

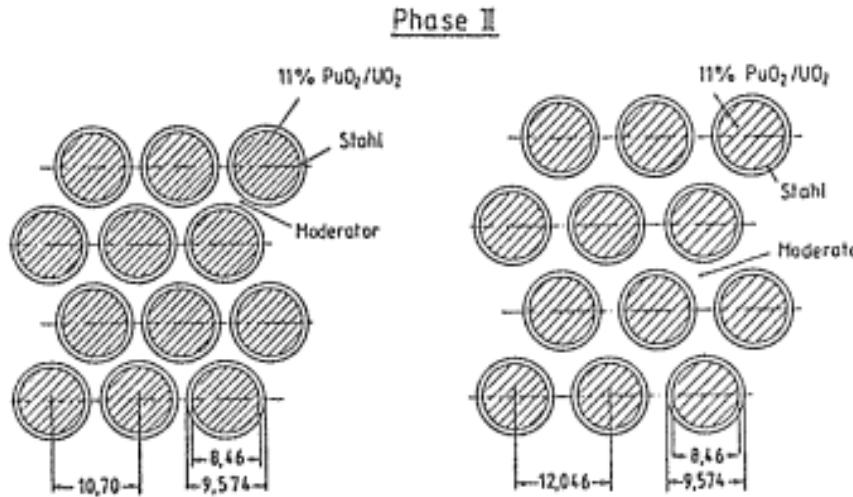
**Wir schaffen Wissen – heute für morgen**

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**PROTEUS FDWR-II (HCLWR) program summary for SG-39**

# FDWR-II – Experimental Configurations

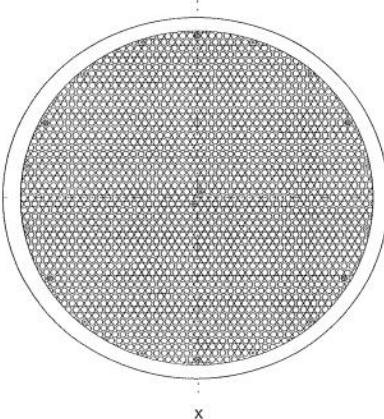


Kern	p/d	$V_M/V_F$	Moderator	Eff. Moderation
7	1.12	0.48	$H_2O$	0.48
8	1.12	0.48	ohne	0.00
9	1.12	0.48	Dowtherm	0.28
10	1.12	0.48	Dowtherm	0.28
11	1.12	0.48	ohne	0.00
12	1.12	0.48	$H_2O$	0.48
13	1.26	0.95	$H_2O$	0.95
14	1.26	0.95	ohne	0.00
15	1.26	0.95	Dowtherm	0.55
16	1.26	0.95	$H_2O$	0.95
17	1.26	0.95	ohne	0.00
18	a)	2.07	$H_2O$	2.07
19	1.26	0.95	$H_2O$	0.95
20	1.26	0.95	$D_2O$	-

## FDWR Phase II

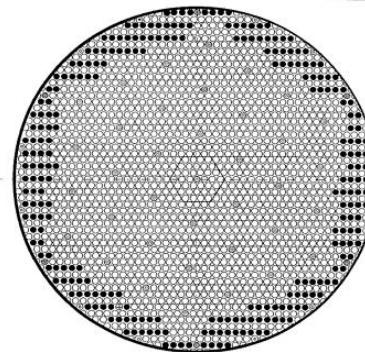
- From 1985 to 1990 in PROTEUS reactor
- PROTEUS is a driven system whose test zone contains the FDWR lattices
- $UO_2/PuO_2$  pellets with 11%  $PuO_2$
- Pu(8/9/0/1/2): 1%, 64%, 23%, 8%, 4%
- Fuel diameter: 8.46mm
- Fuel total height: 84 cm
- 2 axial blankets:
  - Udep. 0.224w%  $^{235}U$
  - 28-cm high each
- Several moderation conditions
  - Two triangular pitches
  - Different moderators (water, dowterm, air)

# FDWR-II – Experimental Configurations



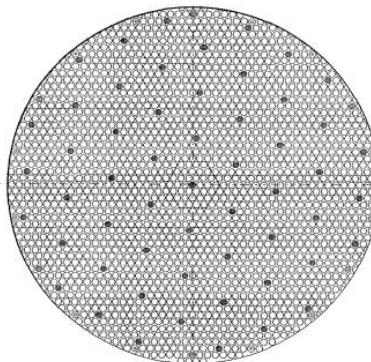
## Core 7,8,9

- Homogeneous ( $V_m/V_f = 0.48$ )
- Water, air and downterm moderators
- $B_4C$  central pin and moderator hole
- Axial MOX blanket interface in central pin



