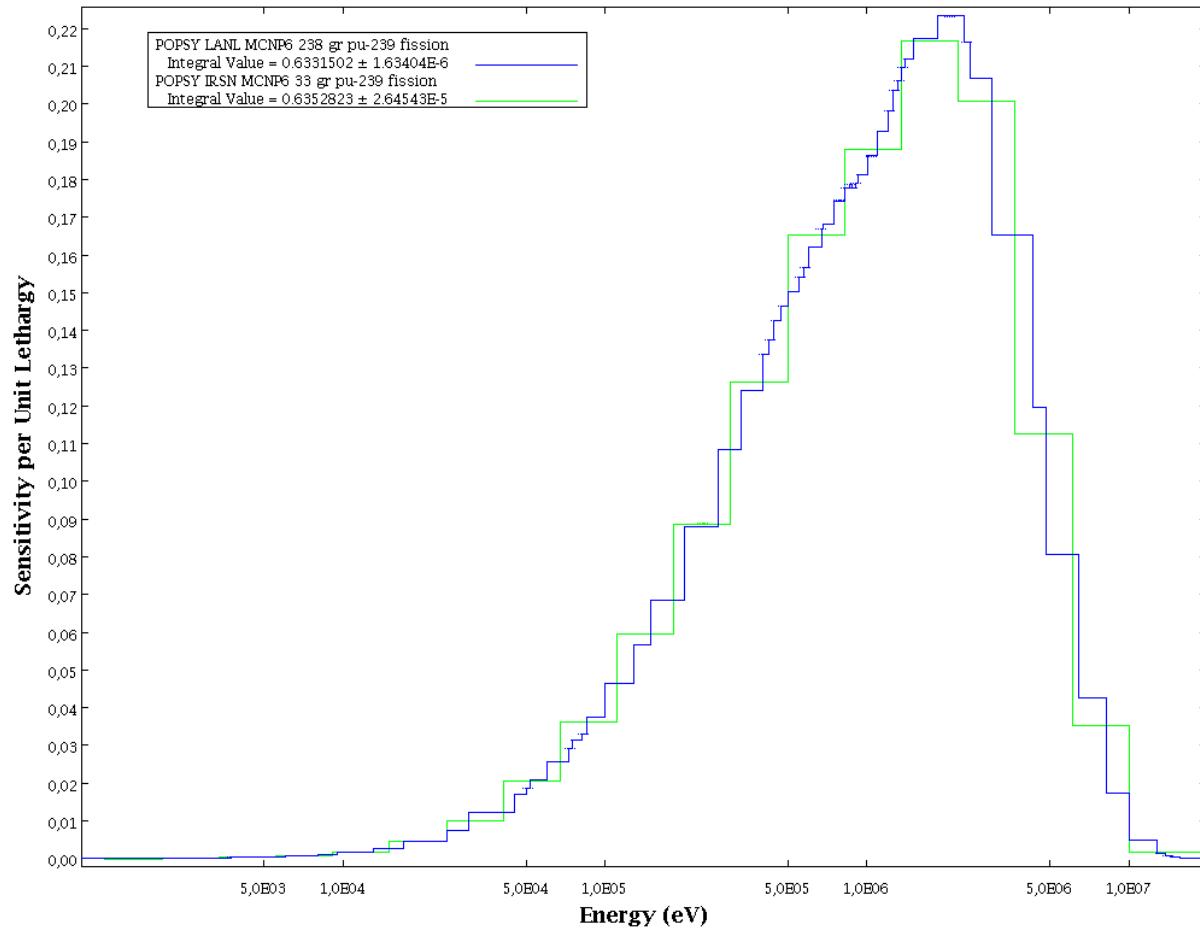
is a number of particles appeared in the point  $\mathbf{r}$  being born in fissions caused by neutron emitted in the point  $\mathbf{r}'$

Formally any infinitely derivable function can be taken instead of adjoint source density, but normalization factor might be unknown if it will be another spatially distributed function.

$$\langle \lambda_i \cdot \hat{\mathbf{F}} \cdot \vec{\Phi}_i, \vec{\Phi}_j \rangle = \langle \lambda_j \cdot \hat{\mathbf{F}}^+ \cdot \vec{\Phi}_j, \vec{\Phi}_i \rangle = a_{i,j} \cdot \delta_{ij}$$

Note It has been proven that the bias of the sensitivity sampling estimator equals zero; e.g. asymptotical convergence of statistical integration to mathematical expectation exists. However there is no one theory to prove the rate of convergence - how many particles are needed to converge the sensitivities, as well there is no proven procedure to associate sampling dispersion with sensitivity profiles parameters.