## Core 10

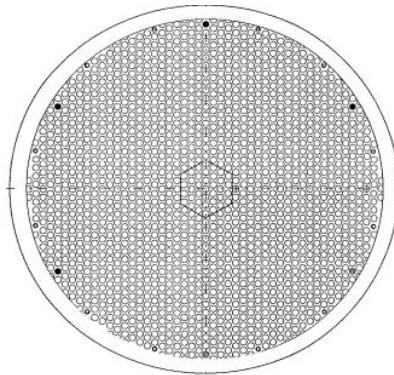
- Heterogeneous with water holes at the periphery and 37  $B_4C$  absorber rods
- Downterm (41.4% void)



## Core 11, 12

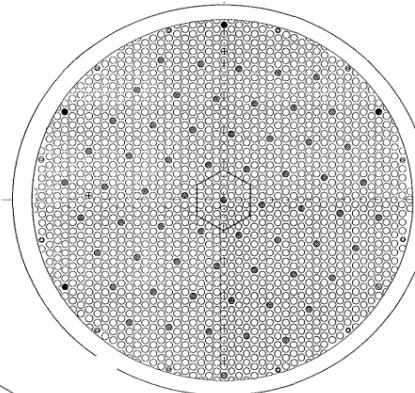
- Heterogeneous with 55  $B_4C$  absorber pins
- Air und Wasser

# FDWR-II – Experimental Configurations



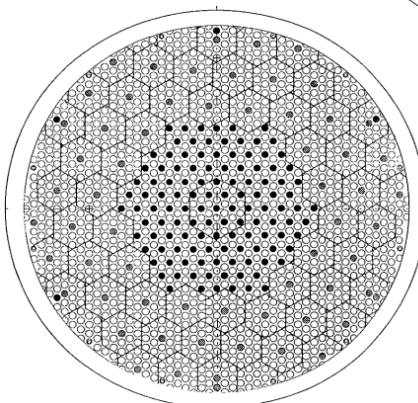
## Core 13, 14, 15

- Homogeneous ( $V_m/V_f = 0.95$ )
- Water, air and downterm moderators
- $B_4C$  central pin and moderator hole
- Axial MOX blanket interface in central pin



## Core 16, 17

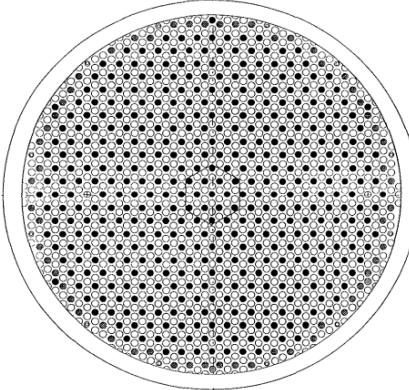
- Heterogeneous with 61  $B_4C$  absorber pins ( $V_m/V_f = 0.95$ )



## Core 18

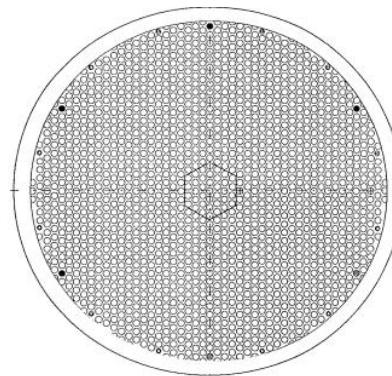
- Heterogeneous with 60  $B_4C$  absorber pins and 121 water holes ( $V_m/V_f = 2.07$ )

# FDWR-II – Experimental Configurations



## Core 19

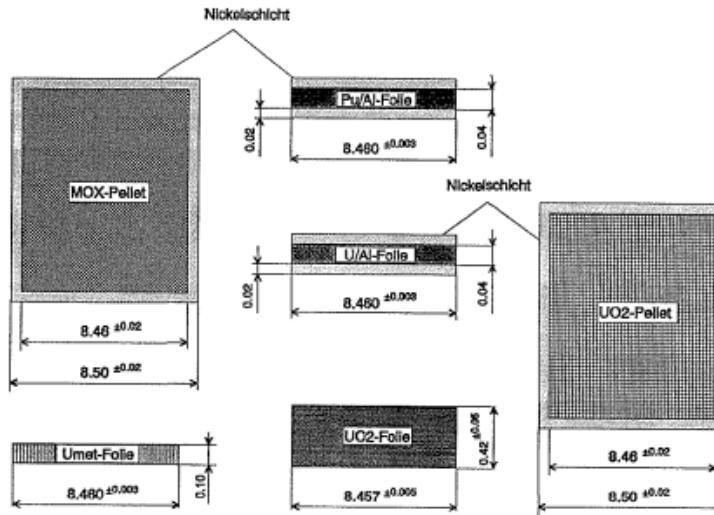
- Heterogeneous with a 2:1 ratio of  $\text{PuO}_2/\text{UO}_2$  and  $\text{UO}_2$  0.22w% pins ( $V_m/V_f = 0.95$ )
- Water, air and downterm moderators
- $\text{B}_4\text{C}$  central pin and moderator hole
- Axial MOX blanket interface in central pin



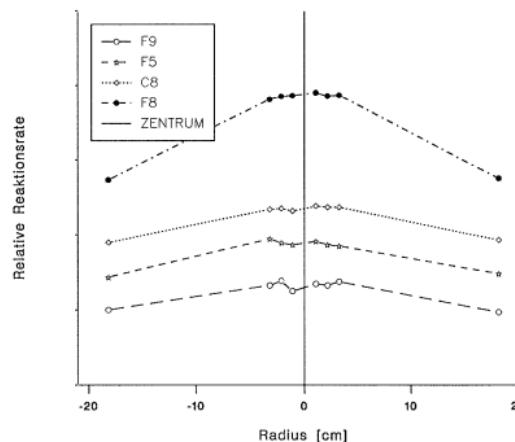
## Core 20

- Homogeneous
- $\text{D}_2\text{O}$  moderator
- $\text{B}_4\text{C}$  central pin and moderator hole
- Axial MOX blanket interface in central pin

# FDWR-II – Measurement types



Ungestoertes Gitter (Kern 7)  
Y-Richtung (13.1.88); F9 ( $R = -18.19\text{cm}$ ) normiert auf 1.0