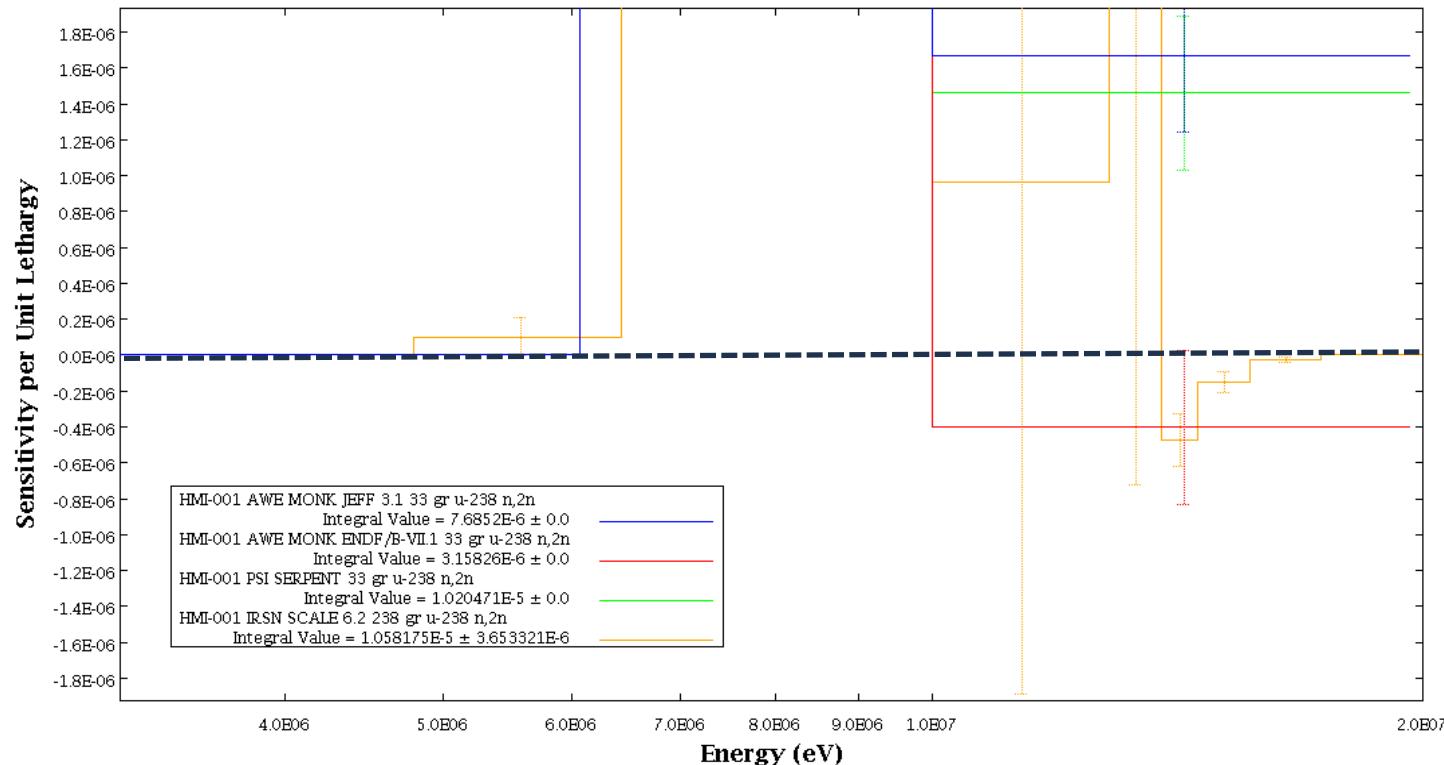
# Popsy: Pu-239 Fission, MCNP6 238 gr. vs 33 gr.



# ZPR9/34: Negative $S_{n,2n}$ Example

MONK with JEFF  
MONK with ENDF  
SERPENT  
SCALE 6.2B

U-238     $n,2n$  reaction  
U-238     $n,2n$  reaction  
U-238     $n,2n$  reaction  
U-238     $n,2n$  reaction  
Zero level



# Summary and Conclusions

- Selected four physically complex benchmarks, sensitive to neutron albedo, enable to highlight angular related issues in sensitivity calculations, if any
- Collected results from 7 organizations that generated sensitivities using 8 codes/methods (6 MC codes and 3 deterministic SN codes)
- Good agreement between deterministic and all MC sensitivities is observed for nu-bar, fission, and capture profiles
- MC scattering sensitivities depends on statistical options
- In general, all tested MC methods and codes demonstrate consistency in the results that confirms the methods maturity

# Other experimental data: SNEAK 7A $\beta_{\text{eff}}$ uncertainties