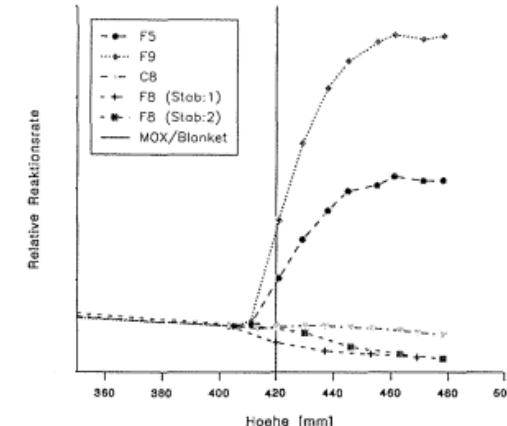


## Spectral index measurements (core 13 - ref)

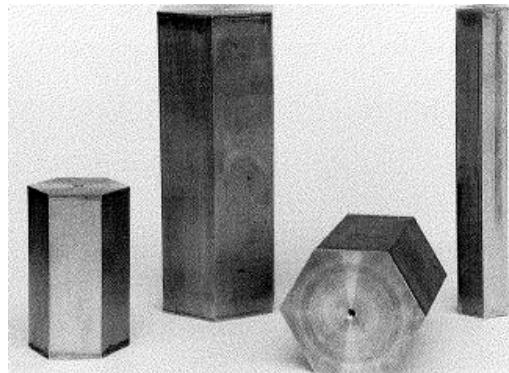
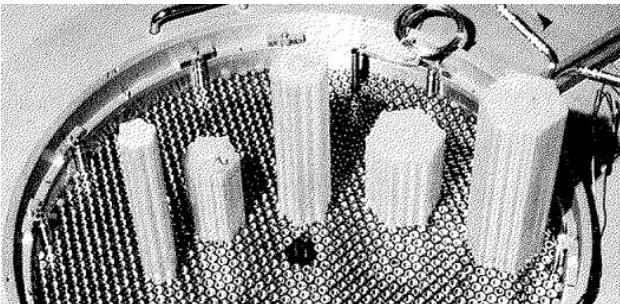
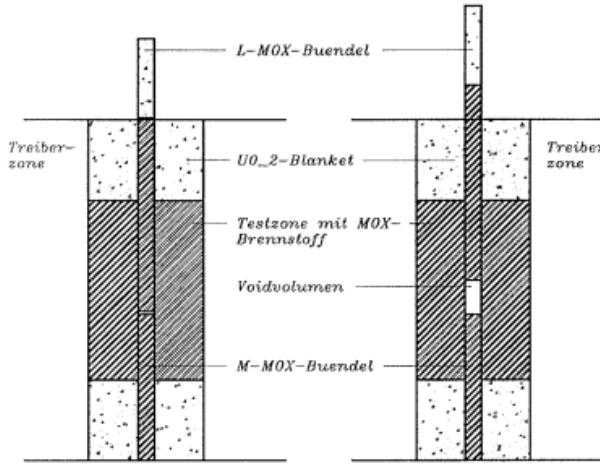
- $F5/F9 \sim 0.72$        $F1/F9 \sim 1.50$
- $F8/F9 \sim 0.89$        $C2/F9 \sim 0.94$
- $C8/F9 \sim 5.1e-2$
- Typical uncertainties  
 $F5: 1.4\%$ ,  $F8: 2.0\%$ ,  $F9: 1.4\%$ ,  $C8: 1.8\%$

## Reaction rate radial and axial traverses

Axiale Traverse durch MOX-Blanket Interface  
Folien (23.2.1986), normiert auf 1.0 bei 404 mm



# FDWR-II – Measurement types



- **K $\infty$  measurements**

$$k_{\infty} = 1 + B^2 \cdot M^2$$

$$\frac{\rho_Z}{\rho_S} \frac{S}{R_f} = \bar{\nu} \frac{\bar{\Phi}^{+X}}{\bar{\Phi}^{+S}} \left( 1 - \frac{1}{k^+} \right)$$

- Using axial and radial bucklings
- Using compensation methods with auto-rod and a  $^{252}\text{Cf}$  sources

- **Reactivity effects of**

- Void volume
- Moderator volume
- Absorber rods

Absorber	Form	Durchmesser	Cladding	Bemerkung
B <sub>4</sub> C(nat)	Pellet	7.473	ja	Referenzabsorber
B <sub>4</sub> C(nat)	Pulver	7.430	ja	
B <sub>4</sub> C(93%) <sup>10</sup> B	Pellet	7.430	ja	
Ag15In5Cd	Legierung	8.830	nein	
Hafnium	Metall	8.350	ja	
Gd <sub>2</sub> O <sub>3</sub>	Pellet	8.310	ja	
Sm <sub>2</sub> O <sub>3</sub>	Pellet	7.000	ja	
Tantal	Metall	8.290	ja	
Eu <sub>2</sub> O <sub>3</sub>	Pellet	8.243	ja	
Zircaloy-2	Legierung	8.300	nein	Strukturmaterial
Stahl	Metall	8.240	nein	Strukturmaterial

## PSI

- Cell calculations: WIMSD4 with the WIMS-1981 data library
- Whole reactor calculations: ONEDANT (one dimension transport)
- Macroscopic cross-sections generation:
  - WIMSD4 (P0 transport corrected) → DSNXSL → XSLIB

## KfK

- Cell calculations: KAPER4 with the G69P1V02 data library (69 Groups)
- Whole reactor calculations: 2D DIXY2 diffusion and TWODANT transport codes
- Macroscopic cross-sections with transport corrected P0 and P1, S4

## TUBS

- XS preparation: modified WIPRO, NJOY (ENDF/B-V, JEF-1), various DATUBS-nn
- Cell calculations: SPEKTRA (various libraries)
- Whole reactor calculations: DITUBS (2D diffusion, 35 groups)

## Plans:

In addition to ERANOS, recalculation of these experiments by means of SERPENT-2.

Testing of the new built-in adjoint-weighting sensitivity coefficient methodology by investigating these reactivity effects.

Detailed testing is currently undergoing for the sodium void in the framework of ESNI+ leading to promising results. GPT will be available in the next official release of the code (Manuele Aufiero).

Inclusion of SERPENT-2 based sensitivity coefficients and these experiments in data assimilation studies, e.g. the SG33 benchmark.

(Question: what should be used in multi-group cross-section adjustment studies, namely “complete” or explicit sensitivity coefficients ?)